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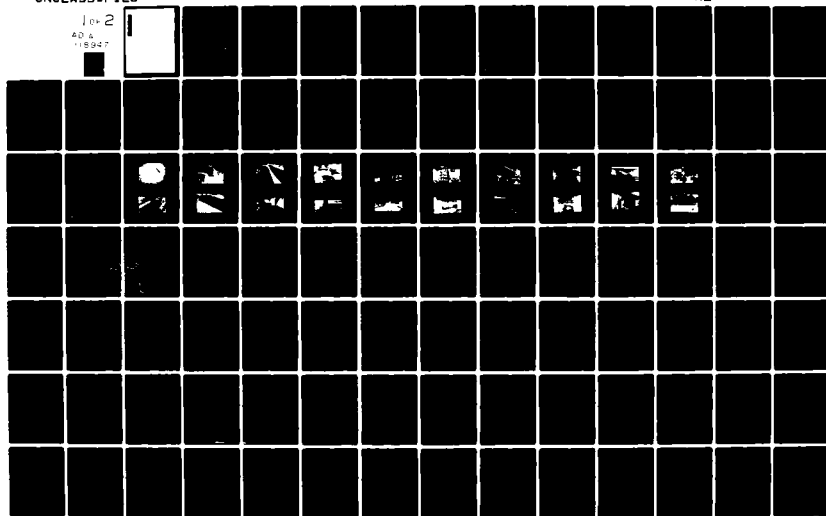
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US ARMY, CORPS OF ENGINEERS

OPERATION AND MAINTENANCE MANUAL

MELVERN LAKE
Marais des Cygnes River, Kansas

APPENDIX V

EMBANKMENT CRITERIA AND PERFORMANCE REPORT

August 1982



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KANSAS CITY DISTRICT, CORPS OF ENGINEERS

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OPERATION AND MAINTENANCE MANUAL
MELVERN LAKE
MARAIS DES CYGNES RIVER, KANSAS

APPENDIX V
EMBANKMENT CRITERIA AND PERFORMANCE REPORT

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DEPARTMENT OF THE ARMY
KANSAS CITY DISTRICT, CORPS OF ENGINEERS
700 FEDERAL BUILDING
KANSAS CITY, MISSOURI 64106

MELVERN LAKE
MARAI DES CYGNES RIVER, KANSAS

APPENDIX V
EMBANKMENT CRITERIA AND PERFORMANCE REPORT

CHAPTER 1
GENERAL

1-01. Location. Melvern Lake is located 4 miles west of Melvern, Kansas. The dam crosses the Marais des Cygnes River (Osage River in Missouri) in Sections 1, 2 and 12, T18S, R15E, and Section 35, T17S, R15E, in Osage County. See Plate No. 1.

1-02. Project Authorization. Melvern Lake was authorized by Federal flood control legislation and constructed by the US Army Corps of Engineers, Kansas City District. This project was authorized by the Flood Control Act of 1954 (Public Law 780, of the 83d Congress).

1-03. Project Purpose. The purposes for which Melvern Lake was constructed are flood control, water supply, improved water quality, public recreation, and benefits to fish and wildlife.

1-04. Purpose and Scope of the Report. The purpose of this Embankment Criteria and Performance Report is to assemble information on the embankment conditions of the project. It provides a summary record of significant design data, design assumptions, design computations, specification requirements, construction equipment, construction procedures, construction experience, field control and record control test data and embankment performance as monitored by instrumentation during construction and during initial lake filling. This report is intended to provide in one volume the significant information needed by engineers to (1) familiarize themselves with the project, (2) re-evaluate the embankment in the event unsatisfactory performance occurs, and (3) provide guidance for designing comparable future projects.

Pertinent Data

1-05. General.

Location of the Project	On Marais des Cygnes River, 4 miles upstream of Melvern, Kansas
Operating Agency	Corps of Engineers Project Manager onsite
Purpose	Flood control, water supply, water quality, recreation, and fish and wildlife
Authorization	Flood Control Act of 1954, Public Law 83-780, Water Supply Act of 1958, Title II Public Law 85-500
Closure of Dam	2 October 1970
Began Multipurpose Operations	January 1975
Cost of Project Dam & Reservoir	\$26,230,000 (1963)

Basin

Drainage area above Dam	349 square miles
Approximate Length of Lake	13 miles
Average Width of Lake	1 mile
Channel Capacity:	
Dam to confluence with 110-mile Creek	9,000 sec.-feet
Zero damage flow in above reach	7,000 sec.-feet
Fee Taking Line, elevation m.s.l.	1,062.0 feet
Maximum Discharge of Record at Melvern, Kansas, 11 July 1951	68,500 c.f.s.

Dam and Embankment

Type	Rolled earthfill
Fill Quantity	8,000,000 cubic yards
Crest Elevation	1078.0 feet
Top Width	30 feet
Maximum Base Width	915 feet

Dam and Embankment --con.

Length	9,750 feet
Maximum Height above Streambed	123 feet
Freeboard	3 feet
Type and Number of Instrumentation Devices:	
Air Operated Earth Pressure Cells (Goetzl Cells)	5 each
Sonic Transducer Boxes	6 each
Piezometers in Conduit	24 each
Alinement Lines	2 each
Air Operated Pore Pressure Cells	31 each
Open Tube Piezometers	33 each
Settlement Devices	3 each
Settlement Monuments (on crest)	9 each

Reservoirs

<u>Pool</u>	<u>Elevation of Top of Zone (ft., m.s.l.)</u>	<u>Surface Area (Acres)</u>	<u>Storage Allocation</u>	
			<u>Initial (ac.-ft.)</u>	<u>100-year (ac.-ft.)</u>
Surcharge	1073.0			
Flood Control	1057.0	13,950	209,000	200,000
Multipurpose	1036.0	6,930	154,000	137,000
Gross Storage		---	363,000	337,000
Sedimentation Reserve				26,000*

*Initial distribution 1/3 (9,000 acre-feet) to the flood control zone and 2/3 (17,000 acre-feet) to the multipurpose zone.

Spillway

Location	2,000 feet beyond left abutment
Type	Uncontrolled
Crest Elevation	1057.0 feet
Width	200 feet
Discharge Capacity at Elevation 1073.0 feet	35,500 c.f.s.
Side Slopes	1 on 2.5

Outlet Works

Location	Dam Station 45+00 near right abutment
Type	Single Horseshoe, 11.5 feet diameter
Invert Elevation of Conduit	Intake 962.0 feet Outlet 952.0 feet
Length of Conduit	Portal to Portal 855 feet Conduit only 767 feet
Capacity at Elevation 1057.0	Two service gates fully open - 7,100 c.f.s.
Capacity at Elevation 1036.0	Two service gates fully open - 6,300 c.f.s.
Service Gate No., Size, Type	Two 6- by 12-foot, hydraulically operated slide gates with 2- by 2-foot low flow gate
Emergency Gate No., Size, Type	Two 6- by 12-foot, hydraulically operated slide gates
Stilling Basin	30- by 84-foot single rectangular

1-06. List of Contracts.

<u>Project</u>	<u>Contract No.</u>	<u>Construction Dates</u>	
		<u>Begun</u>	<u>Accepted</u>
Relocation of State Highway	67-C-0015	28 Oct 66	5 Nov 73
Right Abutment Access Roads	67-C-0164	29 May 67	3 Jul 68
Construction of Melvern Dam	68-C-0012	10 Aug 67	21 May 73

List of Contracts. --con.

<u>Project</u>	<u>Contract No.</u>	<u>Construction Dates</u>	
		<u>Begun</u>	<u>Accepted</u>
Construction of Administrative Facilities	68-C-0018	31 Aug 67	4 Oct 68
Relocation, Rearrange- ment or Alteration of Facilities	68-C-0021	22 Jan 68	3 Nov 72
Alteration of Gas Pipeline	70-C-0014	9 Apr 70	13 Apr 71
Relocation, Removal and Alteration of Powerlines	70-C-0047	29 Jun 70	6 Nov 72
Relocation, Removal of Electrical Powerlines	71-C-0003	12 Jul 70	15 Aug 73
Relocation, Altera- tion, and Removal of Telephone Lines	71-C-0016	8 Jan 71	9 Sep 72
Relocation and Alter- ation of Telephone Facilities	71-C-0017	23 Jun 71	5 Oct 72
Osage County Road Relocation and Sun Dance Public Use Area Development, Phase I	71-C-0018	26 Aug 70	13 Dec 72
Clearing, Stage I	71-C-0135	17 May 71	10 Feb 72
Construction of Public Use Area Development, Phase I	72-C-0005	6 Aug 71	2 Jun 72

List of Contracts. --con.

<u>Project</u>	<u>Contract No.</u>	<u>Construction Dates</u>	
		<u>Begun</u>	<u>Accepted</u>
Construction of Osage County Road Relocation, Phase II	72-C-0086	11 Feb 72	1 May 74
Lake Clearing, Stage II	72-C-0108	28 May 72	29 Sep 72

1-07. Project Features. The project consists of three principal features; (1) rolled earthfill embankment, (2) controlled outlet works, and (3) uncontrolled service spillway. See Plate No. 2. The embankment extends 9,750 feet across the valley and rises 123 feet above the streambed. The controlled outlet works consists of an intake tower, a conduit extending through the embankment, a stilling basin, and approach and outlet channels. The control tower is equipped with two hydraulically operated slide gates and two emergency gates to regulate the flow through the dam. The single horseshoe conduit 11.5 feet in diameter, is 767 feet long and has a discharge capacity of 7,100 cubic feet per second at full pool. The stilling basin is constructed to reduce the velocity of water released through the conduit before flowing into the outlet channel. The uncontrolled, 200 feet wide emergency service spillway is located in a small draw on the left abutment. The spillway concrete control sill, 25 feet in breadth, extends across the entire spillway width and is anchored to the limestone below. The spillway crest elevation 1057.0 controls the full pool reservoir which has a storage capacity of 337,000 acre-feet. The Melvern Lake multipurpose pool elevation is 1036 feet, with a surface area of 6,930 acres extending upstream approximately 13 miles from the damsite to a point in the streambed near the Lyon-Osage County line north of Reading, Kansas. The flood pool elevation, 1057.0 feet, has a surface area of 13,950 acres. The dam is situated just downstream from where Elm Creek, 142-Mile Creek, Duck Creek, and Hill Creek all converge to form the main stem of the Marais des Cygnes River. The general flow of the Marais des Cygnes River is eastward toward the Kansas-Missouri state line. In western Missouri, it is joined by a number of other streams to form the Osage River, which flows into the Missouri River just east of Jefferson City, Missouri. The Osage River, together with its Marais des Cygnes River tributary, drains a watershed area of 15,300 square miles in east-central Kansas and west-central Missouri. Three hundred and forty-nine (349) square miles of this watershed comprise the drainage area for Melvern Lake.

1-08. Embankment Description. The embankment is approximately 9,750 feet in length, with a maximum height above the streambed of 123 feet, and an average height above the flood plain of 100 feet. Elevation of top of dam is 1078.0, which includes freeboard allowance of 5.0 feet above the maximum spillway design flood. Crest elevation of the uncontrolled service spillway is at full pool elevation 1057.0, 21.9 feet below top of dam. The rolled fill embankment consists of impervious, pervious, random, and berm zones. The centrally located impervious zone includes a cutoff trench extending to bedrock. The upstream and downstream random and berm zones were designed to make use of material from required excavations and near by borrow. A downstream inclined and horizontal pervious drain are provided for seepage control. In order to decrease the length of the conduit and provide better seepage control, the embankment around the conduit was constructed entirely of impervious except for the pervious drain. The top width of the embankment is 30 feet, and accommodates a 30-foot wide service road. For the typical valley section an upstream slope of 1V on 3H has been used from the crest (elevation 1078.0) to elevation 1041.0, followed by a 1V on 8H slope to elevation 1015.0, then a 1V on 4H slope to the ground surface. The downstream valley slope is a 1V on 2.5H from the crest to elevation 1048.0, followed by a 1V on 6H slope to elevation 1008.0, then 1V on 4H to the ground. The conduit section upstream slopes are 1V on 3H to elevation 1048.0, 1V on 5H to elevation 988.0, and 1V on 3.5H to the ground surface. The downstream conduit slopes are 1V on 2.5H to elevation 1048.0 and 1V on 5H to the service road behind the stilling basin.

1-09. History of Construction Contract. The basic embankment and outlet works construction was accomplished in one stage, beginning in August 1967, and final acceptance of the work was made 21 May 1973. Excavation and embankment placement was done by the prime contractor, Cook Construction Company of Jackson, Mississippi. The drilling and grouting for the grout curtain was accomplished by subcontractor, Golden Drilling Company of Golden, Colorado. The concrete structures for outlet works and stilling basin were done by subcontractor, Bushman Construction Company of Grand Island, Nebraska. All work during construction was done under the supervision of the Resident Engineer's office, Melvern Dam and Reservoir, Mr. Kenneth A. Rowen, Resident Engineer. Initially Mr. Reuben J. Vig was the Project Geologist followed by Mr. John Doty. Mr. Marty Mueller was the chief embankment inspector. Total bid price of the construction contract was \$9,834,632; total final payment was \$10,056,206.10. There were a total of 45 modifications to the contract.

1-10. Significant Operational Events. The only significant operational events since project completion have been associated with

pool levels. The first event was the first filling of the reservoir, beginning in March 1973 and continuing in June 1975 when the pool rose to elevation 1040.0. (Multipurpose pool elevation 1036.0 was reached in April 1975.) The second event occurred on 27 June 1977 when the pool reached a maximum elevation of 1047.07, 11.07 feet above the normal pool. The project stored 246,650 acre-feet of flood water and prevented significant flood damage downstream. Slow release of the storage continued until the pool was again at the normal level. The embankment, outlet works, and riprap protection performed satisfactorily during these two events.

CHAPTER 2 SITE GEOLOGY

2-01. Geologic Structure. The Melvern Lake is located within the Osage Plains section of the Central Lowlands Physiographic Province. The topography is that of a dissected plain developed on unequally resistant shale and limestone formations. The gently rolling topography has valleys which are comparatively wide in reference to the height of the surrounding hills. The hills have moderate to steep slopes and are about 100 to 150 feet above the valley floor. Kansas is in the Central Stable Region of North America, an extension of the Canadian Shields. A thin mantle of sedimentary rocks consisting of many thin units lying nearly parallel to one another cover the Pre-Cambrian complex. The Melvern damsite lies in the southwestern part of the structure province called the Forest City Basin. The proximity of the Basinal axis, the Brownville Syncline to the Nemaha Anticline produces an asymmetrical profile. The beds on the west flank are relatively steep while the beds on the east flank rise gently toward the Ozark Dome in Missouri. The gradual westward dip of 20 to 30 feet per mile from the Ozark Dome to the Brownville Syncline forms the structure called the Prairie Plains Homocline. Melvern damsite is located on the Homocline. Pleistocene deposits in Kansas consist chiefly of fluvial deposits. Glacial sediments left by the retreating ice sheet occurs only in the northeastern section of Kansas. The fluvial deposits in the streambeds and flood plain of the valleys consist of clay, silt, sand and gravel. These deposits are of Wisconsin and Recent age. The embankment fill was obtained from the unconsolidated deposits of Recent and Pleistocene age. This material consists of residual, colluvial, and fluvial deposits. The major source of material for the embankment was obtained from the alluvial deposits of the flood plain in the upstream and downstream borrow areas. See Plate Nos. 11, 12 and 13 for geologic information. Preliminary investigations for the Melvern damsite were made during the fall and winter of 1940-41, and included 23 borings, as part of a study on the Marais des Cygnes basin. Investigations include a total of 327 additional borings consisting of auger, drive, push (undisturbed) and core (primarily NX 2-1/8 inches), made during the period from September 1963 through September 1966. Refraction seismograph and electrical resistivity studies were also used for investigations. Foundation borings for the embankment, spillway and outlet works structures were obtained. Many of the embankment foundation borings were assigned to obtain undisturbed samples for triaxial testing of bedrock members. The siting of the spillway and intake tower structures were dependent primarily on the position of certain limestone members. During construction, about 20 test pits were dug in the borrow areas by a bulldozer. The purpose was to obtain additional information for delineating the type of borrow material available for the embankment. Embankment observation devices were installed during the fall of 1967 and spring of 1968. A total of 39 holes were drilled; 24 for pore pressure devices; 12 for piezometers; and 3 for settlement plates.

CHAPTER 3
EMBANKMENT DESIGN AND CONSTRUCTION

3-01. Foundation and Abutment Treatment. The foundation for the cutoff trench was excavated to firm bedrock. Considerable more excavation was required than originally estimated, due to highly weathered and jointed limestone. Vertical joints in the limestone varied from hairline up to 1 foot in width. The larger joints were filled with a very soft, moist, fat clay which was not considered to be a suitable material. Badly weathered limestone was removed until the joint openings were closer spaced and contained a sufficient cover of firm shale above it. A modification was made to the contract to place filter gravel against exposed ledges of limestone on the downstream side of the cutoff trench. The purpose was to prevent piping of impervious fill through any passageways in the limestone. No leakage problems were anticipated and leakage around the ends of the abutments would require long passage for the water. Extension of the grout line at both ends of the abutment could be accomplished easily at little expense requiring no drilling in the embankment fill. The shale of the Tecumseh A was very soft and moist in the vicinity of station 37+00 and some trouble was encountered in cleaning the foundation before placing impervious backfill. Artesian pressure was encountered in grout holes in this area. The artesian elevation is at or above multipurpose pool of 1036.0.

3-02. Seepage Control.

a. General. Seepage beneath the embankment is controlled by the impervious cutoff and bedrock grouting under the embankment impervious zone. Seepage through the embankment is controlled by an inclined and horizontal pervious drain.

b. Underseepage. A cutoff trench was determined necessary because of the possible permeability and interconnection of the lower foundation lenses and strata as interpreted from borings; the borderline factors of safety against uplift pressure at the downstream embankment toe, and the inability to design relief wells to relieve excess pressures in the semipervious thin lensed water bearing strata.

c. Through-seepage. Several different geometric configurations for the pervious zone were considered. The adopted design was the most economical scheme considered fully adequate. An alternate material considered for use in the horizontal portion of the adopted design was 3 feet of grizzled rock mixed with 18 inches of grizzly fines. The cost of this alternate was \$330,000 more and was not considered as desirable as the natural sand that was used. Because the pervious material was costly, extensive studies were undertaken to obtain maximum seepage

control with minimum pervious material. Positioning of the inclined pervious was the result of stability studies which balanced overall embankment size and required quantities for pervious material. The selected position utilized the maximum stability for the smallest embankment and pervious drain size. The inclined pervious location assures the saturation line is kept well within the downstream slope and provides filter protection against failure due to embankment cracking for the most frequent pool elevations.

3-03. Slope Protection.

a. General. Two graded riprap layers were placed on the embankment. The 30-inch layer which was placed above elevation 1037.0 and on the 1V on 5H conduit slope, was underlain with a 12-inch spall layer and 12-inch bedding layer. The 24-inch graded riprap layer on the 1V on 8H slope was placed over a 9-inch spall layer and 6-inch bedding layer the riprap and embankment. A 5-foot layer of limestone was placed on the 1 on 8 slope between elevations 1015.0 and 1027.0 (10-year drawdown). A 3-foot layer of limestone and shale was placed between the natural ground and elevation 1015.0. A 36-inch graded riprap layer (with 12-inch spalls and 12-inch bedding) was placed in the stilling basin area of the outlet channel. Stone for riprap was not blasted or quarried between 1 October and 1 April. Type "C" (36-inch) riprap in the closure area was stockpiled and allowed to dry for a period of 3 months prior to placement. To facilitate drying, the stockpile did not exceed 6 feet in height.

b. Placement. The better quality rock material was used for the graded riprap. Poorer quality materials (limestone and shale) were used between the bottom of the riprap and natural ground. The poorer quality rock provided protection while the reservoir was being filled and in case lower drawdown occurs. Each layer of slope protection was placed in one operation to the full layer thickness. To provide increased erosion protection on the berm, a minimum 5-foot layer of fat clay was placed immediately underlying the slope protection. Since fat clay was in ample supply in the borrow area and was a short haul, its use at this location was cost effective.

c. Gradations. The 5-foot layer of limestone fill was hard durable limestone with a maximum allowable size of 30 inches. Fifty percent of the rock was between 6 inches and 12 inches, with 5 to 20% passing the 2-inch screen. The 3-foot layer of limestone and shale on the 1 on 4 slope between natural ground and elevation 1003.0 was a well graded mixture of Jackson Park Shale from required excavation. Between elevation 1003.0 and 1015.0 the shale-limestone contained a uniform distribution of limestone and shale from the Ozawakie Limestone Zone "A" spillway excavation. The source of stone for riprap, bedding and spalls

was the Cook Construction Company Quarry located 1-1/2 miles southwest of Melvern, Kansas, NW 1/4 Section 16, T18S, R16E, Osage County. A 16-foot ledge of the Plattsmouth Limestone from the Oredd Formation, Shawnee Group was approved. Stone protection materials were a reasonably uniform material graded from coarse to fine within and between the following limits:

<u>Sieve Size</u>	<u>Bedding</u>	<u>Percent by weight passing</u>
2-inch		Maximum allowable size
1/2-inch		75-95
No. 10		35-50
No. 40		5-20

	<u>Spalls</u>	
8-inch		Maximum allowable size
4-inch		70-90
1 1/2-inch		15-40
1-inch		0-15
<u>Weight in pounds per stone</u>		<u>Percent of total weight lighter than</u>

	<u>Type "A" Riprap (24-inch)</u>
700	Maximum allowable size
500	85-95
200	30-50
50	0-10

	<u>Type "B" Riprap (30-inch)</u>
1,600	Maximum allowable size
1,300	85-95

600	30-10
100	0-10

Type "C" Riprap (36-inch)

2,400	Maximum allowable size
1,800	85-95
600	30-50
50	0-10

3-04. Diversion and Closure. During the initial period of outlet works construction, a levee was built for protection against floods. The river was temporarily diverted into a diversion channel around the approach walls and intake tower, through the embankment area and along the downstream embankment toe. The embankment to the left of the diversion channel was constructed to a minimum elevation of 1041.0, the outlet works completed, and right bank embankment was constructed to elevation 1060.0. Diversion of the river through the outlet works began 15 September 1970. The general plan of making final diversion and closure is shown on Plate No. 7 and involved the following sequence of operations:

- a. Removal of downstream channel plug and outlet works protection levee leaving the upstream river channel plug until last.
- b. Construction of the diversion dike to elevation 979.0.
- c. Foundation excavation and cleanup in closure area.
- d. Construction of the initial upstream cofferdam to elevation 1000.0.
- e. Construction of remainder of the upstream cofferdam to elevation 1015.0 and placement of the downstream cofferdam to elevation 972.0.
- f. Completion of the closure embankment to an effective elevation of 1041.0 by March 1971. Details of the various operations and selection of cofferdam elevations are discussed in subsequent paragraphs.

3-05. Time of Diversion. The period of 1 August to 31 March was selected for diversion and closure. The river was diverted through the outlet works on 15 September 1970 and actual closure of the dam began on 2 October 1970. The upstream cofferdam was constructed to elevation 1015.0 in order to provide protection against flows during the closure period.

3-06. Diversion Dike. The diversion dike was located at the upstream edge of the cofferdam. It had a top width of 15 feet at elevation 979.0. Most of the material was stockpiled adjacent to the riverbank for quick placement at the start of diversion. The resultant dumped fill was sufficiently impervious to reduce the flow without the addition of special blanketing material on the upstream slope other than channel fill. During diversion channel construction muck and silt were removed from beneath the diversion dike and replaced with impervious material. To reach elevation 979.0 the diversion dike required the placement of about 9,000 cubic yards.

3-07. Upstream Cofferdam. A top width of 50 feet was established, which was adequate for a two-way haul road and to allow room for quickly raising the cofferdam if high water occurred. The cofferdam top elevation was 1015.0 and the base width 475 ft. Because the compaction control during the cofferdam construction was difficult and hurried, it was considered to locate the cofferdam slightly outside the upstream embankment slope. However, since the cofferdam was constructed entirely of random material (no berm material), it was finally decided to locate it so the upstream slope coincided with the upstream embankment slope. After the diversion dike construction, muck and silt were removed from beneath the cofferdam, beginning at the upstream end and continuing downstream as the diversion channel drained. The cofferdam was completed as fast as practical by placement of rolled random material, concentrating initially in the upstream area required for initial protection to elevation 1000.0. Impervious channel fill upstream of the cofferdam was placed concurrently with cofferdam construction in order to lengthen the seepage path beneath the cofferdam in the event high water occurred.

3-08. Downstream Cofferdam. Construction of the downstream cofferdam (elevation 972.0) was delayed until the water had drained out of the closure area. This cofferdam was outside the embankment limits; therefore, only traffic compaction was required.

CHAPTER 4
EMBANKMENT SPECIFICATION REQUIREMENTS

4-01. General. Significant types of materials that were placed in the embankment were impervious, random, berm, pervious, and rockfill. Materials were placed in the appropriate embankment zone as determined during the excavation. No material suitable for pervious or impervious was to be placed in the random zone unless it was apparent that there would be a surplus of the appropriate material for the required fill

4-02. Description, Placement, and Density Control of Embankment Material. The embankment specifications were based on guide specifications and experience on similar embankments built throughout the Kansas City District. The compaction specifications was a procedural one in that it specified the equipment and procedure to be used and the conditions of moisture and the material type necessary for compaction. The assumption was that if these procedures were used and the conditions met then the required density would be attained.

4-03. Compaction Equipment.

a. Tamping Rollers. The tamping rollers consisted of heavy duty, double drum units with a drum diameter not less than 60 inches and an individual drum length of not less than 60 inches. The drums were ballasted with liquid or sand and liquid. Each drum had staggered feet uniformly spaced over the cylindrical surface such as to provide approximately three tamping feet for each two square feet of drum surface. The tamping feet were to be seven to nine inches in clear projection from the cylindrical surface of the roller and have a face area of not less than 7 nor more than 10 square inches. The roller was equipped with cleaner bars, so designed and attached as to prevent the accumulation of material between the tamping feet, and these cleaner bars were maintained at their full length throughout the period of roller use. The weight of the roller were not less than 3,500 pounds per foot of linear drum length empty. The design and operation of the tamping roller were subject to approval. The allowable roller was self-propelled, speed was 2-1/2 to 5 miles per hour. The self-propelled sheepsfoot Model 50-55 roller manufactured by R. G. Le Tourneau, Inc. was the approved sheepsfoot roller.

b. Rubber-tired Roller. The rubber-tire rollers has a minimum of four wheels equipped with pneumatic tires. The tires were of such size and ply that they were maintained at tire pressures between 80 and 100 pounds per square inch for a 25,000 pound wheel load during rolling operations. The roller wheels were located abreast and so designed that each wheel carried approximately equal load in traversing uneven ground.

The spacing of the wheels were such that the distance between the nearest edges of adjacent tires were not greater than 50 percent of the tire width of a single tire at the operating pressure for a 25,000 pound wheel load. The wheel suspension was designed for traveling over rough and uneven ground. The roller had a rigid steel frame provided with a body suitable for ballast loading such that the load per wheel may be varied as directed from 18,000 to 25,000 pounds. The roller had to be fitted with cleaner bars if they would increase the equipment efficiency. The entire assembly (roller plus motivating equipment) had to be capable of executing a 180-degree turn on a 25-foot radius. The roller had to be towed at speeds not to exceed 5 miles per hour. The Grace 50 ton Model Mo. W18R, rubber-tired roller was approved for this operation.

c. Vibratory Rollers. The vibratory rollers has a total static weight of not less than 10,000 pounds with at least 90 percent of this weight transmitted to the ground through a single smooth drum when standing on level ground. The drum had a diameter of not less than 48 inches and a width between 60 and 72 inches, and the weight of the drum, shaft and internal machinery was not less than 6,500 pounds. The frequency of vibration during operation was within 1,100 and 1,500 vibrations per minute, and the dynamic or vibrating force at the operating frequency was not less than 15,000 pounds. The roller produced a total minimum compactive effort of 25,000 pounds (dynamic or vibrating force plus the static weight of the roller). The roller was towed at speeds not to exceed 1.5 miles per hour by a suitable crawler-type tractor, or be self-propelled. For self-propelled rollers, in which steering was accomplished through the use of rubber tire wheels, the tire pressure was not to exceed 40 pounds per square inch. The roller was operated in the forward direction except as otherwise approved for the equipment to be used. The Seishuc Model VP-10 was approved for use in compacting the pervious material.

4-04. Moisture Control: Impervious. The moisture content was required to be as uniform as practicable throughout any one layer of material. The upper limit of moisture content was that which permitted excavating, hauling, placing, and proper compaction without excessive deformation of the embankment but was not more than three percent above the optimum value at maximum density. The lower limit of moisture content was not more than two percent below the optimum value. The optimum water content was determined as specified for standard compaction test in Corps of Engineers Manual EM 1110-2-1906 dated 10 May 1965, Appendix VI. Material that had a moisture content greater than specified was spread on the embankment and permitted to dry, assisted by discing or harrowing, if necessary, until moisture content was reduced to within the specified limits. Each layer of material that had a moisture content less than specified was sprinkled on the fill and worked with harrows, discs, or other approved methods until the moisture content was within

the range specified and uniform distribution of moisture was obtained.

4-05. Pervious. The material was wetted as directed, to facilitate compaction. The amount of water added essentially produced saturation when the material was being compacted. Water was applied by power spray, which uniformly wet the material without erosion or ponding.

4-06. Random. Moisture content was controlled the same as impervious.

4-07. Berm. Moisture content was limited to the extent required to permit even routing of the hauling equipment.

CHAPTER 5 INSTRUMENTATION

5-01. General. Instrumentation was installed for the following purposes.

- a. To measure pore pressures during construction in foundation overburden clays and shales.
- b. To measure pore pressures during construction in compacted embankment material.
- c. To measure hydrostatic pressures and establish underseepage gradients in basal gravels after completion of the project.
- d. To measure total earth forces on the side and back of the intake tower.
- e. To measure foundation settlement during and after construction.
- f. To measure combined foundation and embankment settlement upon completion of the project.

Instrumentation to determine foundation excess hydrostatic pressures was limited to the area where the embankment exceeds 50 feet in height. All initial installations were done by hired labor crews who were experienced in similar installations. Extensions as necessary were accomplished by the Contractor.

5-02. Location. The location of all devices are shown in Plate No.14. They are also shown in cross sections at stations where devices have been concentrated.

- a. Devices to check excess hydrostatic pressures in foundation shales are located at stations 44+00 and 84+00 to check the pressure in the Doniphan shale and at station 56+00 to check the Jackson Park shale. They are set in the weathered shale about 10 feet below the top of bedrock.
- b. To check possible pore pressure buildup in the foundation clays during construction, devices were grouped at stations 54+00, 60+00, 72+00 and 80+00, with additional isolated devices at other locations. At each of these stations, the devices were located under the embankment both upstream and downstream of centerline and at the downstream toe to measure possible lateral transfer pressure. The group at stations 72+00

and 80+00 are in the area where the lowest "Q" strengths were measured. Those at station 60+00 measured the possible pressure buildup in the typical valley foundation prior to closure and the group at station 54+00 measured pressures during the rapid construction of the closure area.

c. Embankment pore pressure devices included 5 installations near the bottom of the cutoff trench backfill since these were subjected to the maximum loading. Additional devices were installed at various locations and elevations throughout the embankment.

d. Devices to measure hydrostatic pressures in the foundation basal sands and gravels were located generally at the same stations as the foundation clay pore pressure installations. Because of the unknown continuity and permeability of these foundation gravels, these devices furnished information on possible construction pore pressures if they happened to fall in discontinuous or perched pervious pockets.

e. Five total pressure devices were installed on the intake tower to measure the earth forces transmitted to the tower. Two devices were installed on the side of the tower and three on the back.

f. Three settlement plates were installed at the original ground surface in the valley at stations 53+50, 60+00 and 75+00 to measure foundation settlement during and after construction.

g. Settlement monuments were established along crest of the dam after construction to measure the total embankment and foundation settlement which occurs after construction.

5-03. Pressure Cell and Piezometer Devices. Pneumatically operated pressure cells included both Warlam cells and Shannon-Wilson (Slope Indicator Co.) cells. The Casagrande type (open-tube) were used for the upstream devices to avoid carrying the tubes required by the pneumatic devices through the impervious section of the embankment. The pneumatic devices were used for two reasons: Their response time should be faster than the open-tube devices, especially in clay or shale and they eliminate the construction difficulty of extending pipes up through the embankment. Furthermore, the mortality rate in past installations of the Casagrande type had been quite high because of settlement drag on the pipe, coupling failures and leakage. It was felt that much of this could be avoided with the pneumatic device. A monitor box for reading the Warlam and Shannon-Wilson cells is located at the downstream toe where a number of the lines are collected at one location for reading. The installation details for both pneumatic cells and Casagrande type piezometer are shown on Plate No. 15. Past experience has shown that the principal problems in installations of the Casagrande type in getting a

positive seal at the tip to prevent pressures from escaping along the sides of the drill hole and in providing means to eliminate drag on the pipe above the tip during settlement. Granular bentonite was used to provide a seal in installations where the drill hole was dry. Bentonite balls (Pi-pellets) manufactured by Joy Drilling Co., 700 Whittier St., Bronx, N.Y., were substituted for the granular bentonite where conditions were such that the installation must be made under water. The use of bentonite balls for under water installations has been found to be very satisfactory since they maintain their structure long enough to be tamped. Above the seal, a protective pipe with double bell couplings (slip joints) was installed outside the reading pipe or tubes to prevent settlement drag on the reading pipe. An annular space outside the protective pipe was filled with bentonite to eliminate excessive drag.

5-04. Settlement. The consolidation data and foundation conditions at Melvern were similar to that at Pomona Dam. The accumulated settlement during the embankment construction was observed by periodically reading the settlement plates. Melvern foundation reacted as that at Pomona in that the foundation layer settlement was about 80 percent complete at the end of construction. The dam was overbuilt a foot to compensate for the settlement which occurs after construction.

5-05. Settlement Plates. The three settlement plates were set on original foundation material to monitor embankment settlement with respect to the foundation and any foundation consolidation. The settlement plates are at stations 53+50, 60+00, and 75+00. The 3-inch galvanized steel pipes extend from the foundation bedrock vertically to 3-1/2 feet above the embankment surface and are protected by 6-inch galvanized pipes with caps.

5-06. Settlement Monuments. There are nine 1/2-inch reinforcing rod settlement monuments along the downstream side of the dam crest. The monuments are buried 6 feet in the embankment and extend vertically to within a foot of the dam crest where they are protected by a galvanized pipe and cap. See Plate No. 15 for details. These monuments monitor the combined consolidation of the embankment and foundation. These monuments are read annually. Settlement was essentially complete by 1975. See Plate No. 16 for readings.

5-07. Alinement Lines. Permanent alinement monuments on 200-foot centers were installed in two lines, one on the upstream and the other on the downstream slope of the embankment. The upstream line is set at elevation 1039.6, 3.6 feet above multi-purpose pool, and may be underwater during flood water storage periods. The alinement monuments are used to monitor horizontal and/or vertical movement of the extent embankment slope. See Plates No. 68 and 69 for readings.

5-08. Prototype Test Installation Testing Equipment. The piezometers, sonic transducers, and pressure transducers were installed in the conduit for use by the Waterways Experimental Station in their studies conforming theoretical and actual water velocity design relationships. Twenty-four piezometers and four sonic transducers fittings are monitored in a manometer well located adjacent to the stilling basin. The five pressure transducers are monitored from the intake tower.

PHOTOGRAPHS

PHOTOGRAPHS



1. Melvern Lake, Construction Photo, Neg. No. 375
(Overall view of Melvern Lake)



2. Melvern Lake, Construction Photo, Neg. No. 86612-6
(Placing impervious backfill in cutoff trench)



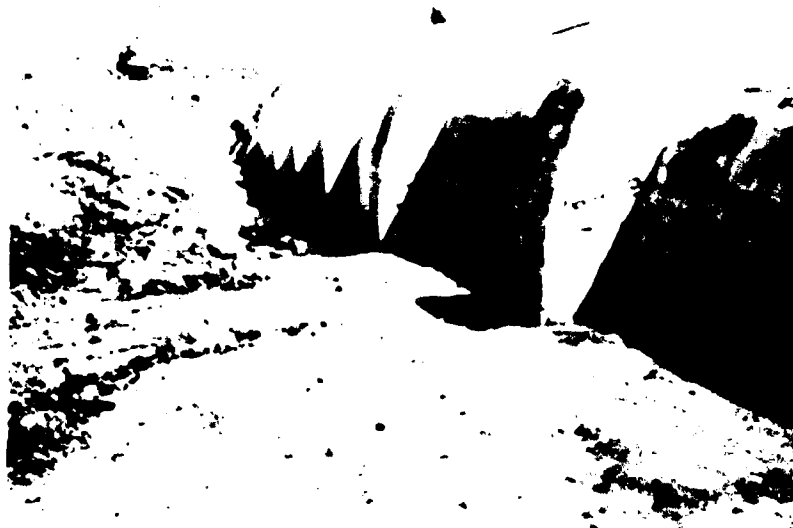
3. Melvern Lake, Construction Photo, Neg. No. 694-R1 -24
(Station 50+50, River Bank, looking up station
cutoff trench)



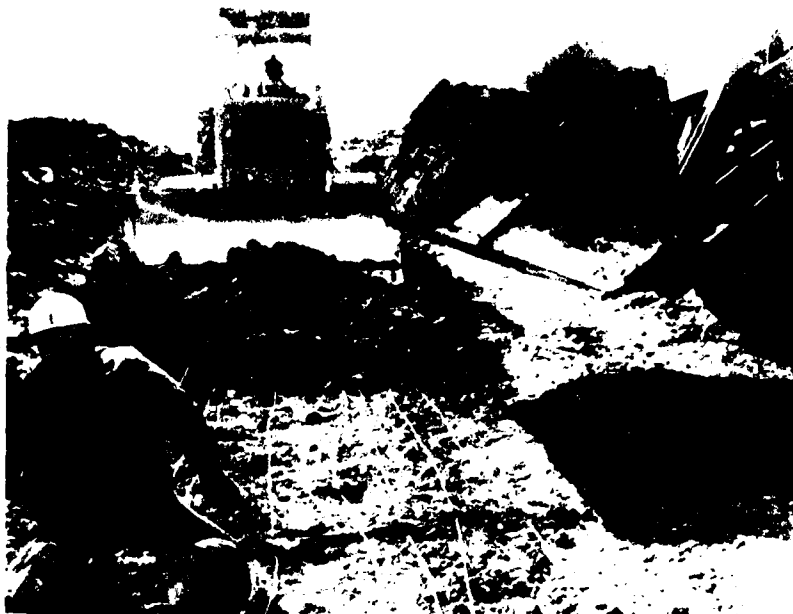
4. Melvern Lake, Construction Photo, Neg. No. 694-R1-23
(Impervious backfill in cutoff trench)



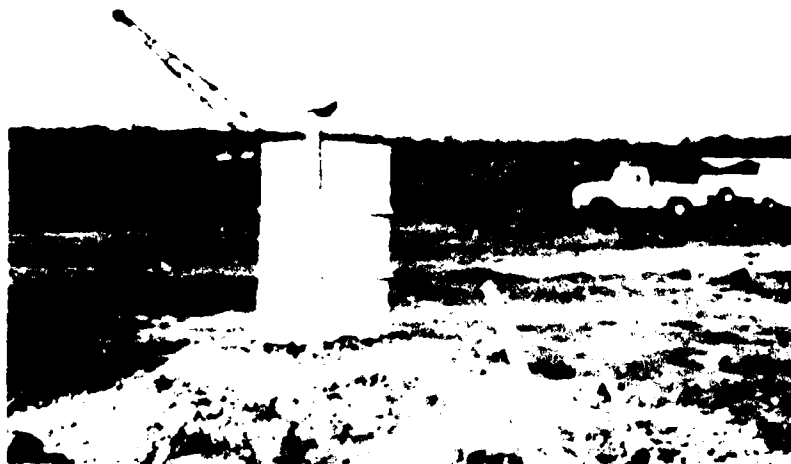
5. Melvern Lake, Construction Photo, Neg. No. 694-R1-3
(Excavation for conduit before placement of backfill)



6. Melvern Lake, Construction Photo, Neg. No. 694-R1-6
Backfill material at seepage and alignment collars
on conduit



7. Melvern Lake, Construction Photo, Neg. No. 85149-1
(Backfill placement in tubing ditch for embankment
pressure cells)



8. Melvern Lake, Construction Photo, Neg. No. 694-R1-15
(Typical piezometer and pore pressure extension
backfill)



9. Melvern Lake, Construction Photo, Neg. No. 694-R2-16
(Typical piezometer and pore pressure devices protection during embankment placement)



10. Melvern Lake, Construction Photo, Neg. No. 694-R1-10
(Self-propelled tamping roller on embankment fill)



11. Melvern Lake, Construction Photo Neg. No. 87531-11
(Placement of fill material in old river channel
for beginning of closure)



12. Melvern Lake, Construction Photo Neg. No. 87531-10
(Foundation excavation and cleanup in old river
channel downstream)



13. Melvern Lake, Construction Photo Neg. No. 88982
(Placement of slope protection on the upstream
embankment)



14. Melvern Lake, Construction Photo Neg. No. 694-R1-5
(General view of slope protection on the upstream
embankment)



15. Melvern Lake, Construction Photo Neg. No. 88987-6
(General view of embankment slope protection near
Station 75+00)



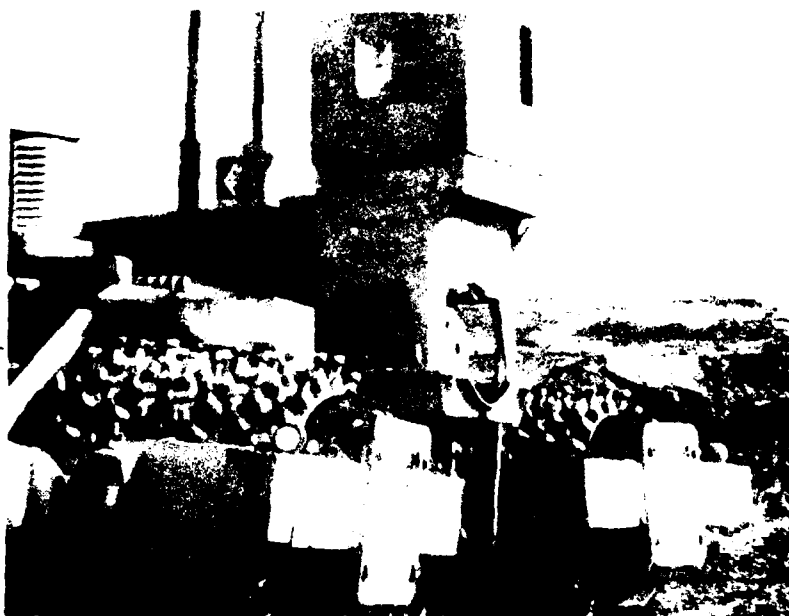
16. Melvern Lake, Construction Photo Neg. No. 88752
(General view of embankment and both valley and
downstream borrow areas)



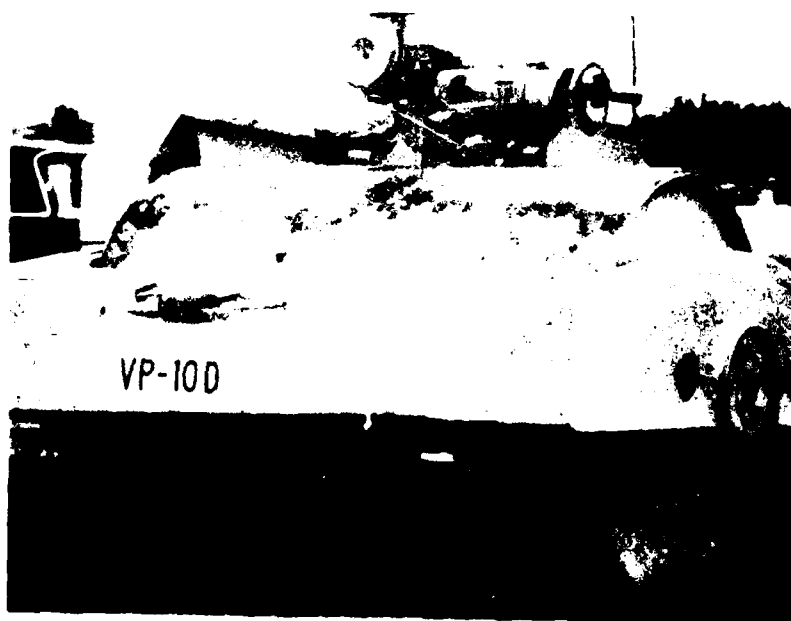
17. Melvern Lake, Construction Photo Neg. No. 694-R1-4
(General view of the outlet channel)



18. Melvern Lake, Construction Photo Neg. No. 88987-7
(View of intake tower and embankment)



19. Melvern Lake, Construction Photo Neg. No. 694-R1-21
(Self-propelled tamping roller)

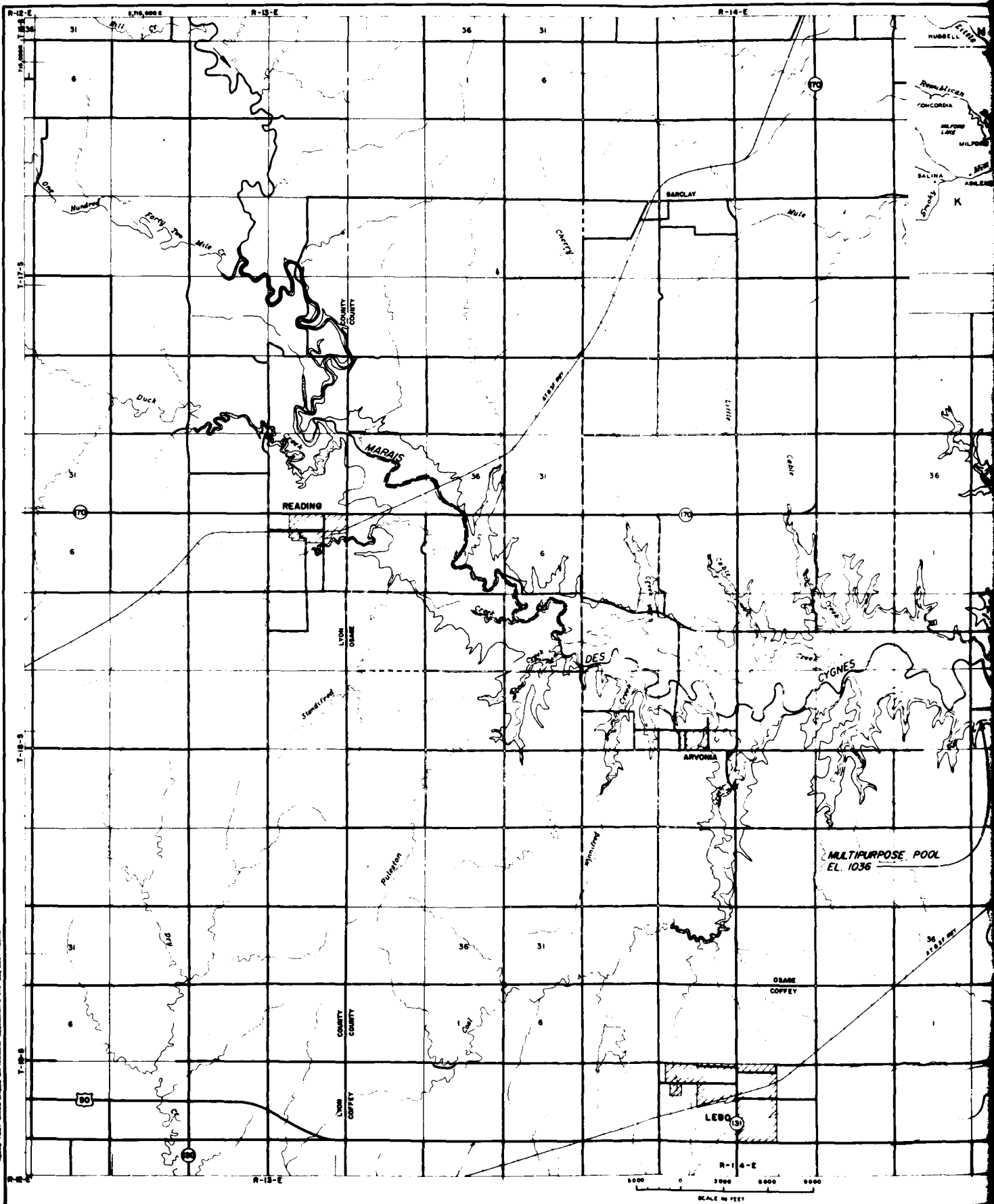


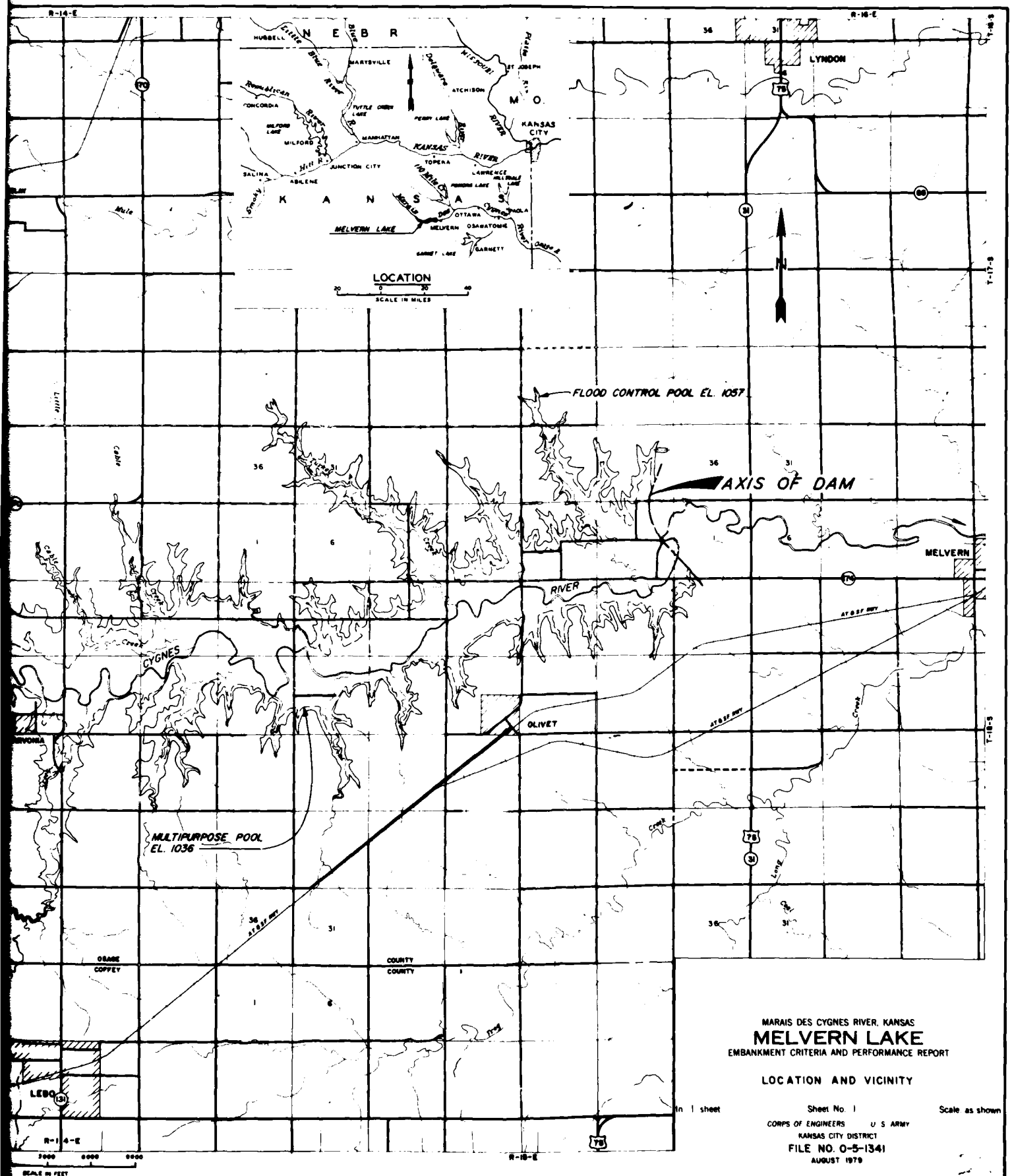
20. Melvern Lake, Construction Photo Neg. No. 694-R1-22
(Vibratory steel drum roller)

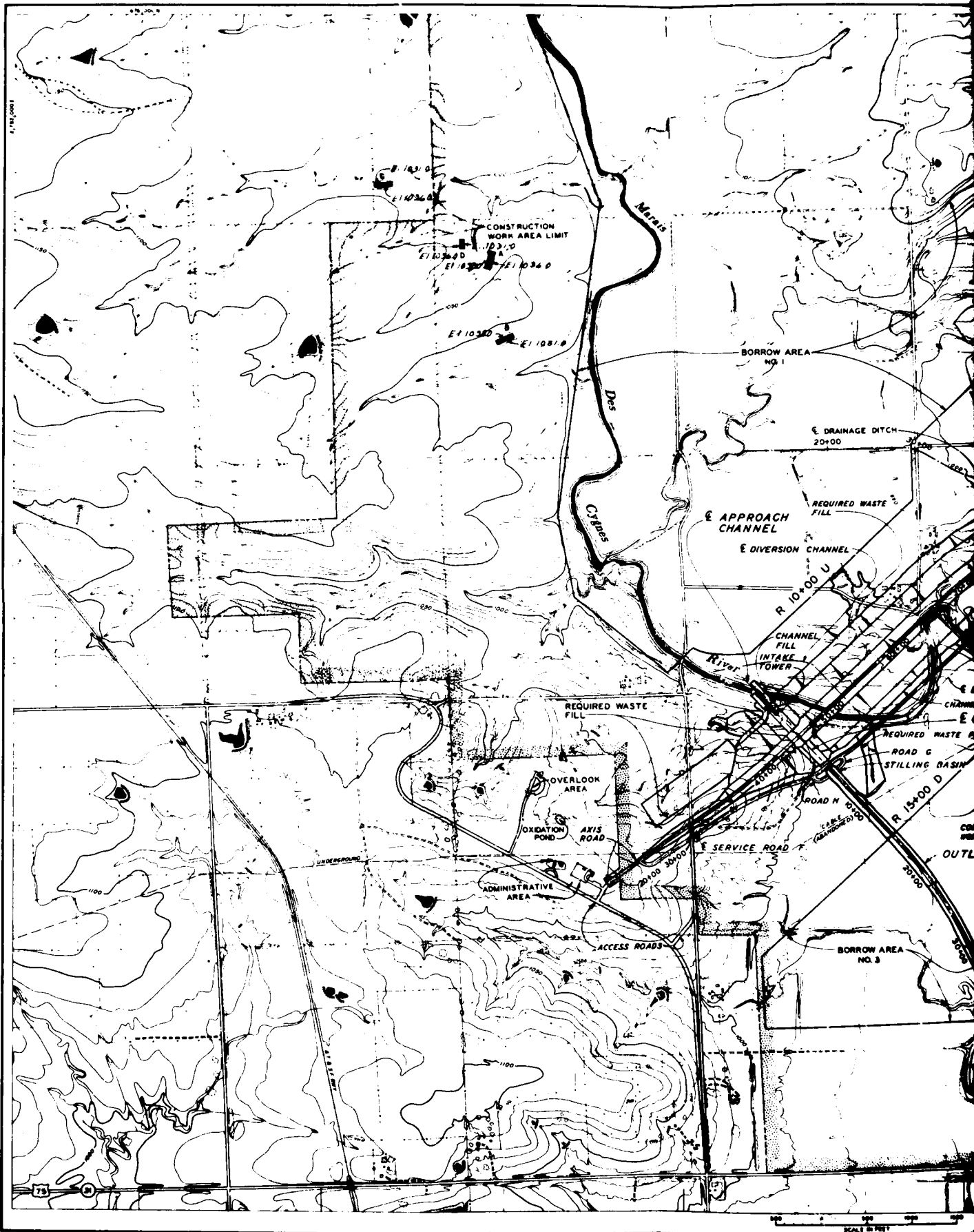
DRAWINGS

DRAWINGS

REVISIONS
July 1964







NOTE: THIS MAP WAS PREPARED BY THE U.S. ARMY CORPS OF ENGINEERS, WASHINGTON, D.C. FROM AERIAL PHOTOGRAPHS TAKEN IN 1960.

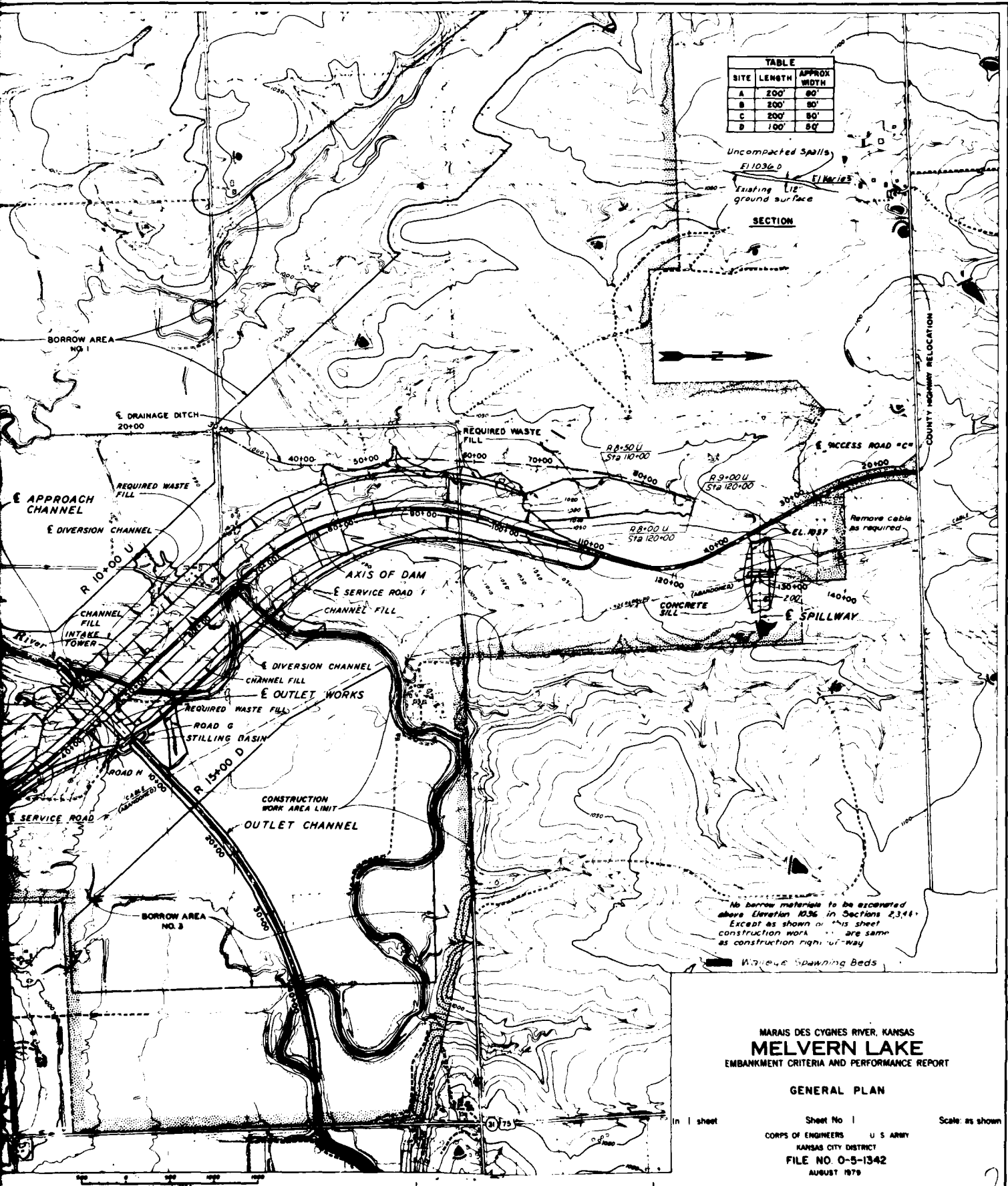
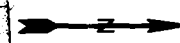
SCALE IN FEET

TABLE		
SITE	LENGTH	APPROX WIDTH
A	200'	80'
B	200'	80'
C	200'	80'
D	100'	50'

Uncompacted Spalls
F11036.0

Existing 12' ground surface

SECTION



MARAIS DES CYGNES RIVER, KANSAS MELVERN LAKE EMBANKMENT CRITERIA AND PERFORMANCE REPORT

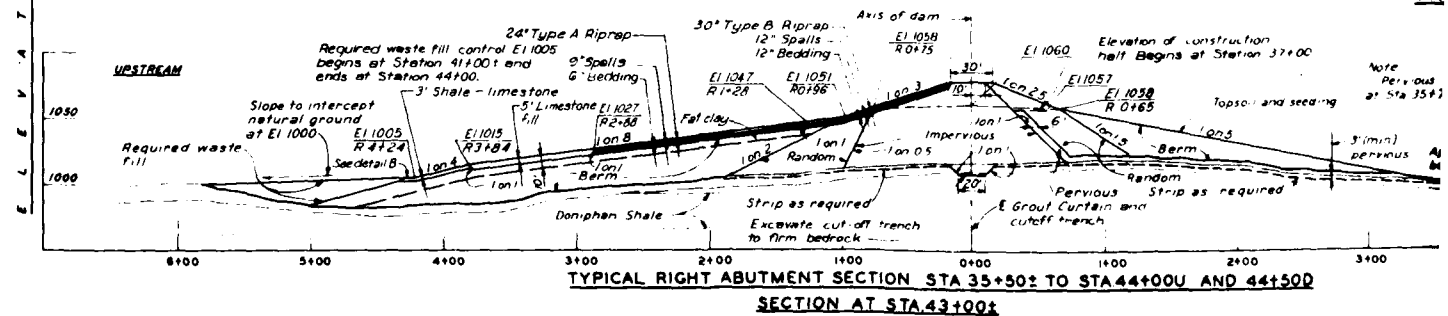
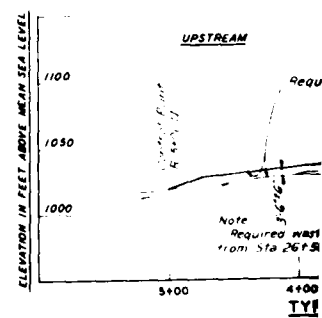
GENERAL PLAN

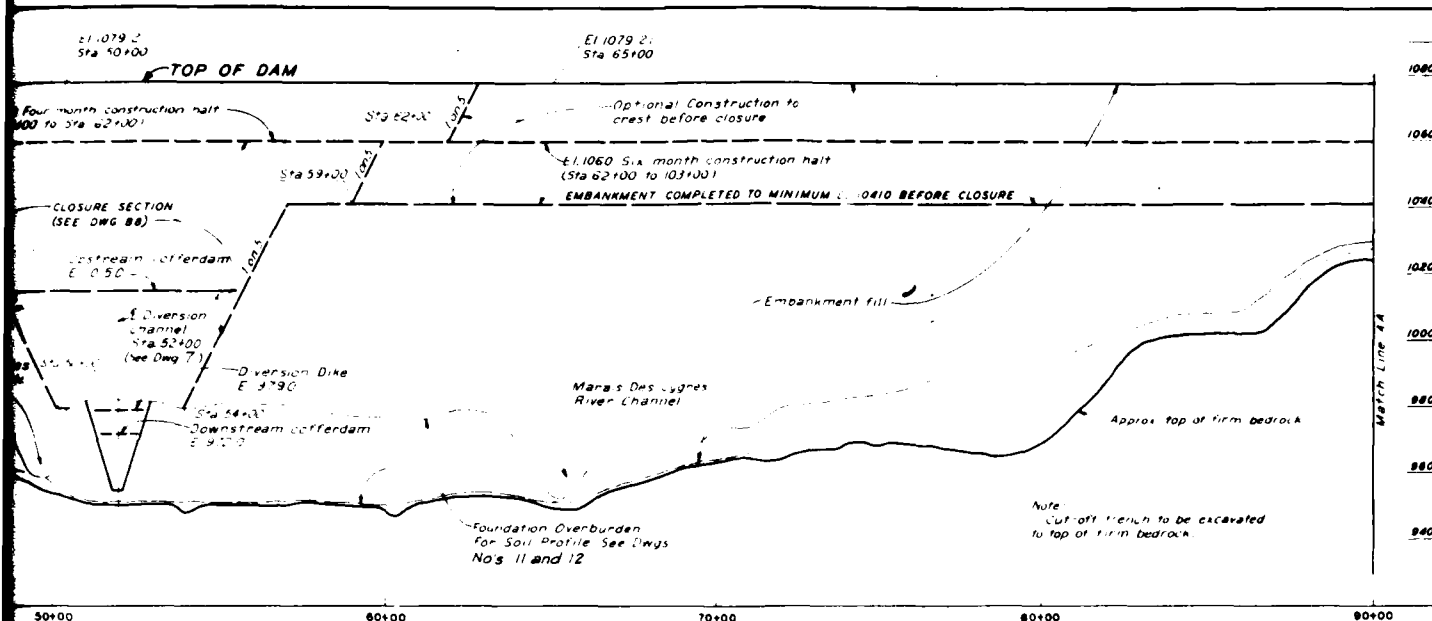
In 1 sheet

Sheet No. 1
CORPS OF ENGINEERS U. S. ARMY
KANSAS CITY DISTRICT
FILE NO. 0-5-1342
AUGUST 1979

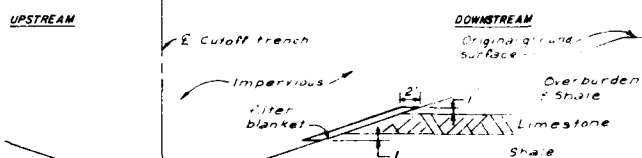
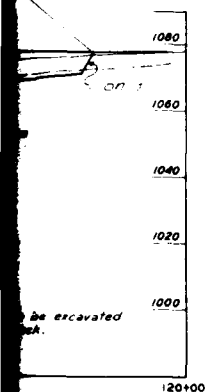
Scale: as shown

SCALE IN FEET



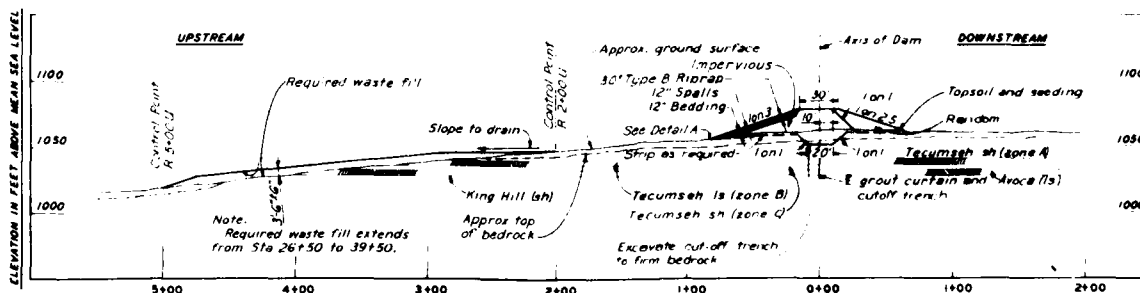


PROFILE ALONG AXIS OF DAM
(LOOKING UPSTREAM)



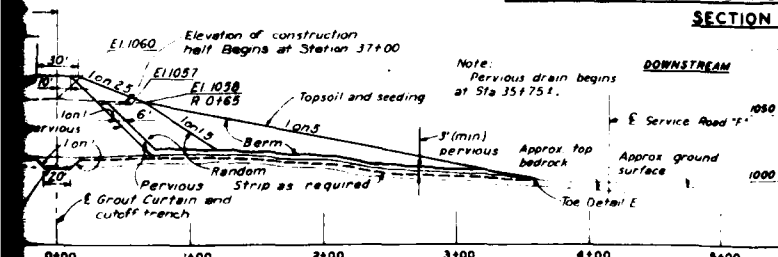
TYPICAL CUTOFF TRENCH CROSS SECTION
NOT TO SCALE

LOCATION WHERE FILTER BLANKET WAS PLACED			
STA	TO	STA	TO
30+35	34+50	82+75	83+65
37+50	38+70	83+65	86+10
40+00	41+36	88+11	94+25
44+30	43+99	96+31	98+07
46+00	46+20	99+20	100+25
48+00	49+66	102+75	107+00
81+00	81+26		



TYPICAL RIGHT ABUTMENT SECTION STA 22+50 TO STA 35+50

SECTION AT STA 34+50



SECTION AT STA 35+50 TO STA 44+00 AND 44+50

MARAI DES CYGNES RIVER, KANSAS MELVERN LAKE EMBANKMENT CRITERIA AND PERFORMANCE REPORT

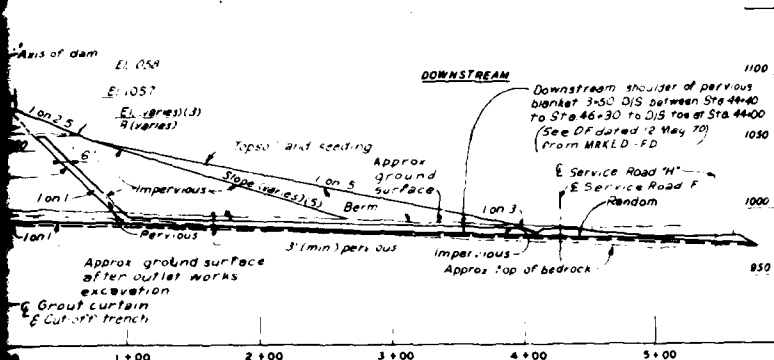
AXIS OF DAM PROFILE AND EMBANKMENT SECTIONS RIGHT ABUTMENT

In 1 sheet

Sheet No 1

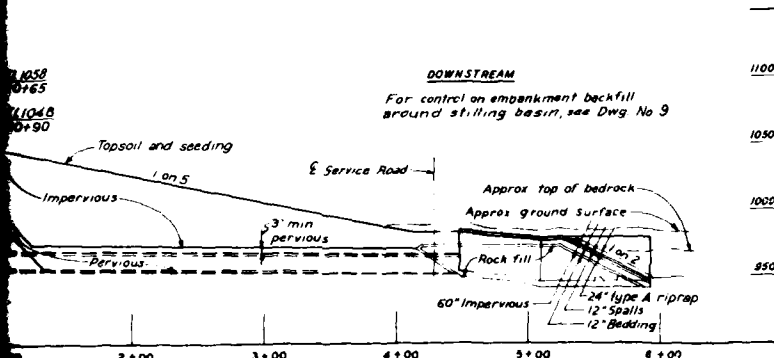
Scale as shown

CORPS OF ENGINEERS U. S. ARMY
KANSAS CITY DISTRICT
FILE NO 0-5-1343
AUGUST 1979

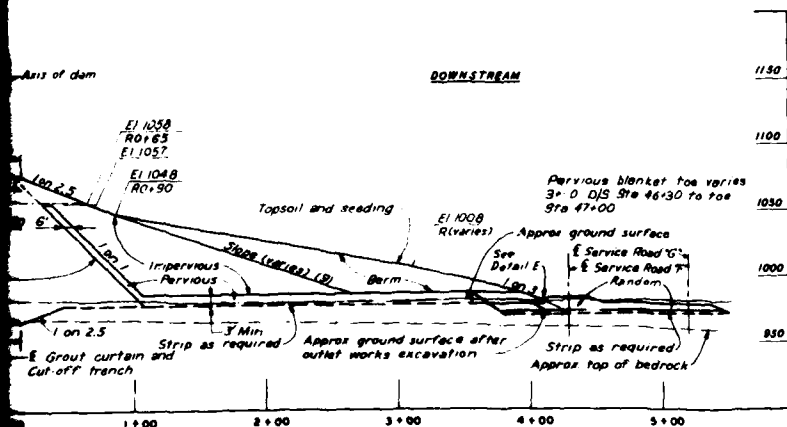


AND 44+50 TO STA. 45+00
 1+55±

Note
 Roadway embankment is
 not continuous between
 Sta 45+00 and Sta 46+00.



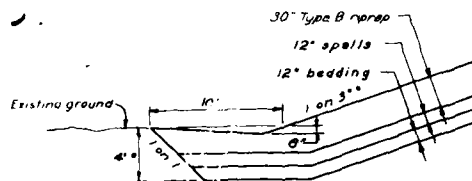
45+00 TO STA. 46+00
 1+50±



46+00 TO STA. 46+80
 1+50±

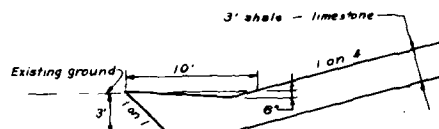
Notes:

- (1) Control point varies linearly from El. 1051, R. 0+96U at Station 44+00 to El. 1048, R. 105U at Station 45+00.
- (2) Control point varies linearly from El. 1015, R. 3+84U at Station 44+00 to El. 988, R. 4+105U at Station 45+00.
- (3) Control point varies linearly from El. 1058, R. 0+65D at Station 44+50 to El. 1048, R. 0+90D at Station 45+00.
- (4) Slope varies linearly from 1 on 2 at station 44+00 to 1 on 5 at station 45+00.
- (5) Slope varies linearly from 1 on 1.5 at station 44+50 to 1 on 5 at station 45+00.



* To bedrock if less than
 a depth of 4 ft
 * Embankment slope at
 toe may be 1 on 8 and may
 have different layer thicknesses

DETAIL "A"
 Not to scale



DETAIL "B"
 Not to scale

Notes:

- (6) Control point varies linearly from El. 1048, R. 1+05U at Station 46+00 to El. 1041, R. 1+26U at Station 46+80.
- (7) Control point varies linearly from El. 988, R. 4+105U at Station 46+00 to El. 1015, R. 3+34U at Station 46+80.
- (8) Slope varies linearly from 1 on 5 at station 46+00 to 1 on 2 at station 46+80.
- (9) Slope varies linearly from 1 on 5 at station 46+00 to 1 on 1.5 at station 46+80.
- (10) For top of dam detail see dwg No 6

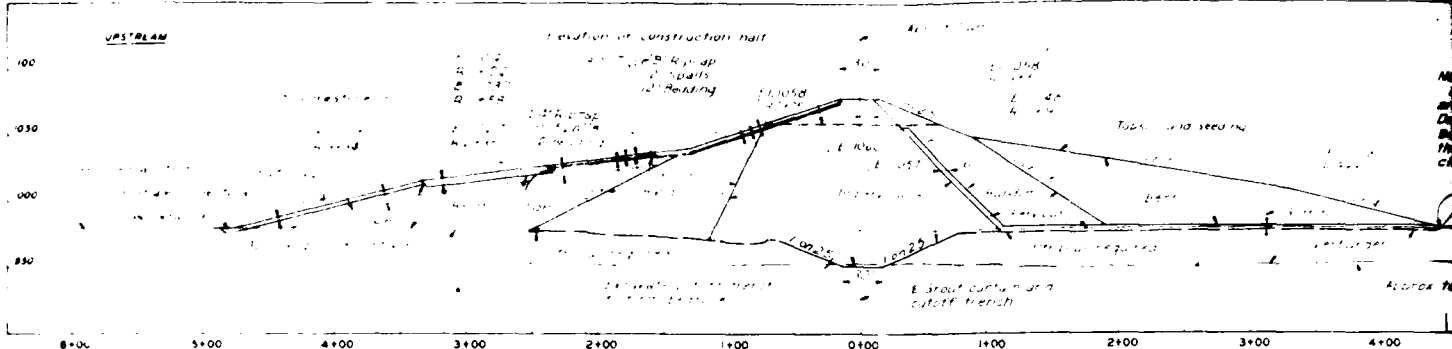
MARAS DES CYGNES RIVER, KANSAS MELVERN LAKE EMBANKMENT CRITERIA AND PERFORMANCE REPORT EMBANKMENT SECTIONS CONDUIT AND TRANSITIONS

In 1 sheet

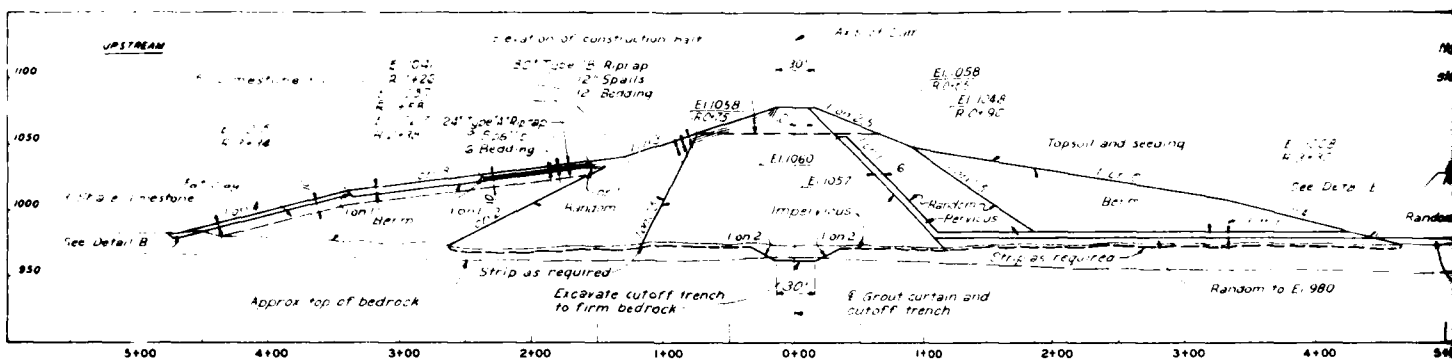
Sheet No. 1
 CORPS OF ENGINEERS U S ARMY
 KANSAS CITY DISTRICT
 FILE NO. 0 5 1344
 AUGUST 1979

Scale as shown

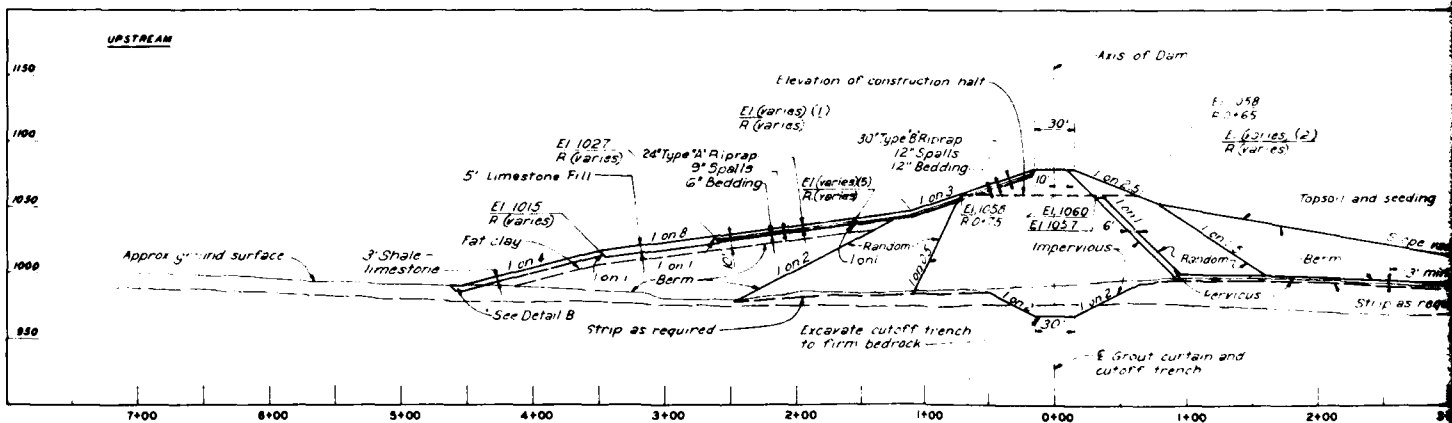
ELEVATION IN FEET ABOVE MEAN SEA LEVEL



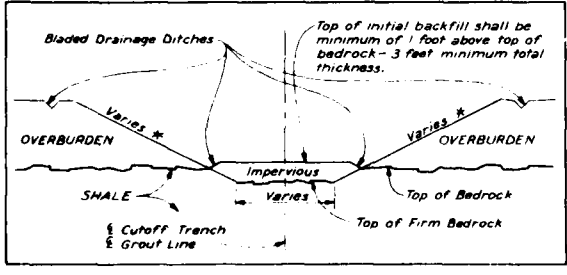
TYPICAL VALLEY SECTION - STA. 46+80 TO STA. 63+00
SECTION AT STA. 60+00±



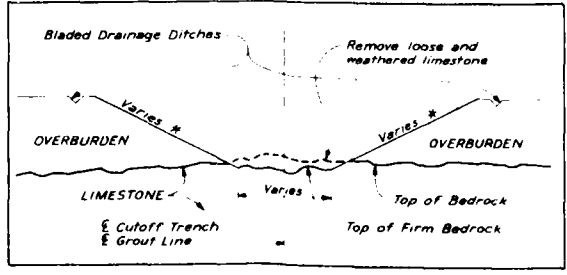
TYPICAL VALLEY SECTION - STA. 63+00 TO STA. 76+00
SECTION AT STA. 70+00±



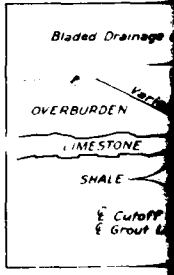
TYPICAL TRANSITION SECTION - STA. 76+00 TO STA. 80+00
SECTION AT STA. 78+00±



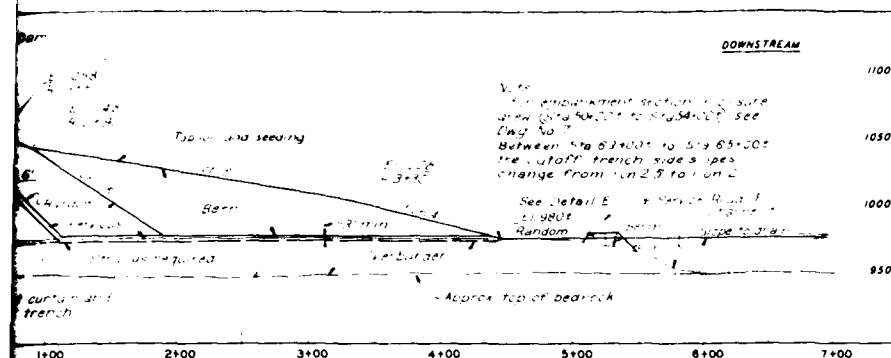
CUTOFF TRENCH DETAIL
BASE IN SHALE
Not to Scale



CUTOFF TRENCH DETAIL
BASE IN LIMESTONE
Not to Scale

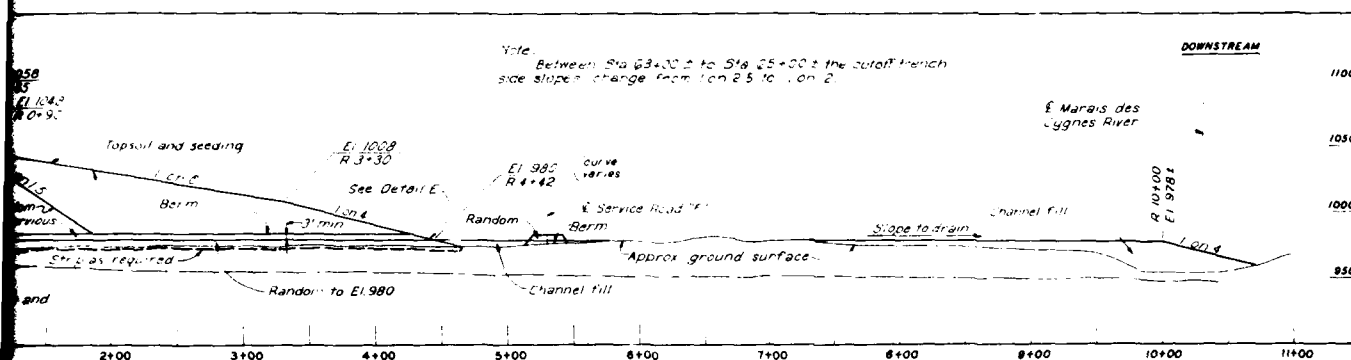


Bladed Drainage
OVERBURDEN
LIMESTONE
SHALE
Cutoff Trench
Grout Line



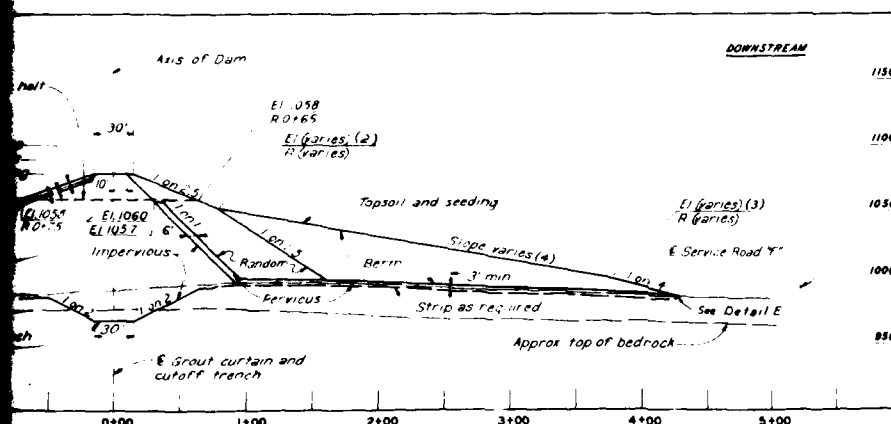
0 TO STA. 63+00

104-1



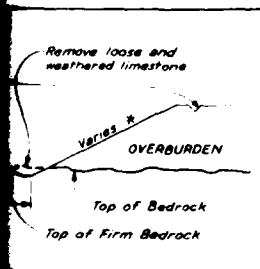
VALLEY SECTION - STA. 63+00 TO STA. 76+00

SECTION AT STA. 70+00±



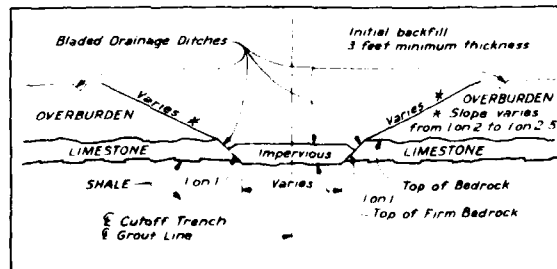
STA. 76+00 TO STA. 80+00

78+00±



DETAIL

STONE



CUTOFF TRENCH DETAIL
BASE THROUGH LIMESTONE IN SHALE
Not to Scale

Notes

- (1) Control point varies linearly from El. 1041, R1+260 at station 76+00 to El. 1051, R0+960 at station 80+00.
- (2) Control point varies linearly from El. 1048, R0+900 at station 76+00 to El. 1058, R0+650 at station 80+00.
- (3) Control point varies linearly from El. 1028, R3+200 at station 76+00 to ground surface elevation 915.1, range 4+1510 at station 80+00.
- (4) Slope varies linearly from 1 on 2 at station 76+00 to 1 on 1.5 at station 80+00.
- (5) Control point varies linearly from El. 1037, R1+58 at station 76+00 to El. 1047, R1+28 at station 80+00.

GENERAL NOTE

River channels existing within the embankment area shall be mucked to remove unsuitable materials and the river banks shall be excavated to 1 on 3 within Range 2+00 upstream to 2+00 downstream then transitioned to 1 on 2 at Range 3+00 up and 3+00 down and maintained 1 on 2 to the embankment toe.

For top of dam detail see drawing No. 104-2

MARAI DES CYGNES RIVER, KANSAS
MELVERN LAKE
EMBANKMENT CRITERIA AND PERFORMANCE REPORT

EMBANKMENT SECTIONS
VALLEY AND TRANSITION

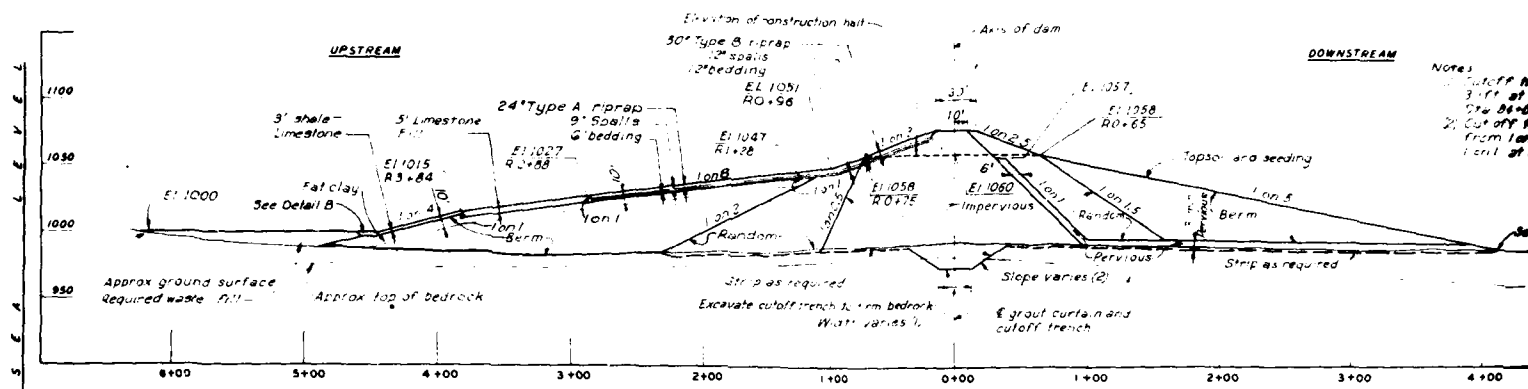
In 1 sheet

Sheet No. 1

Scale as shown

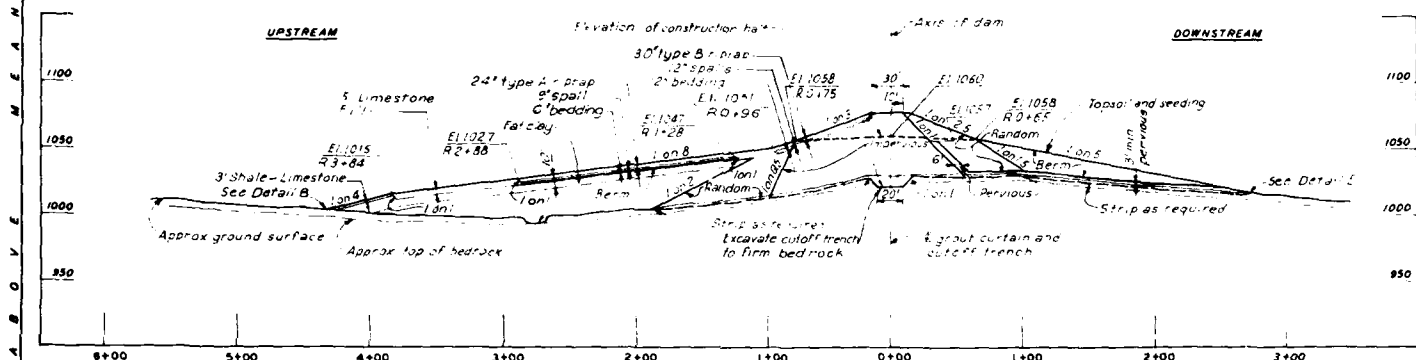
CORPS OF ENGINEERS U.S. ARMY
KANSAS CITY DISTRICT
FILE NO. 0-5-1345
AUGUST 1979

PLATE NO. 5



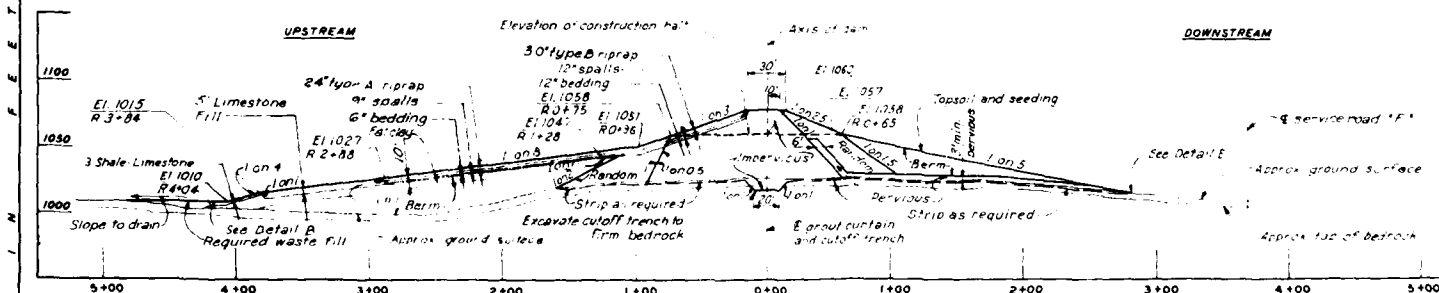
TYPICAL TERRACE SECTION-STA. 80+00 TO STA. 84+00

SECTION AT STA. 82+00±



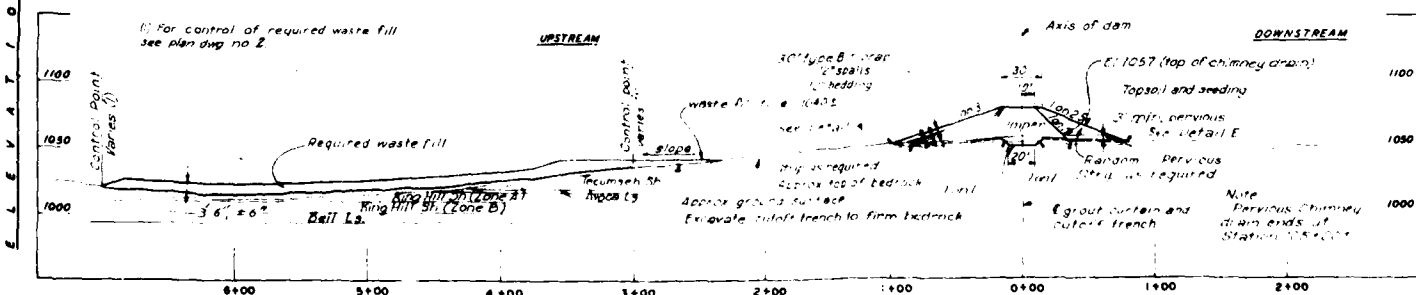
TYPICAL TERRACE SECTION-STA. 84+00 TO STA. 92+00±

SECTION AT STA. 90+00±



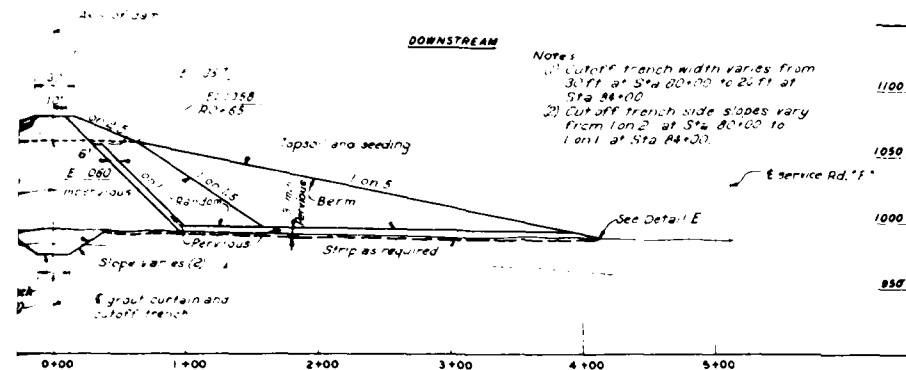
TYPICAL TERRACE SECTION-STA. 92+00± TO STA. 101+00±

SECTION AT STA. 97+00±



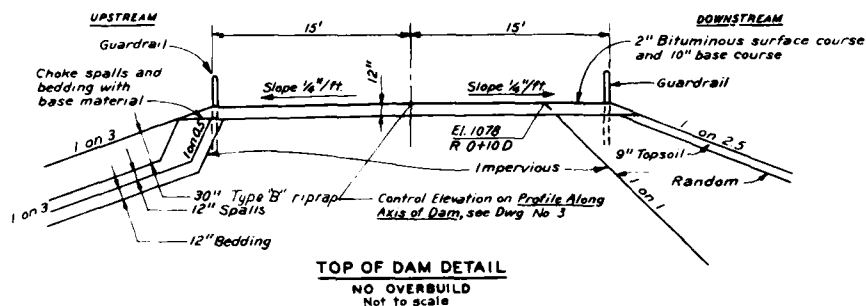
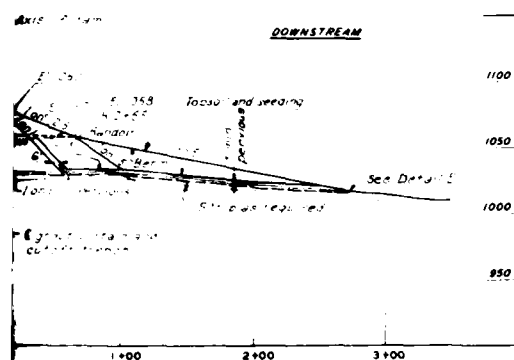
TYPICAL LEFT ABUTMENT SECTION-STA. 101+00± TO STA. 120+00

SECTION AT STA. 105+00±

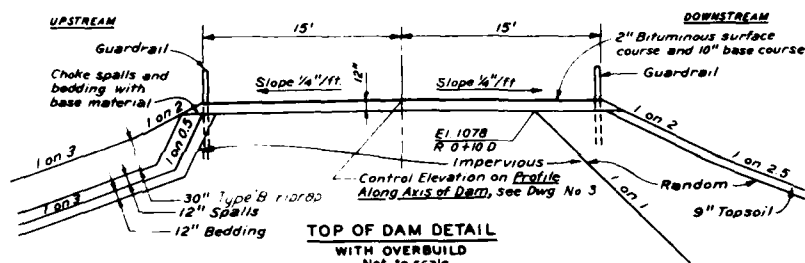
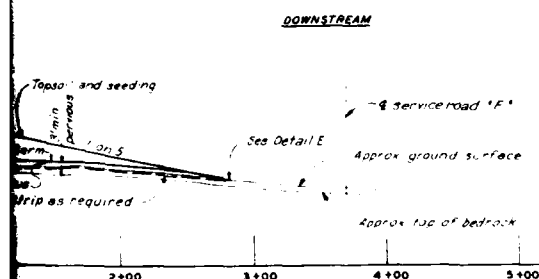


SCHEDULE OF GUARDRAIL For top of dam				
Station to Station	Side	Length	Remarks	
24+00 to 45+36±	Left	21625±		
45+64± to 110+00	Left	64625±		
24+00 to 110+00	Right	8600'		

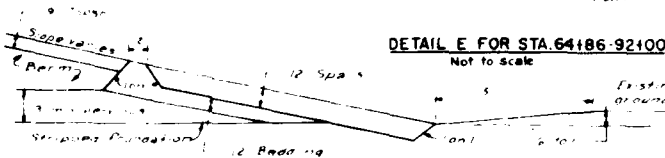
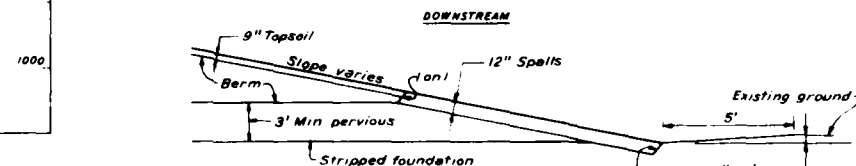
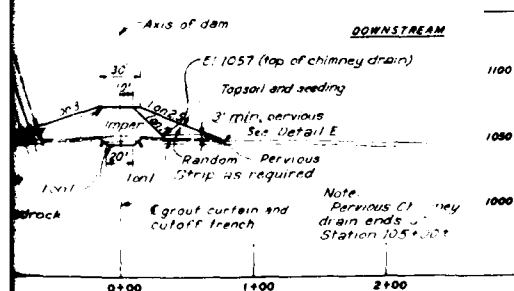
STA 80+00 TO STA 84+00
AT STA 82+00±



STA 80±



STA 101+00±



DETAIL F FOR STA 92+00 TO 105+50
STA 35+75 TO 44+00-47+00 TO 63+50

MARAS DES CYGNES RIVER, KANSAS
MELVERN LAKE
 EMBANKMENT CRITERIA AND PERFORMANCE REPORT

**EMBANKMENT SECTIONS
 TERRACE AND LEFT ABUTMENT**

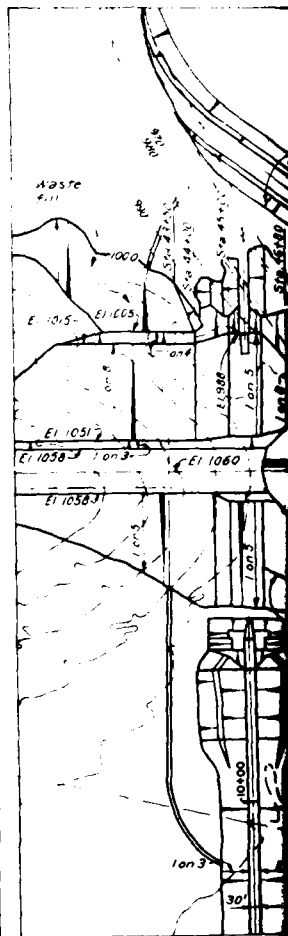
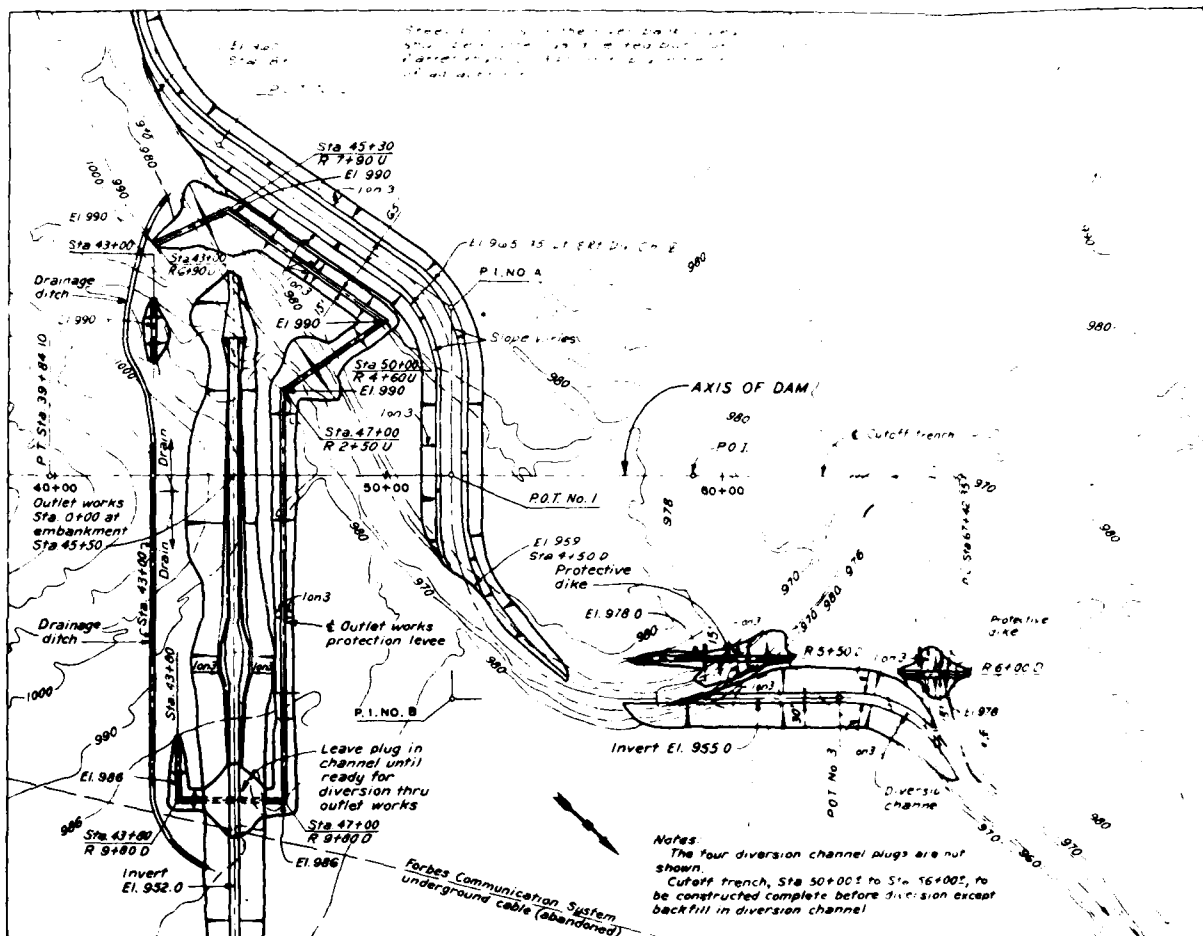
In 1 sheets

Sheet No 1

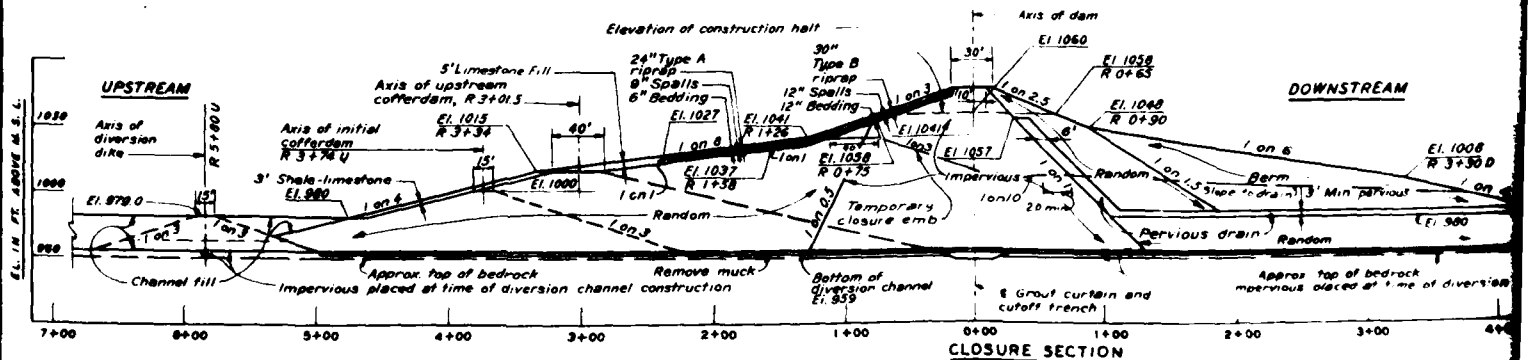
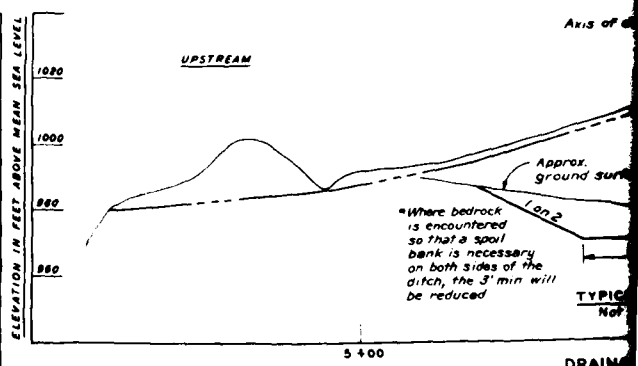
Scale as shown

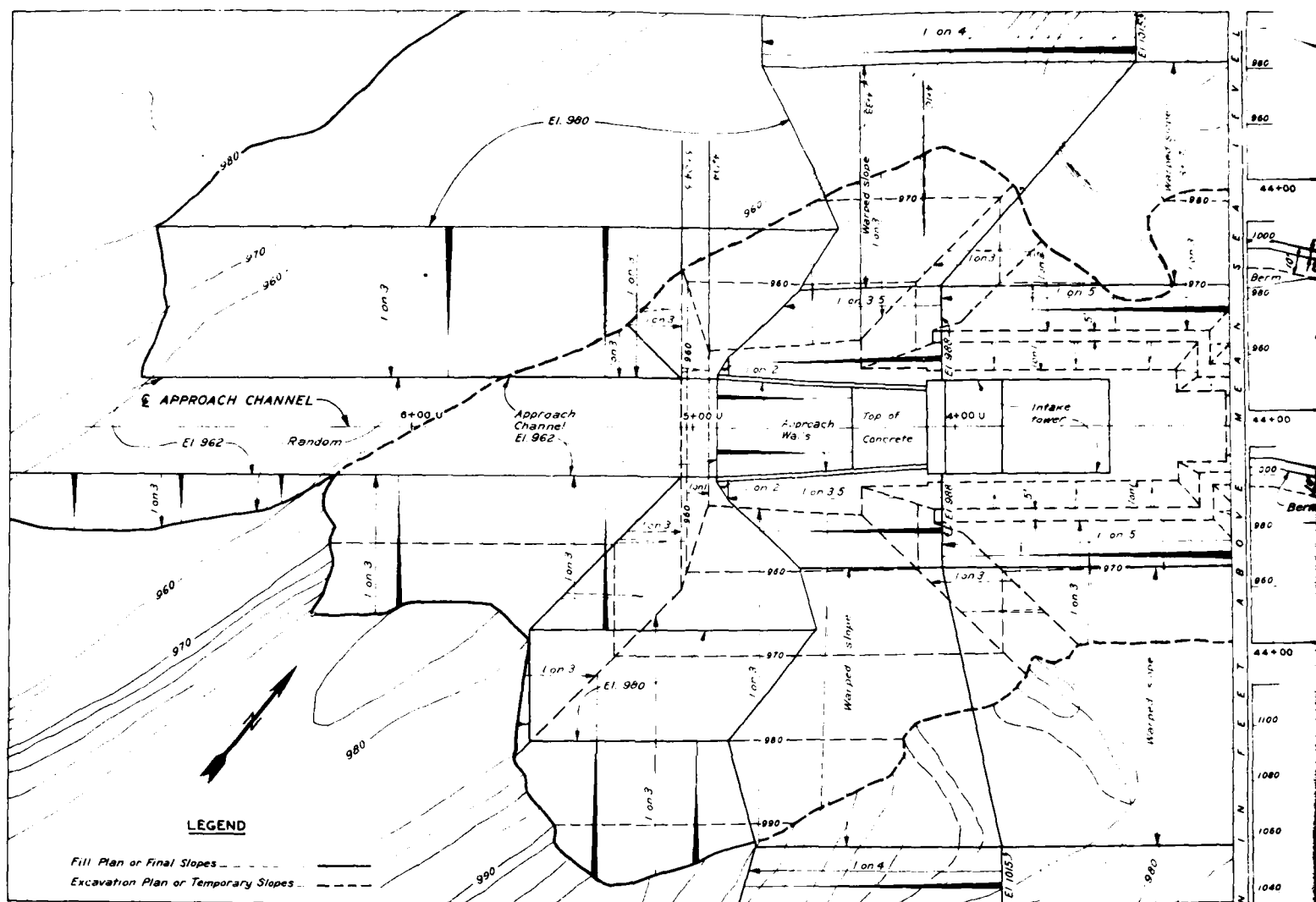
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 KANSAS CITY DISTRICT
 FILE NO 0-5-1346
 AUGUST 1978

PLATE NO. 6

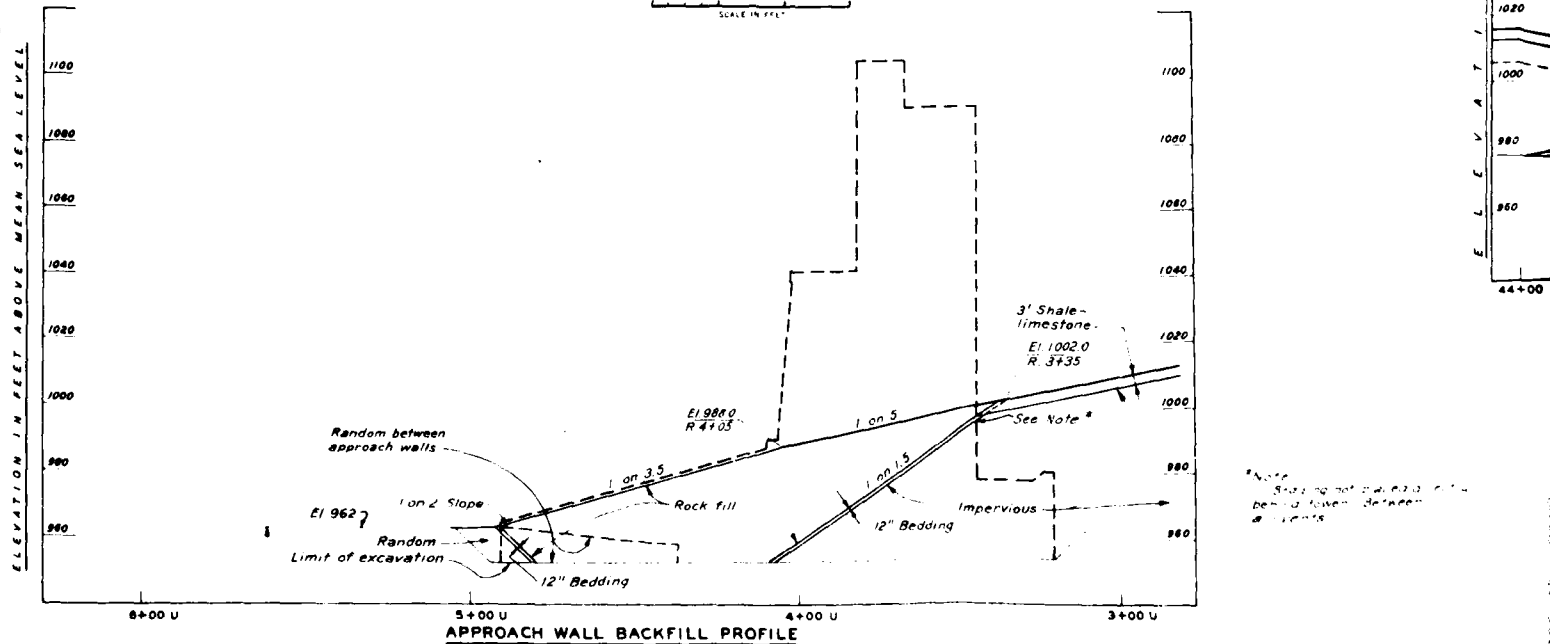


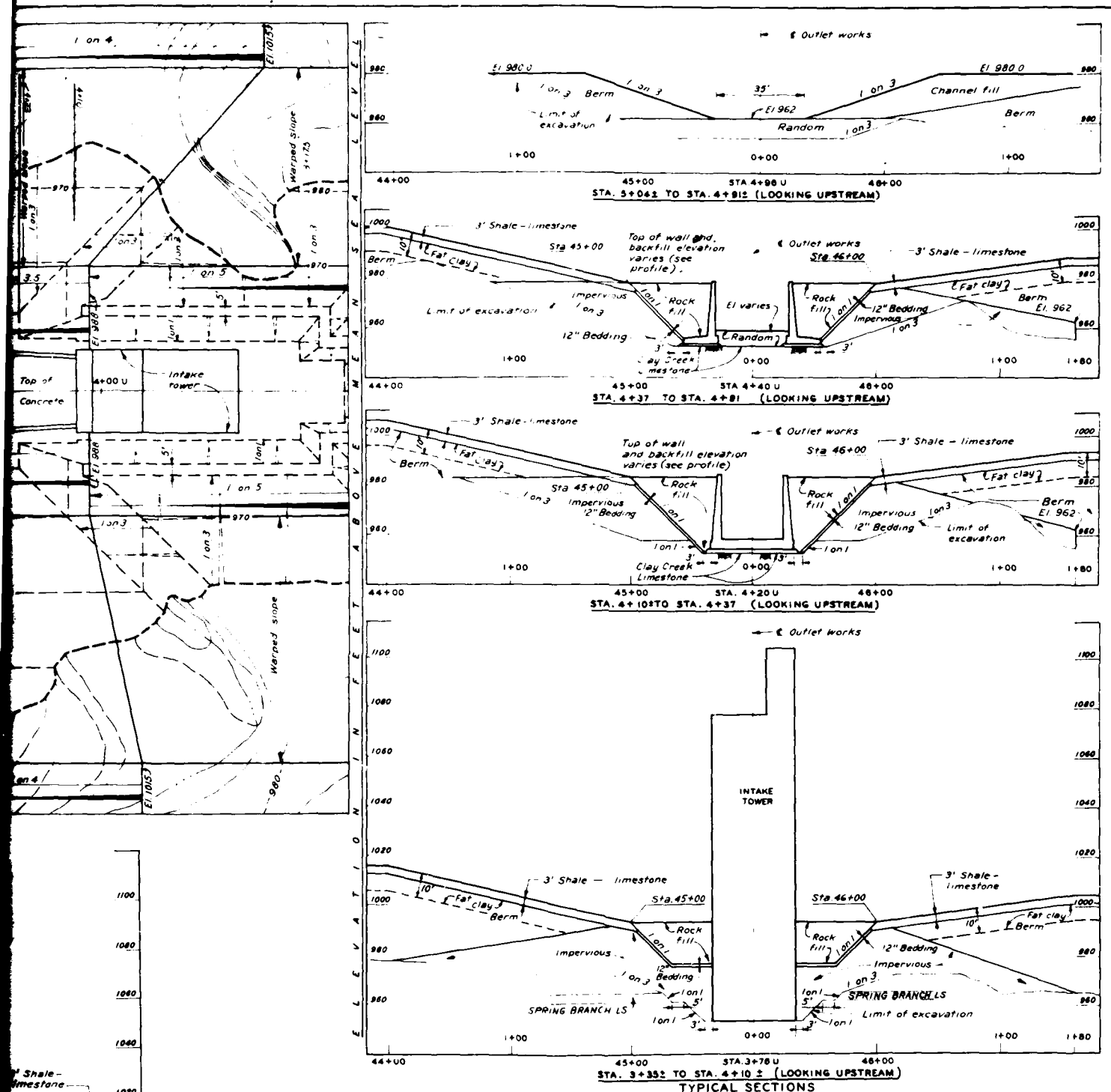
ALINEMENT DATA														
P. I.	LATITUDE	DEPARTURE	AZIMUTH	DISTANCE	STATION	P.C.	STATION	P.T.	STATION	Δ	D	T	R	L
(UPSTREAM DIVERSION)														
P.O.T. No. 1	68° 29' 56"	278.30	30.00		Dam Sta. 32+00 = Sta. 0+00 Diversion Channel									
P.O.T. No. 2	64° 21' 17"	278.81	30.00	37° 0' 0"	713.34		59+13.35	(Line P.O.T. No. 2 to P.I.A. intersects Dam Axis)						
P.O.T. No. 3	68° 29' 56"	278.30	30.00	47° 0' 0"	508.20									
A	68° 29' 56"	278.30	30.00	35° 05' 49"	833.00			3+12.37U	6+74.37U	34° 34' 11"	15° 10' 0"	196.83	378.84	362.00
P.O.T. No. 4	68° 29' 56"	278.30	30.00	26° 05' 49"	—		13+30.34U	(Swing to river)			7° 30' 0"		764.43	
(DOWNSTREAM DIVERSION)														
P.O.T. No. 1	68° 29' 56"	278.30	30.00		Dam Sta. 32+00 = Sta. 0+00 Diversion Channel									
B	68° 29' 56"	278.30	30.00	22° 0' 0"	673.00			1+12.77D	8+80.74D	90° 0' 0"	10° 20' 0"	555.23	555.23	870.07
P.O.T. No. 2	68° 29' 56"	278.30	30.00	13° 0' 0"	1778.00									
P.O.T. No. 3	68° 29' 56"	278.30	30.00	47° 0' 0"	—		16+03.30D	(Swing to river)			18° 30' 0"		458.28	





PLAN
SCALE IN FEET
0 20 40





*Note
Bedding not placed directly
behind tower. Between
air vents.

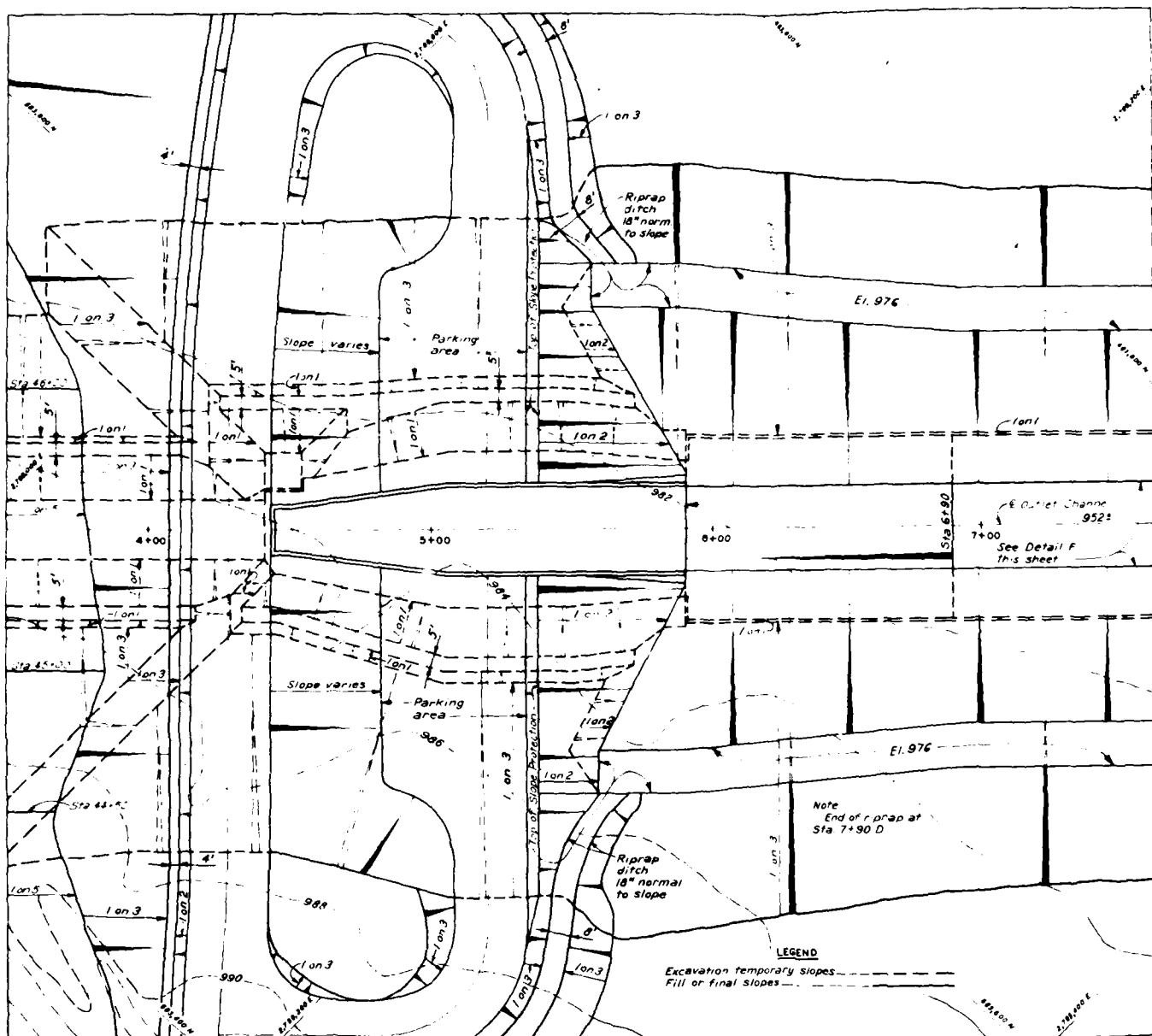
MARAI DES CYGNES RIVER, KANSAS
MELVERN LAKE
 EMBANKMENT CRITERIA AND PERFORMANCE REPORT
 EMBANKMENT TRANSITION DETAILS
 INTAKE TOWER AREA

In 1 sheet

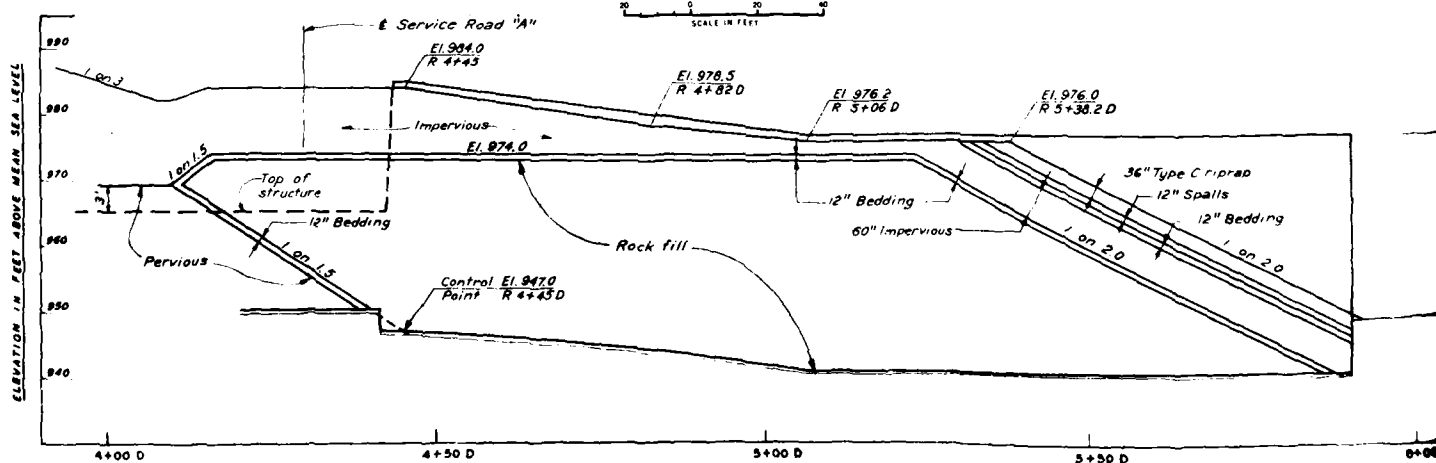
Sheet No. 1

Scale as shown

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 KANSAS CITY DISTRICT
 FILE NO. 0-5-1348
 AUGUST 1979

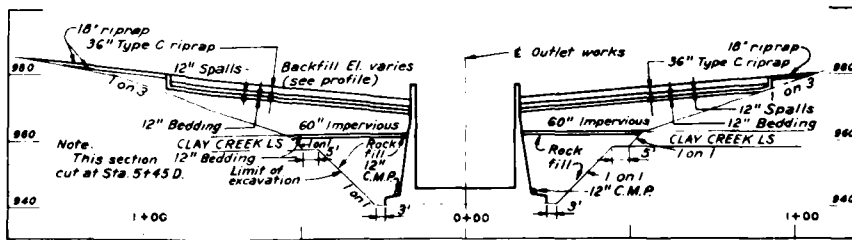
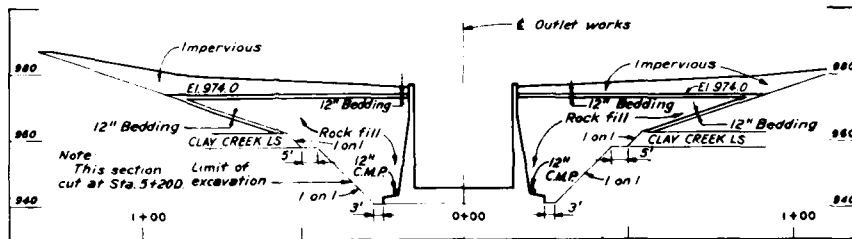
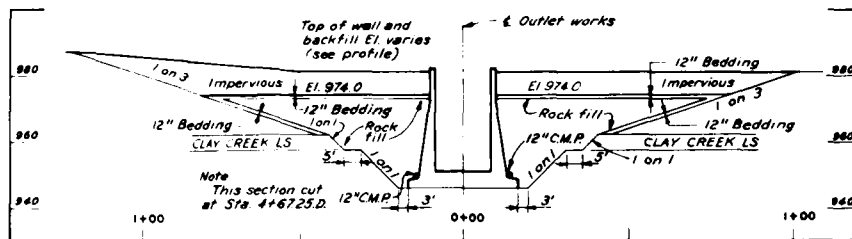
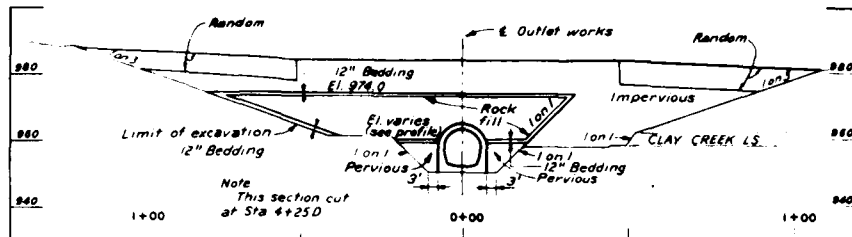


PLAN OF STILLING BASIN EXCAVATION

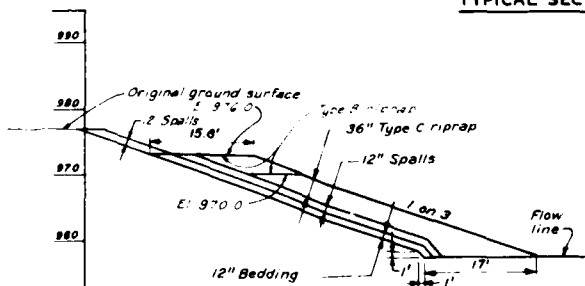
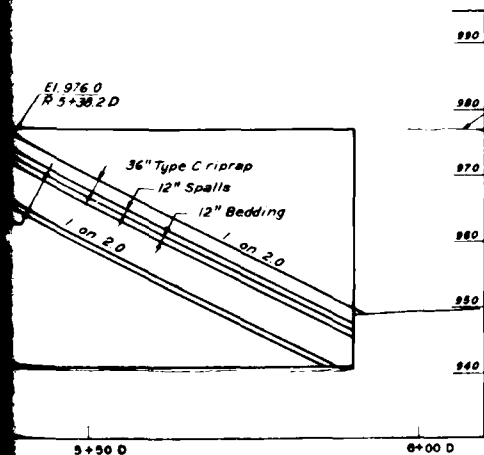
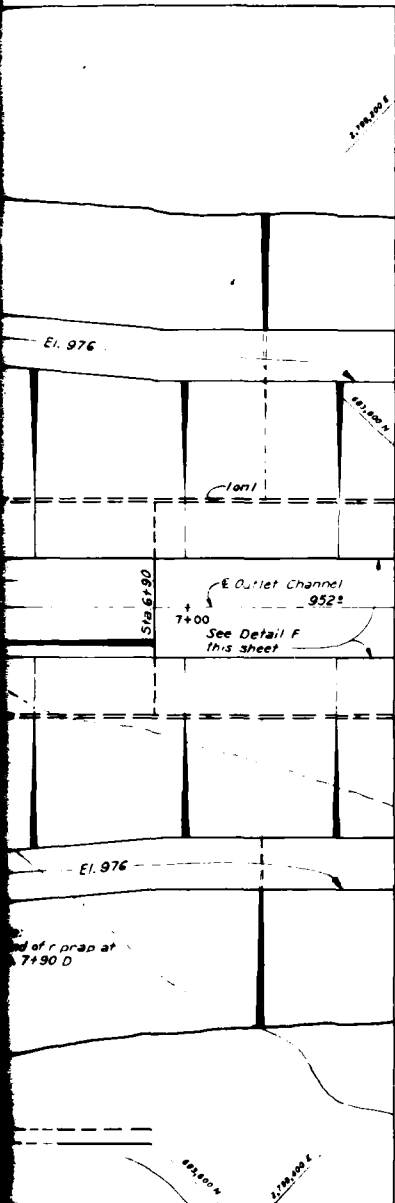


PROFILE SHOWING STILLING BASIN BACKFILL DETAILS

ELEVATION IN FEET ABOVE MEAN SEA LEVEL



TYPICAL SECTIONS



MARAS DES CYGNES RIVER, KANSAS
MELVERN LAKE
EMBANKMENT CRITERIA AND PERFORMANCE REPORT
EMBANKMENT TRANSITION DETAILS
STILLING BASIN AREA

In 1 sheet

Sheet No. 1
CORPS OF ENGINEERS U.S. ARMY
KANSAS CITY DISTRICT
FILE NO. 0-5-1349
AUGUST 1978

Scale as shown

PENNSYLVANIAN					GENERALIZED GEOLOGIC COLUMN					PENNSYLVANIAN					GENERALIZED GEOLOGIC COLUMN				
SYSTEM GROUP FORMATION	MEMBER	THICKNESS	SYMBOL	GENERAL DESCRIPTION	SYSTEM GROUP FORMATION	MEMBER	THICKNESS	SYMBOL	GENERAL DESCRIPTION	SYSTEM GROUP FORMATION	MEMBER	THICKNESS	SYMBOL	GENERAL DESCRIPTION	SYSTEM GROUP FORMATION	MEMBER	THICKNESS	SYMBOL	GENERAL DESCRIPTION
QUATERNARY	Recent Wisconsin & Pahrump	Recent	Recent	Recent	QUATERNARY	Recent Wisconsin & Pahrump	Recent	Recent	Recent	QUATERNARY	Recent Wisconsin & Pahrump	Recent	Recent	Recent	QUATERNARY	Recent Wisconsin & Pahrump	Recent	Recent	Recent
PENNSYLVANIAN	SHANNEE	DEER CREEK	Larch Branch	10' to 15'	PENNSYLVANIAN	SHANNEE	DEER CREEK	Larch Branch	10' to 15'	PENNSYLVANIAN	SHANNEE	DEER CREEK	Larch Branch	10' to 15'	PENNSYLVANIAN	SHANNEE	DEER CREEK	Larch Branch	10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
PENNSYLVANIAN	SHANNEE	DEER CREEK	Larch Branch	10' to 15'	PENNSYLVANIAN	SHANNEE	DEER CREEK	Larch Branch	10' to 15'	PENNSYLVANIAN	SHANNEE	DEER CREEK	Larch Branch	10' to 15'	PENNSYLVANIAN	SHANNEE	DEER CREEK	Larch Branch	10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
				10' to 15'					10' to 15'					10' to 15'					10' to 15'
				10' to 15'															

LEGEND: 1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12. 13. 14. 15. 16. 17. 18. 19. 20. 21. 22. 23. 24. 25. 26. 27. 28. 29. 30. 31. 32. 33. 34. 35. 36. 37. 38. 39. 40. 41. 42. 43. 44. 45. 46. 47. 48. 49. 50. 51. 52. 53. 54. 55. 56. 57. 58. 59. 60. 61. 62. 63. 64. 65. 66. 67. 68. 69. 70. 71. 72. 73. 74. 75. 76. 77. 78. 79. 80. 81. 82. 83. 84. 85. 86. 87. 88. 89. 90. 91. 92. 93. 94. 95. 96. 97. 98. 99. 100. 101. 102. 103. 104. 105. 106. 107. 108. 109. 110. 111. 112. 113. 114. 115. 116. 117. 118. 119. 120. 121. 122. 123. 124. 125. 126. 127. 128. 129. 130. 131. 132. 133. 134. 135. 136. 137. 138. 139. 140. 141. 142. 143. 144. 145. 146. 147. 148. 149. 150. 151. 152. 153. 154. 155. 156. 157. 158. 159. 160. 161. 162. 163. 164. 165. 166. 167. 168. 169. 170. 171. 172. 173. 174. 175. 176. 177. 178. 179. 180. 181. 182. 183. 184. 185. 186. 187. 188. 189. 190. 191. 192. 193. 194. 195. 196. 197. 198. 199. 200. 201. 202. 203. 204. 205. 206. 207. 208. 209. 210. 211. 212. 213. 214. 215. 216. 217. 218. 219. 220. 221. 222. 223. 224. 225. 226. 227. 228. 229. 230. 231. 232. 233. 234. 235. 236. 237. 238. 239. 240. 241. 242. 243. 244. 245. 246. 247. 248. 249. 250. 251. 252. 253. 254. 255. 256. 257. 258. 259. 260. 261. 262. 263. 264. 265. 266. 267. 268. 269. 270. 271. 272. 273. 274. 275. 276. 277. 278. 279. 280. 281. 282. 283. 284. 285. 286. 287. 288. 289. 290. 291. 292. 293. 294. 295. 296. 297. 298. 299. 300. 301. 302. 303. 304. 305. 306. 307. 308. 309. 310. 311. 312. 313. 314. 315. 316. 317. 318. 319. 320. 321. 322. 323. 324. 325. 326. 327. 328. 329. 330. 331. 332. 333. 334. 335. 336. 337. 338. 339. 340. 341. 342. 343. 344. 345. 346. 347. 348. 349. 350. 351. 352. 353. 354. 355. 356. 357. 358. 359. 360. 361. 362. 363. 364. 365. 366. 367. 368. 369. 370. 371. 372. 373. 374. 375. 376. 377. 378. 379. 380. 381. 382. 383. 384. 385. 386. 387. 388. 389. 390. 391. 392. 393. 394. 395. 396. 397. 398. 399. 400. 401. 402. 403. 404. 405. 406. 407. 408. 409. 410. 411. 412. 413. 414. 415. 416. 417. 418. 419. 420. 421. 422. 423. 424. 425. 426. 427. 428. 429. 430. 431. 432. 433. 434. 435. 436. 437. 438. 439. 440. 441. 442. 443. 444. 445. 446. 447. 448. 449. 450. 451. 452. 453. 454. 455. 456. 457. 458. 459. 460. 461. 462. 463. 464. 465. 466. 467. 468. 469. 470. 471. 472. 473. 474. 475. 476. 477. 478. 479. 480. 481. 482. 483. 484. 485. 486. 487. 488. 489. 490. 491. 492. 493. 494. 495. 496. 497. 498. 499. 500. 501. 502. 503. 504. 505. 506. 507. 508. 509. 510. 511. 512. 513. 514. 515. 516. 517. 518. 519. 520. 521. 522. 523. 524. 525. 526. 527. 528. 529. 530. 531. 532. 533. 534. 535. 536. 537. 538. 539. 540. 541. 542. 543. 544. 545. 546. 547. 548. 549. 550. 551. 552. 553. 554. 555. 556. 557. 558. 559. 560. 561. 562. 563. 564. 565. 566. 567. 568. 569. 570. 571. 572. 573. 574. 575. 576. 577. 578. 579. 580. 581. 582. 583. 584. 585. 586. 587. 588. 589. 590. 591. 592. 593. 594. 595. 596. 597. 598. 599. 600. 601. 602. 603. 604. 605. 606. 607. 608. 609. 610. 611. 612. 613. 614. 615. 616. 617. 618. 619. 620. 621. 622. 623. 624. 625. 626. 627. 628. 629. 630. 631. 632. 633. 634. 635. 636. 637. 638. 639. 640. 641. 642. 643. 644. 645. 646. 647. 648. 649. 650. 651. 652. 653. 654. 655. 656. 657. 658. 659. 660. 661. 662. 663. 664. 665. 666. 667. 668. 669. 670. 671. 672. 673. 674. 675. 676. 677. 678. 679. 680. 681. 682. 683. 684. 685. 686. 687. 688. 689. 690. 691. 692. 693. 694. 695. 696. 697. 698. 699. 700. 701. 702. 703. 704. 705. 706. 707. 708. 709. 710. 711. 712. 713. 714. 715. 716. 717. 718. 719. 720. 721. 722. 723. 724. 725. 726. 727. 728. 729. 730. 731. 732. 733. 734. 735. 736. 737. 738. 739. 740. 741. 742. 743. 744. 745. 746. 747. 748. 749. 750. 751. 752. 753. 754. 755. 756. 757. 758. 759. 760. 761. 762. 763. 764. 765. 766. 767. 768. 769. 770. 771. 772. 773. 774. 775. 776. 777. 778. 779. 780. 781. 782. 783. 784. 785. 786. 787. 788. 789. 790. 791. 792. 793. 794. 795. 796. 797. 798. 799. 800. 801. 802. 803. 804. 805. 806. 807. 808. 809. 810. 811. 812. 813. 814. 815. 816. 817. 818. 819. 820. 821. 822. 823. 824. 825. 826. 827. 828. 829. 830. 831. 832. 833. 834. 835. 836. 837. 838. 839. 840

- Plasticity index
- Liquid limit
- Effective size mm, maximum diameter
- Flow number
- Offset for Station and Range
- vertical: Angle and Direction
- Moisture content: percent
- Dry density: pounds per cubic foot
- Unconfined compressive strength

Elevation and date water level observed _____

Unified soil classification determined in lab _____

Field classification (dry) _____

No Sample _____

No Recovery (overburden) _____

Per cent lost drill water _____

Lost core (bedrock) _____

Depth of hole _____

Per cent core recovered (bedrock) _____

Drilling complete - date _____

Diameter of sample _____

*Notes from profile or section may be included in this section.

*Borehole should be 5 ft. or Right Angle

1988 年 12 月 15 日

- | | | | |
|-----------|---|---|---|
| GW | Well graded gravel with sand | Well graded gravel with sand | Well graded gravel with sand |
| GP | Poorly graded gravel with sand | Poorly graded gravel with sand | Poorly graded gravel with sand |
| GM | Silty gravel with sand | Silty gravel with sand | Silty gravel with sand |
| GC | Clayey gravel with sand | Clayey gravel with sand | Clayey gravel with sand |
| SW | Well graded sands with little or no fines | Well graded sands with little or no fines | Well graded sands with little or no fines |
| SP | Poorly graded sands with little or no fines | Poorly graded sands with little or no fines | Poorly graded sands with little or no fines |
| SM | Silty sands | Silty sands | Silty sands |
| SC | Clayey sands | Clayey sands | Clayey sands |

Classification from actual laboratory tests where μ and P are not available.
Dual classification, where used, is in accordance with the Unified Soil Classification System.
For details on the Unified Soil Classification System, See Waterways Experiment Station, Technical Memorandum No. 3-357, dated March 1945, and revised.

• -REVIAI

- [illegible]

BORINGS WITH PZ NUMBER DESIGNATION HAVE PIEZOMETERS 1

LEGEND FOR LOSS OF BORINGS

Elevation and date water first observed	W	SP
Unified soil classification determined in laboratory	10 160	ML
Field Classification Only		FC
No Sample		NS
No Recovery (overburden)		NR
Per cent lost (drill water)	L D W	LS
Lost core (bedrock)	L C B	LS
Depth of hole		100'0"
Per cent core recovered in bedrock		95.5%
Drilling completion date		10 6 60
Diameter of sample		4" test 2 1/2" test

*Offset from profile or section may be Upstream or Downstream (L or R) or Landward or Riverward (L or R) or Right or Left as defined.

UNIFIED SOIL CLASSIFICATION SYSTEM

SW	Well graded gravels, gravel sand mixtures, little or no fines	MC	Inorganic silts and very fine sands
SP	Poorly graded gravels, gravel sand mixtures, little or no fines	ML	Inorganic silts or clayey silts
GM	Silty gravels, gravel sand/silt mixtures	CL	Inorganic clays of low to medium plasticity, gravels, chalk, sand/silt clays, silts, sand/silt clays
GC	Clayey gravels, gravel sand/silt mixtures	CH	Organic silts and organic silts of low plasticity
SW	Well-graded sands, gravelly sands, little or no fines	MH	Inorganic silts, macaceous or fatclayey silts, sandy or silty soils, elastic silts
SP	Poorly graded sands or gravelly sands, little or no fines	CH	Inorganic clays of high plasticity, fat clays
SM	Silty sands, sand/silt mixtures	OL	Organic clays of medium to high plasticity, organic silts
SC	Clayey sands, sand/clay mixtures	PH	Peat and other highly organic soils

Classification from actual laboratory tests where α_L and P_L are shown.
Dual classification, where used, is in accordance with the Unified Soil Classification System.
For details on the Unified Soil Classification System, See Waterways Experiment Station Technical Memorandum No. 3357 dated March 1953 and revised in 1960.

ABSTRACT

alt	alternating	dol	dolomite, dolomitic	lea	learned	st	staircase
ang	angular	ext	extreme	lig	lignite	st	staircase
an	anhydrite	fl	fine, line y	is	isostone	st	staircase
ar	argillaceous	fe	iron	is	isostone	st	staircase
abd	bed bedded bedding	hd	headed	is	isostone	st	staircase
bdr	bedrock	hm	firm	is	isostone	st	staircase
bhy	blocky	fos	fossil, fossiliferous	LDW	lost drill water	st	staircase
bl	blue	frac	fractures, fractured	med	medium	st	staircase
bid	boulder	frag	fragments, fragmented	mc	micaceous	st	staircase
blc	black	fr	fracture	min	mineralized	st	staircase
brec	breccia brecciated	fss	fissile	mod	moderate, moderately	sol	solution solution
brn	brown	gr	grain	mot	mottled	st	sandstone
co	coarse	gre	green	mss	massive	st	staircase
calc	calcareous	grm	gravel	most	most	st	staircase
carb	carbonaceous	grv	gravel, gravely	mtl	material	st	staircase
cav	cavity	gr	gray	mtz	matrix	st	staircase
cbl	cobble	gsp	gypsum	nod	nodules	vert	vertical
cht	chest	h	high angle	num	numerous	st	staircase
chcl	circulation	hd	hard	occ	occasionally, occasional	st	staircase
clp	clay, clayey	hd	heated	op	open	st	staircase
cmid	cemented	hor	horizontal	org	organic	st	staircase
col	col	int	interbedded	pit	pit, pitted pitting	st	staircase
con	concretions	inc	inclusions	pl	plastic	st	staircase
cong	conglomerate	inlm	interlaminate	pla	plate	st	staircase
crn	crumbly	ir	irregular	ph	plane	st	staircase
d	dense	j	joints, joints	ptg	perting, perlings	st	staircase
dk	dark	la	low angle	qtz	quartzite quartz	st	staircase
dmp	damp	lsm	laminated, laminar	rnd	rounded	st	staircase

When used as log symbol
log letter is capitalized

TVDS 2000: $\pm 1.0^\circ$, $\pm 0.4^\circ$, $\pm 0.1^\circ$.

CODE DESIGNATION

- 1) Drive sampler
- 2) Core bar
- 3) Test bit (usually 100 mm dia & 254 mm in length)
- 4) Undisturbed soil core
- A) Agger hole (hand driven) - agger less than 254 mm dia
- B) 5' Analed or rock bit

MAP SYMBOL

- Vertical boring
- Inclined boring showing direction and vertical angle

BEFORE THE UNITED STATES SENATE

Parting	Angle
Blank	0°
Thin Bed	10°
Medium Bed	20°
Thick Bed	30°
Massive	45°

TERMS FOR CONSISTENCY OF
SOIL AND HARDNESS OF BEDROCKSu: 1

Consistency	Estimated Undrained Compressive Strength 1003 per square foot
Very soft	< 0.25
Soft	0.25-0.5
Medium	0.5-1.0
Stiff	1.0-2.0
Very stiff	2.0-4.0
Hard	> 4.0

BEDROCK

SCALE OF HARDNESS

Very soft or plastic	Can be indented easily -
Soft	Can be scratched with -
Moderately hard	Can be scratched easily -
	cannot be scratched with -
Hard	Difficult to scratch with -
Very Hard	Cannot be scratched with -

BORINGS WITH PZ NUMBER DESIGNATION HAVE PIEZOMETERS INSTALLED IN THEM

MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE
EMBANKMENT CRITERIA AND PERFORMANCE REPORT

GENERALIZED GEOLOGIC COLUMN AND LEGEND

In 1 sheet

Sheet No. 1

Scale: as shown

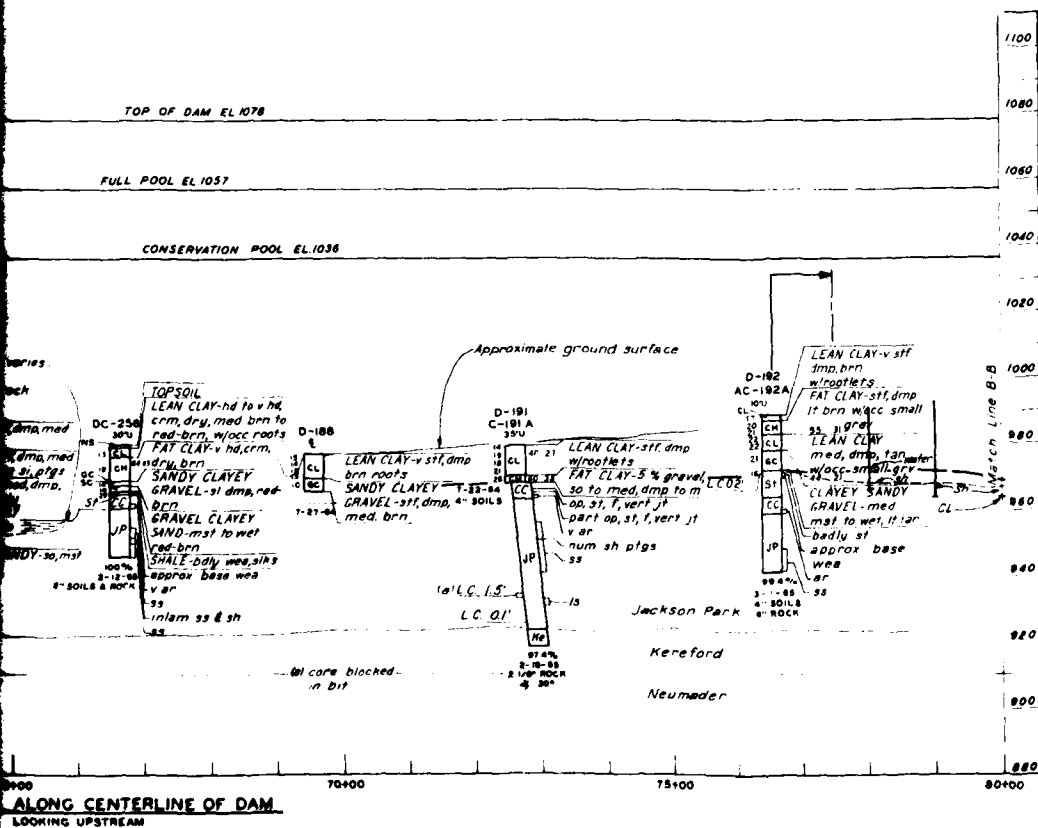
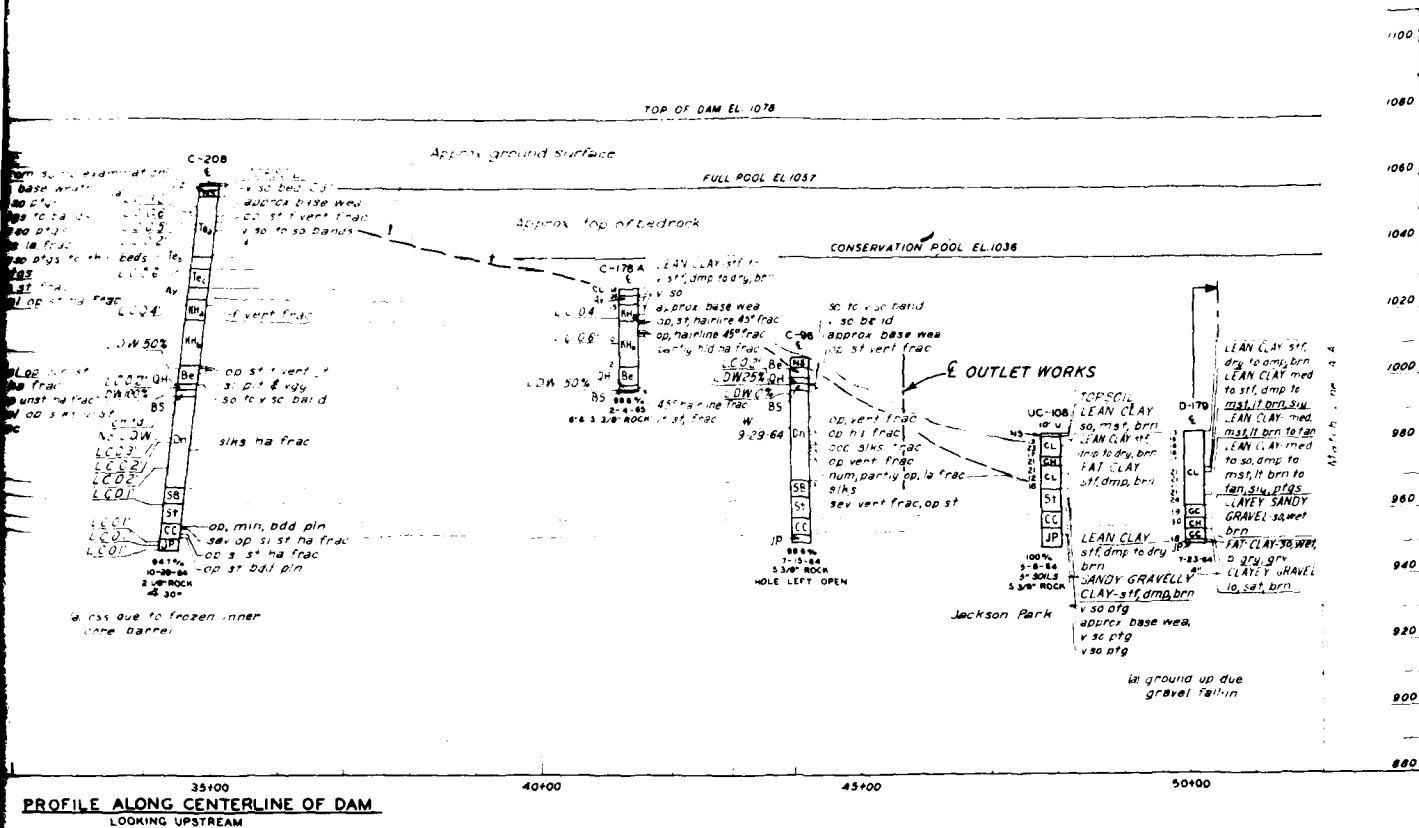
CORPS OF ENGINEERS U S ARMY

KANSAS CITY DISTRICT

FILE NO. 0-5-1350

AUGUST 1973

PLATE NO. 10



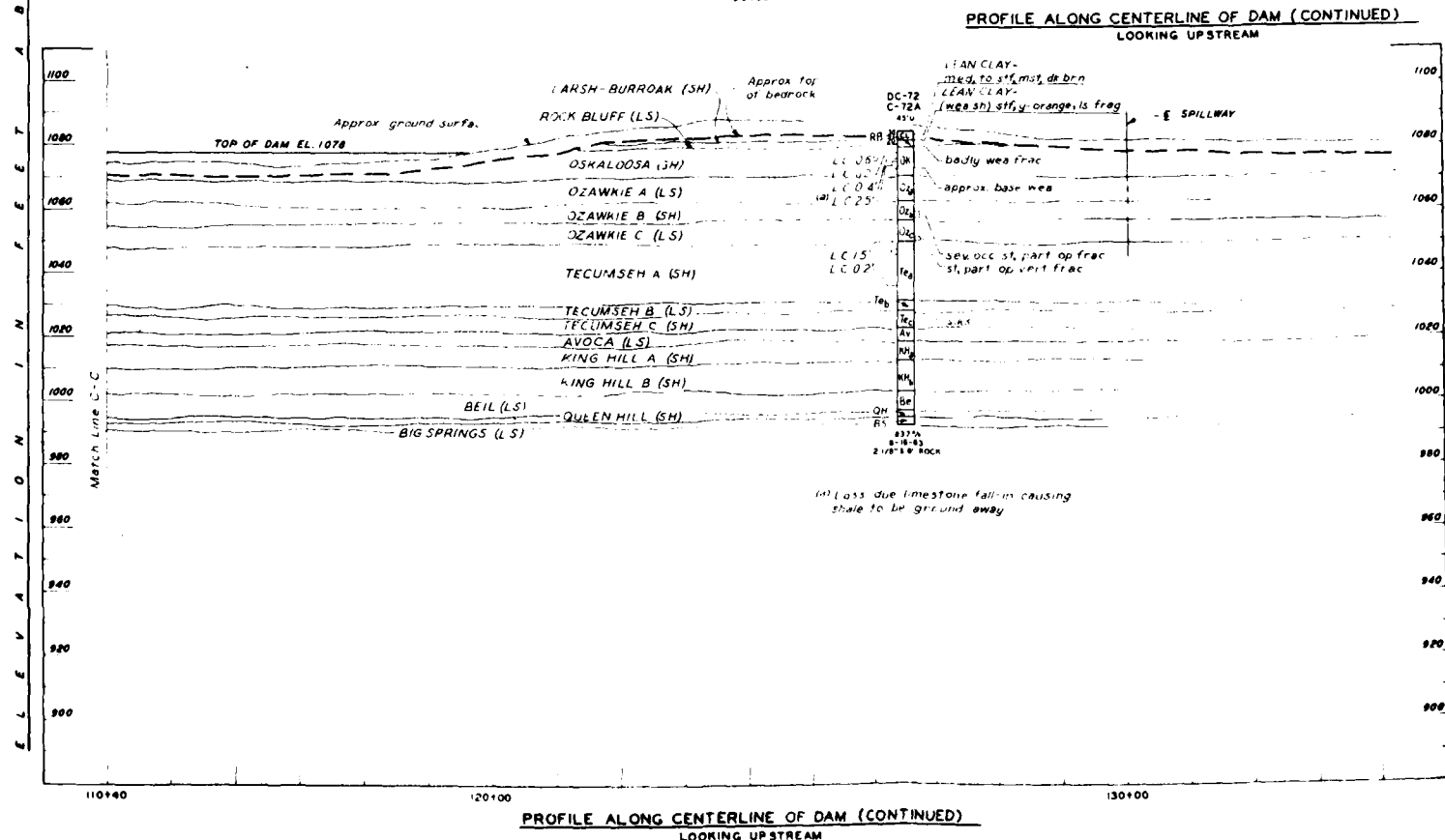
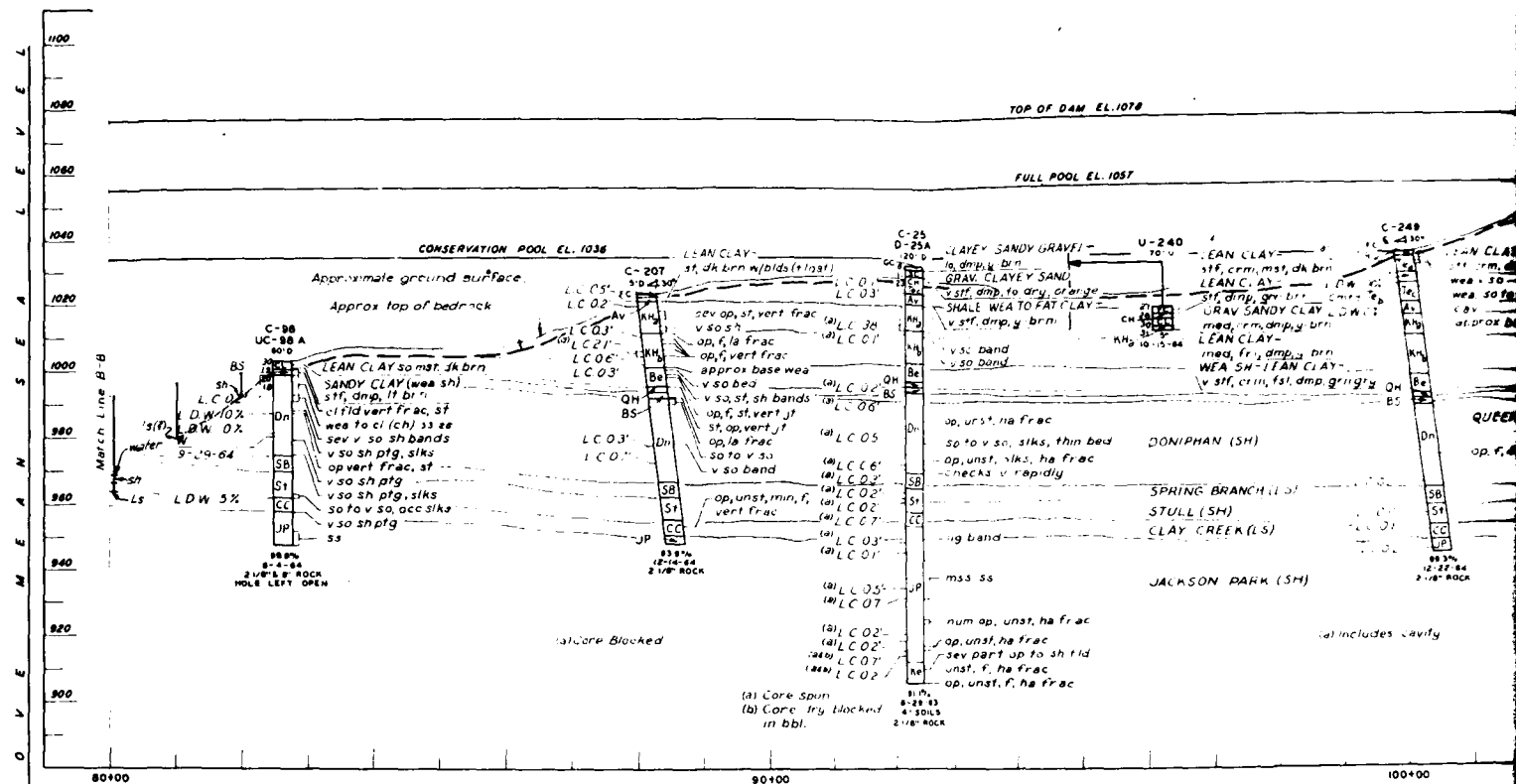
NOTES
 For legend and geologic column
 see Dwg. No. 10
 For excavation detail see Dwg. No. 7
 For grading detail see Dwg. No. 13
 Water levels shown where available

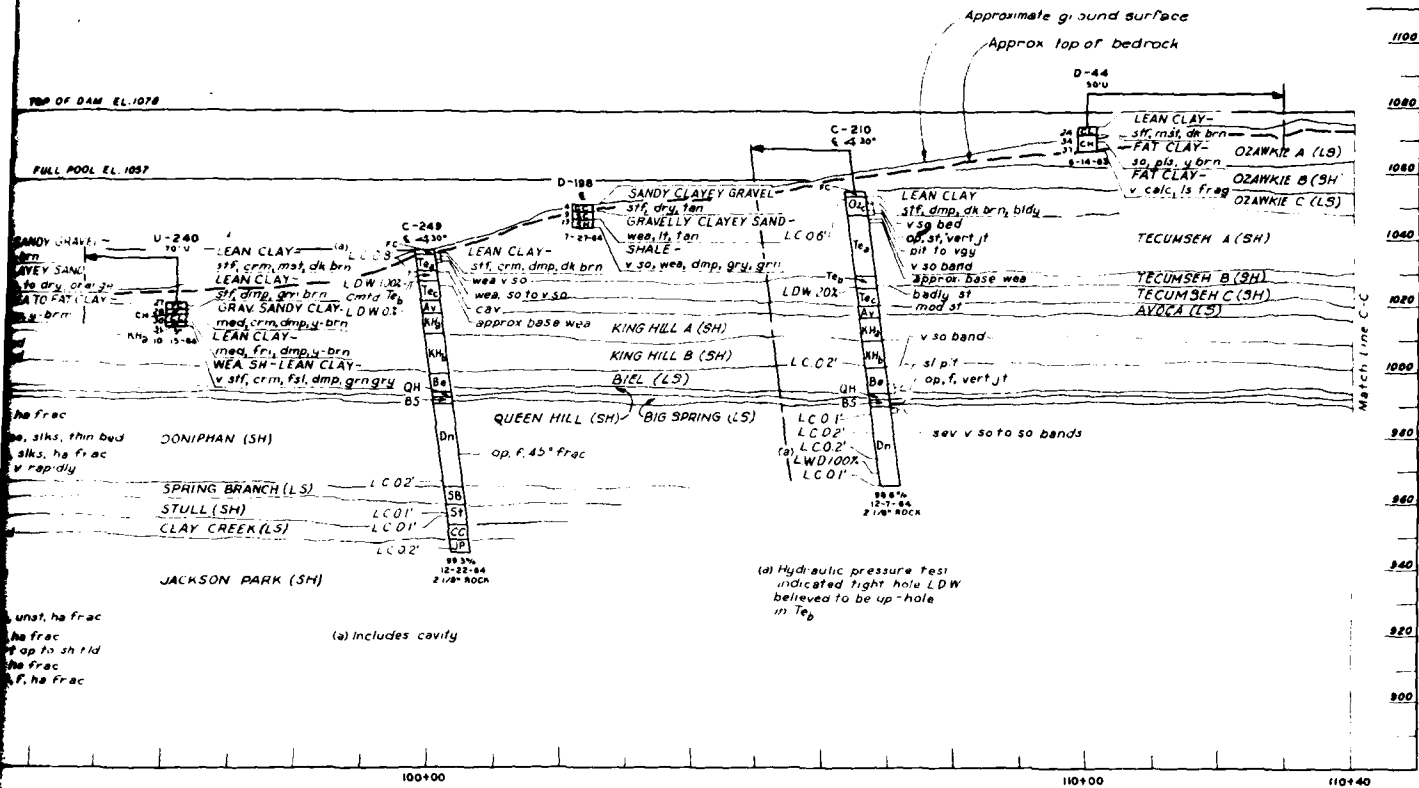
MARAI DES CYGNES RIVER, KANSAS
MELVERN LAKE
 EMBANKMENT CRITERIA AND PERFORMANCE REPORT

LOGS OF EXPLORATIONS
 AXIS OF DAM

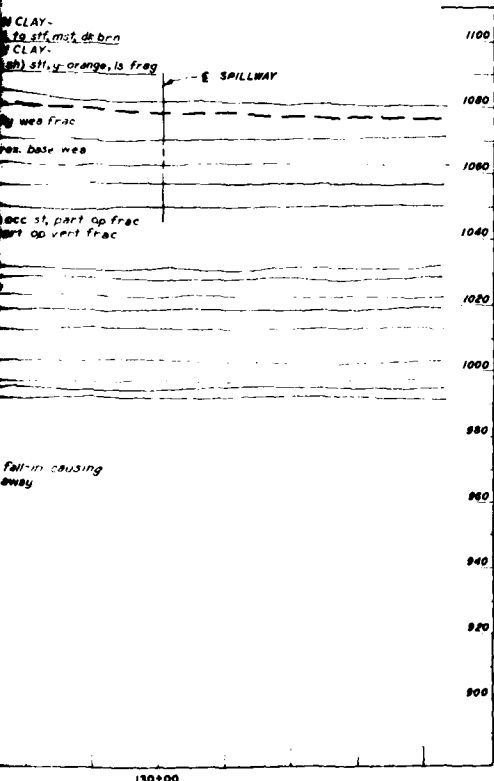
Sheet No. 1
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 KANSAS CITY DISTRICT
 FILE NO. O-5-1351
 AUGUST 1979

Scale as shown





PROFILE ALONG CENTERLINE OF DAM (CONTINUED)
LOOKING UPSTREAM



NOTES:

For geologic column and legend see Dwg. No. 10.
For excavation detail see Dwg. No. 3.
For grouting detail see Dwg. No. 13.
Water levels shown where available.

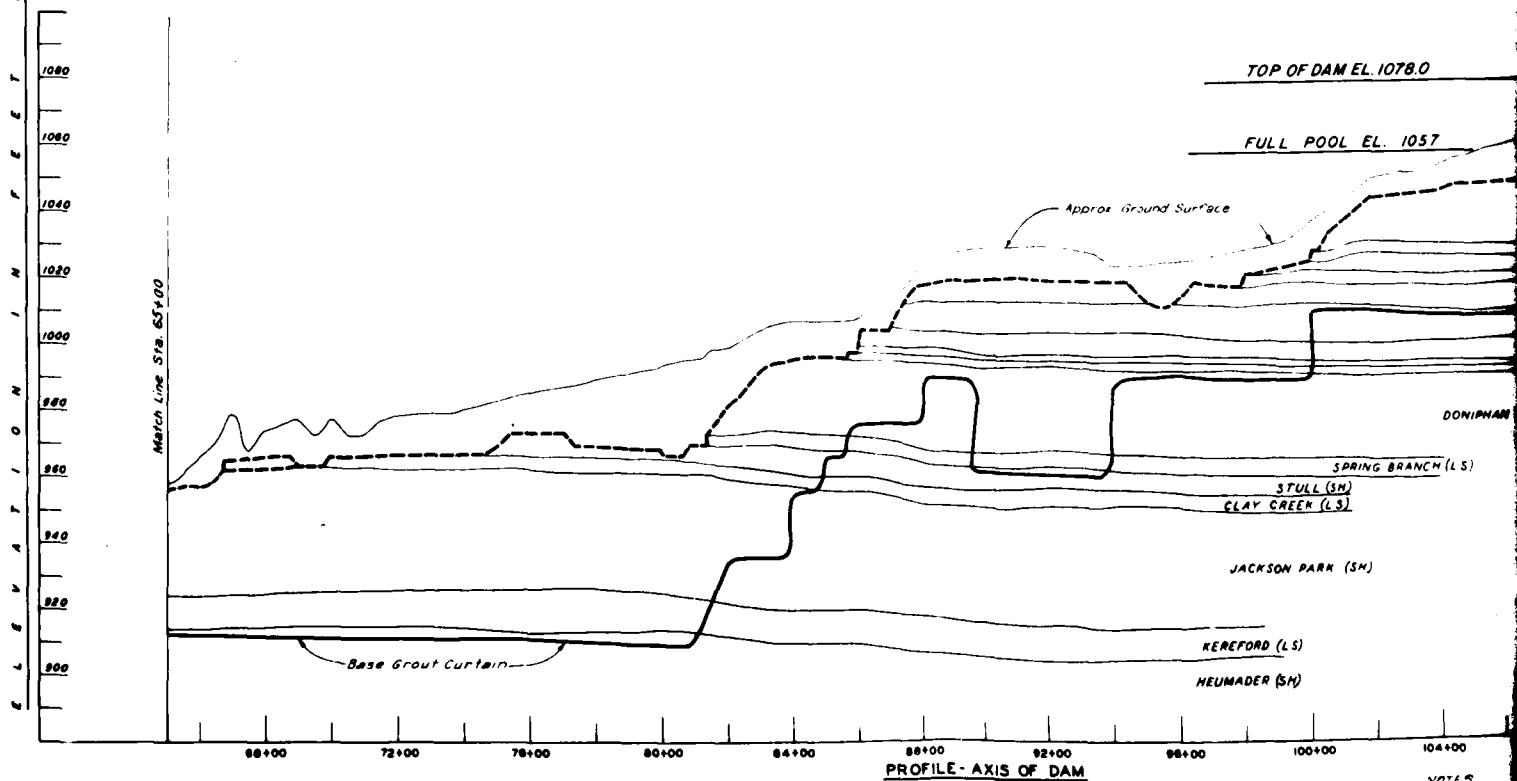
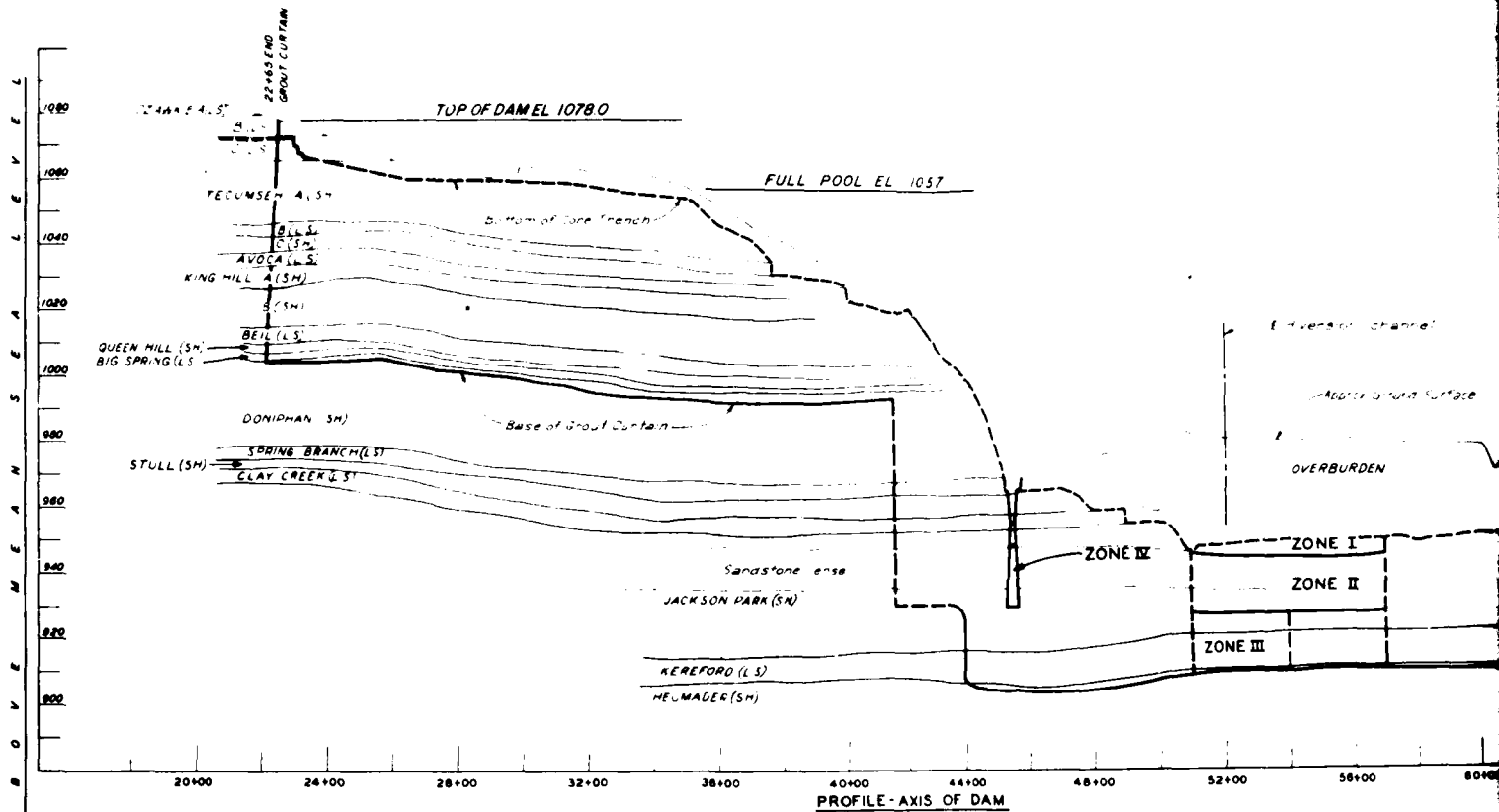
MARAS DES CYGNES RIVER, KANSAS
MELVERN LAKE
EMBANKMENT CRITERIA AND PERFORMANCE REPORT

LOGS OF EXPLORATIONS
AXIS OF DAM

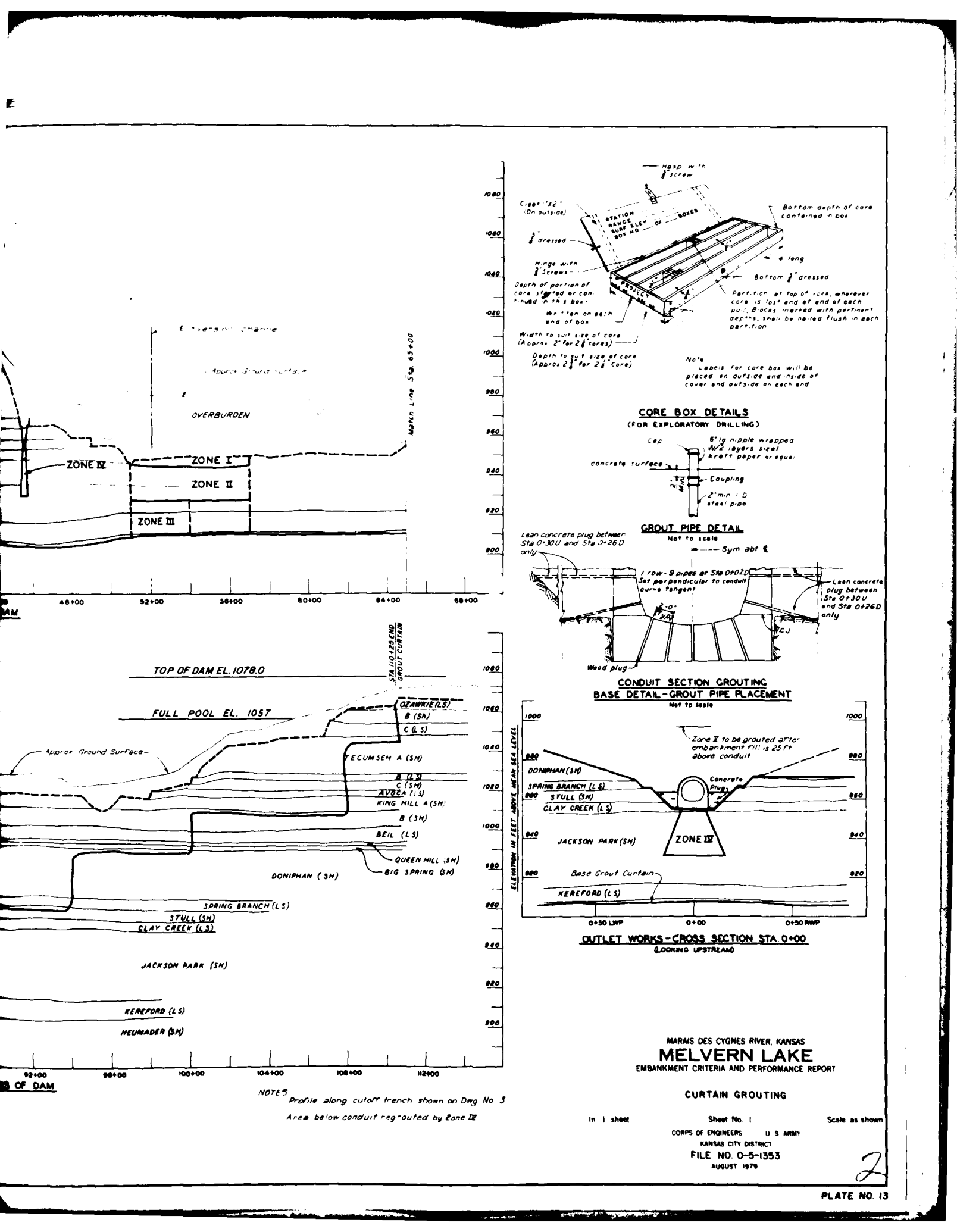
In 1 sheet

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KANSAS CITY DISTRICT
FILE NO. 0-5-1352
AUGUST 1979

Scale as shown



NOTES
Prof.
Area



NOTES
Profile along cutoff trench shown on Dwg. No. 3
Area below conduit regouted by Zone IX

In 1 sheet

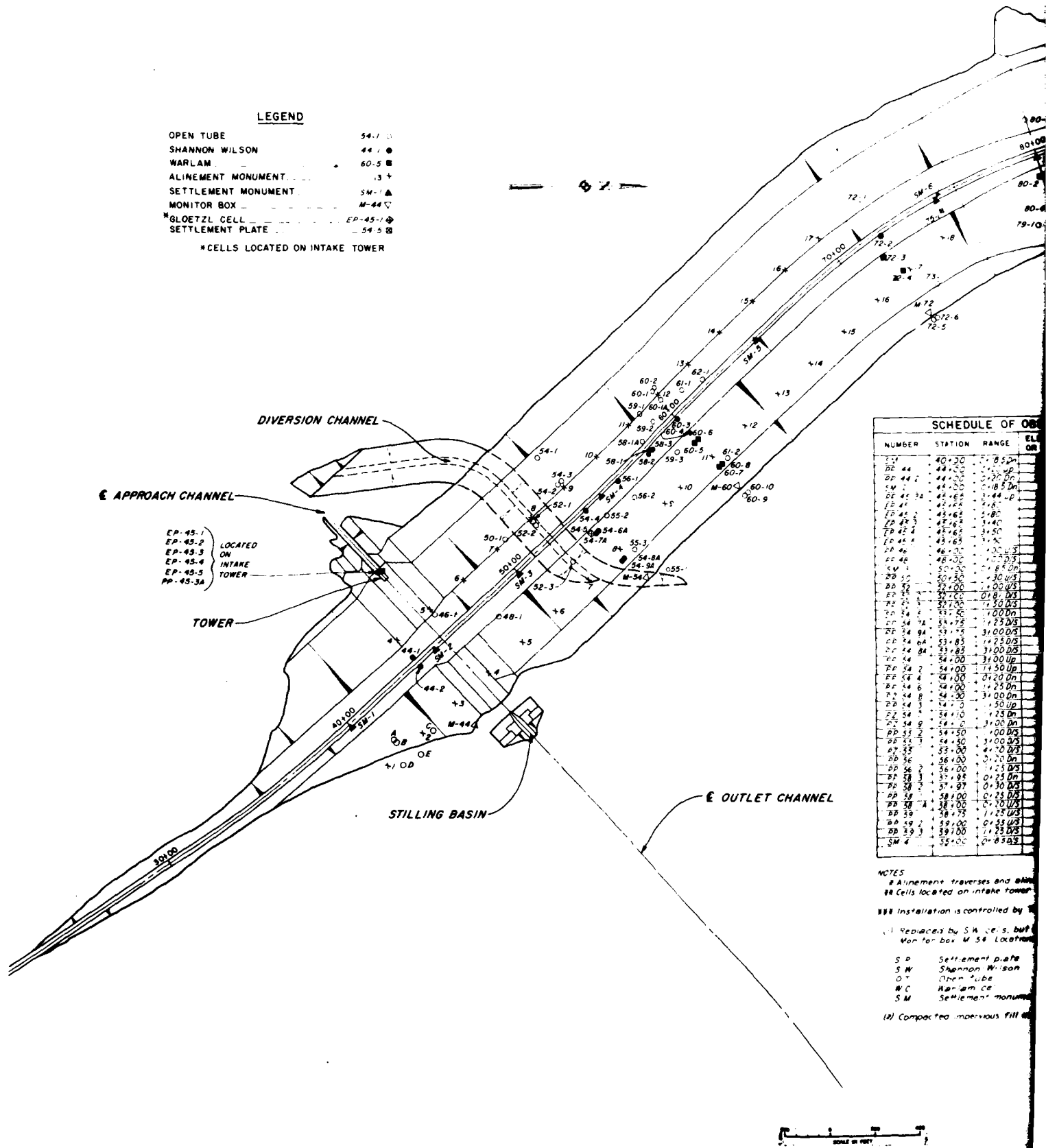
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KANSAS CITY DISTRICT
FILE NO. 0-5-1353
AUGUST 1978

Scale as shown

LEGEND

OPEN TUBE	54-1
SHANNON WILSON	44-1
WARLAM	60-5
ALIGNMENT MONUMENT	13
SETTLEMENT MONUMENT	SM-1
MONITOR BOX	M-44
GLOETZL CELL	EP-45-1
SETTLEMENT PLATE	54-5

* CELLS LOCATED ON INTAKE TOWER



NUMBER	STATION	RANGE	EL. OR
1	40+30	0-85	0
2	44+00	0-85	0
3	44+00	0-85	0
4	44+00	0-85	0
5	44+00	0-85	0
6	44+00	0-85	0
7	44+00	0-85	0
8	44+00	0-85	0
9	44+00	0-85	0
10	44+00	0-85	0
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98	44+00	0-85	0
99	44+00	0-85	0
100	44+00	0-85	0

NOTES

1. Alignment traverses and above

2. Cells located on intake tower

3. Installation is controlled by

4. Replaced by S.W. cells, but

5. Monitor box M-54 Location

S.P. Settlement plate

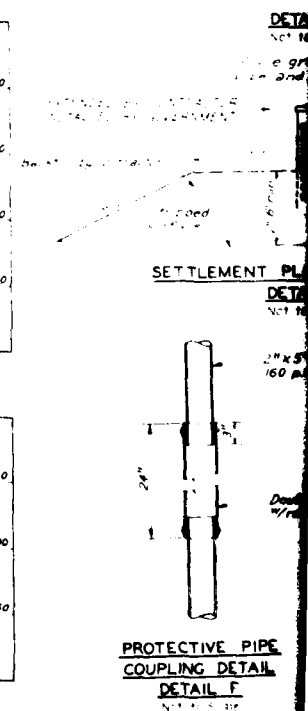
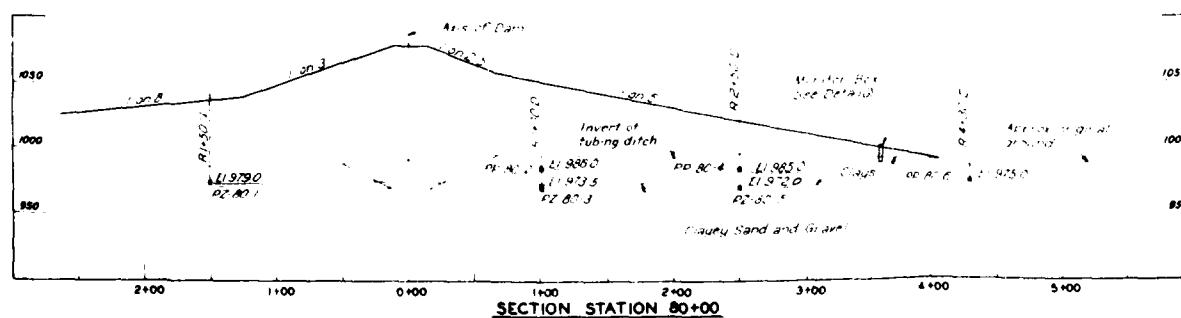
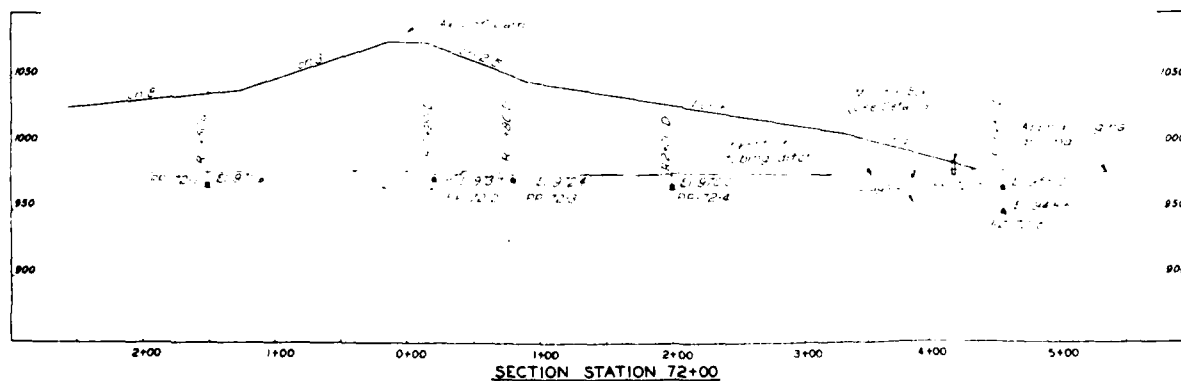
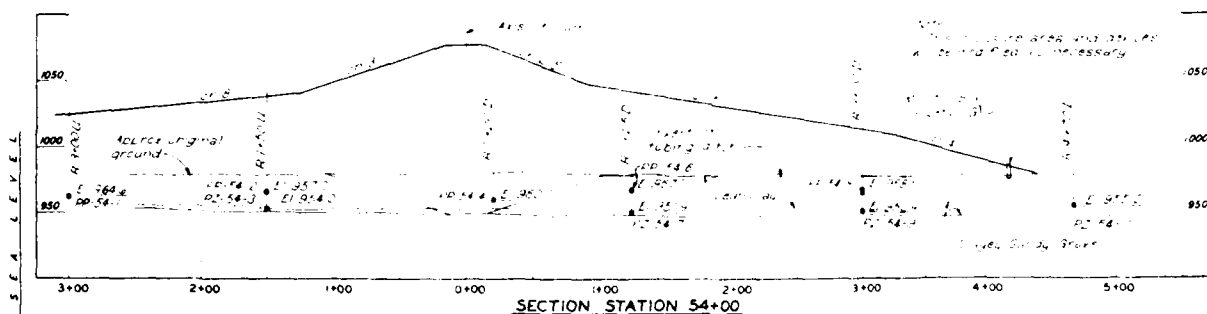
S.W. Shannon Wilson

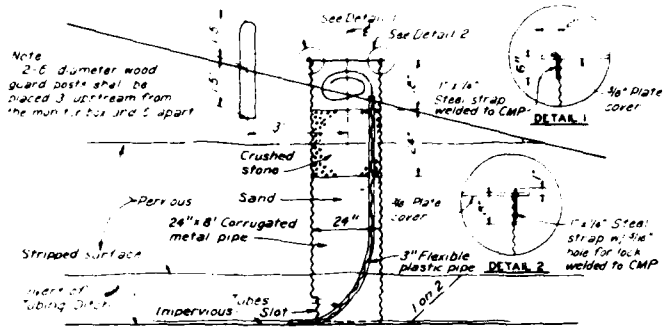
O.T. Open Tube

M.C. Monitor Cell

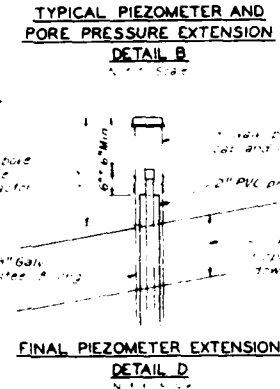
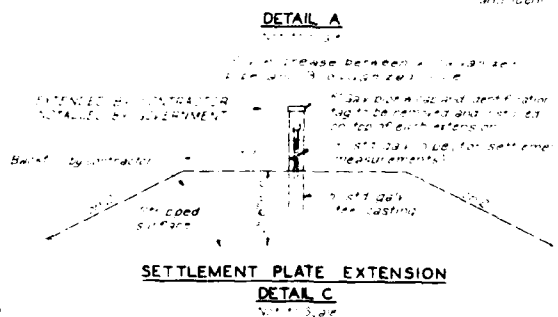
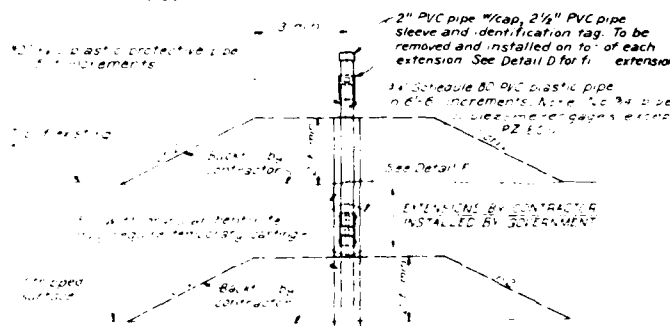
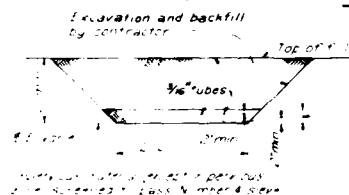
S.M. Settlement Monument

(2) Compacted impervious fill





SCHEDULE OF MONITOR BOX INSTALLATION				
BOX NO.	STATION	RANGE AT	APPROX EL. TOP OF BOX	
44	44+00	2+00	998.0	
54	54+00	4+22	986.0	
60	60+00	4+22	986.0	
72	72+00	4+22	986.0	
80	80+00	1+00	995.0	



NOTES

All PVC plastic pipe shall meet the requirements of ASTM Spec. No. D-1785-60T type I.

Double Bell Couplings shall be similar to Johns-Manville Double Bell Couplings.

Alignment pipes extended above the embankment are to be painted by contractor.

See Plate C for location of 5' scale cells on Control tower.

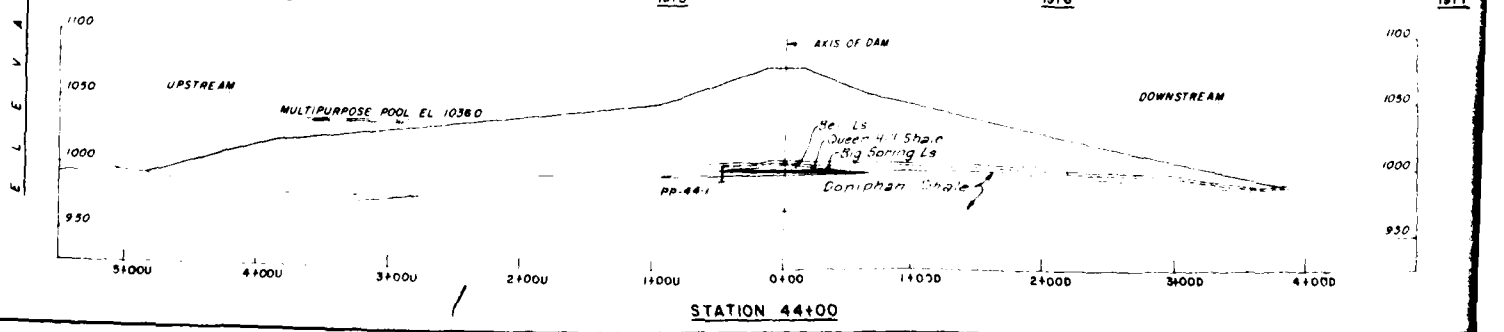
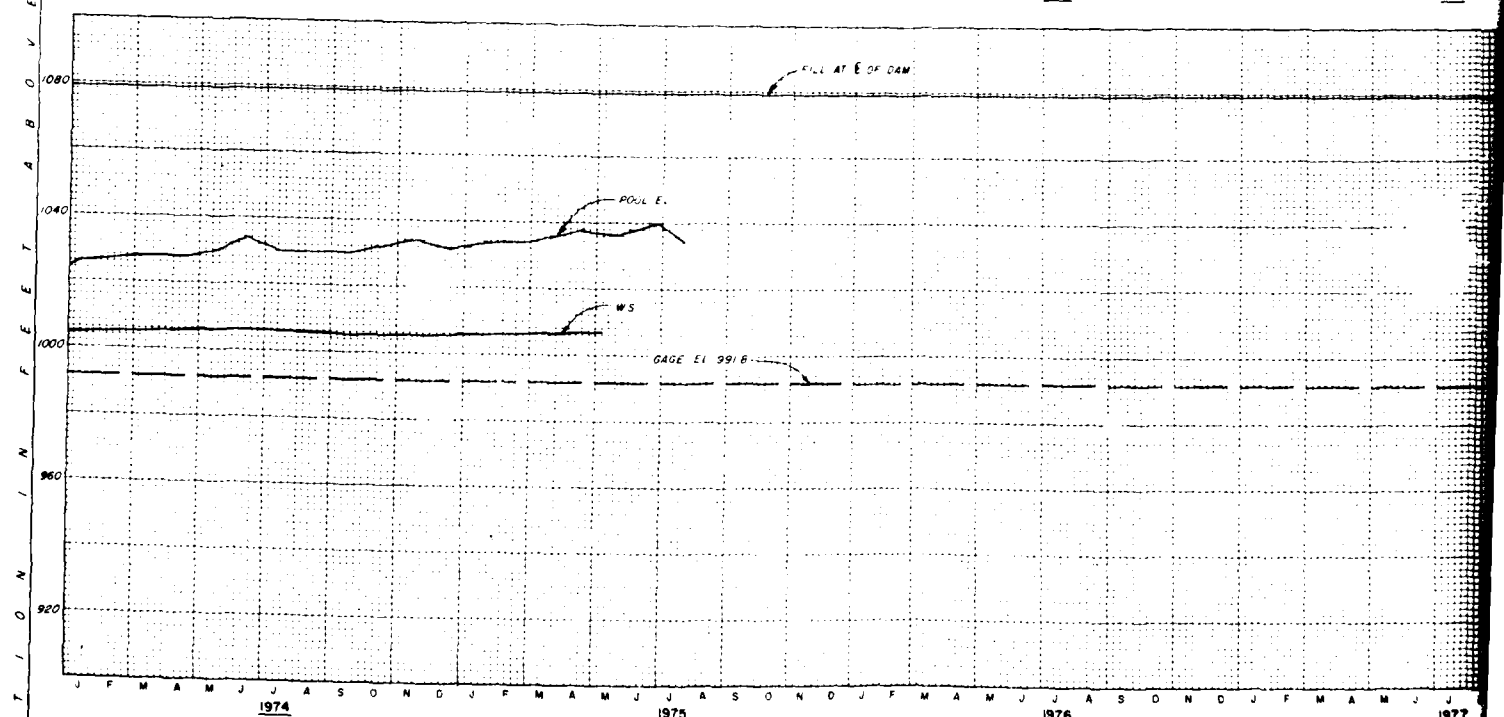
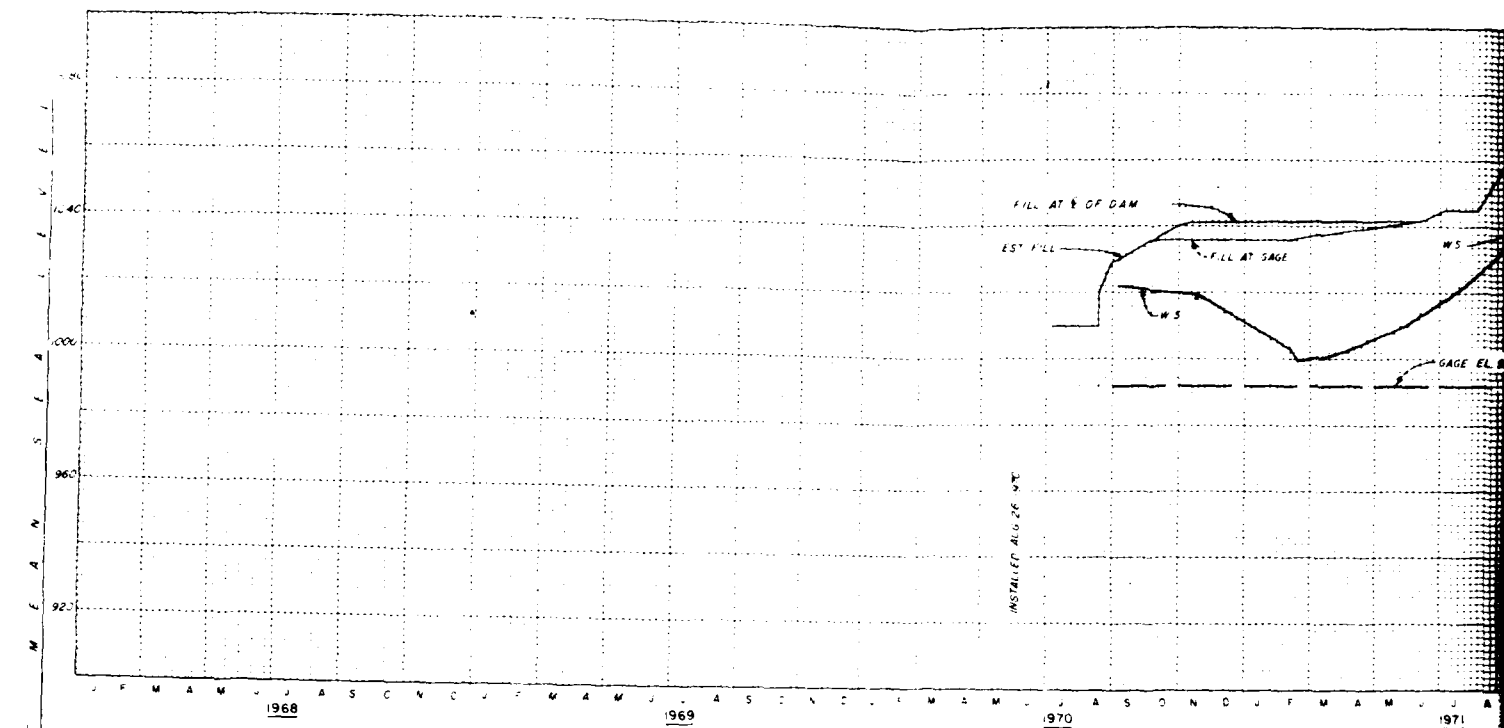
MARAS DES CYGNES RIVER, KANSAS
MELVERN LAKE
EMBANKMENT CRITERIA AND PERFORMANCE REPORT
EMBANKMENT OBSERVATION DEVICES

In 1 sheet

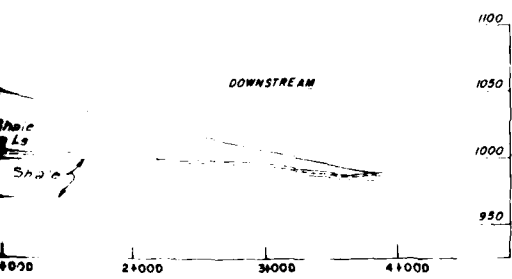
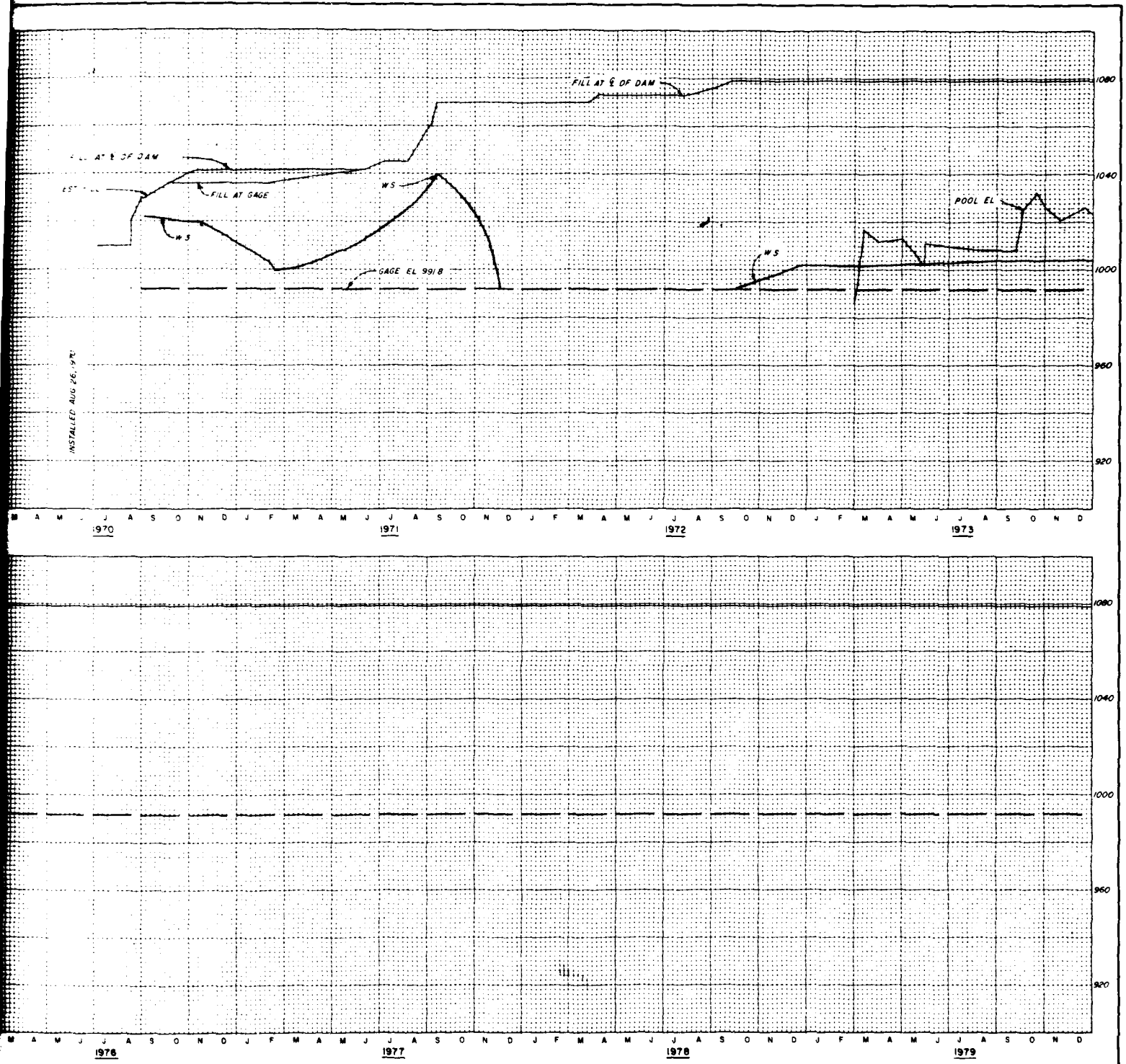
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Scale as shown

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KANSAS CITY DISTRICT
FILE NO. 0-5-1355
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STATION 44+00



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MARAI DES CYGNES RIVER, KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
PP-44-1 (SHANNON-WILSON CELL)

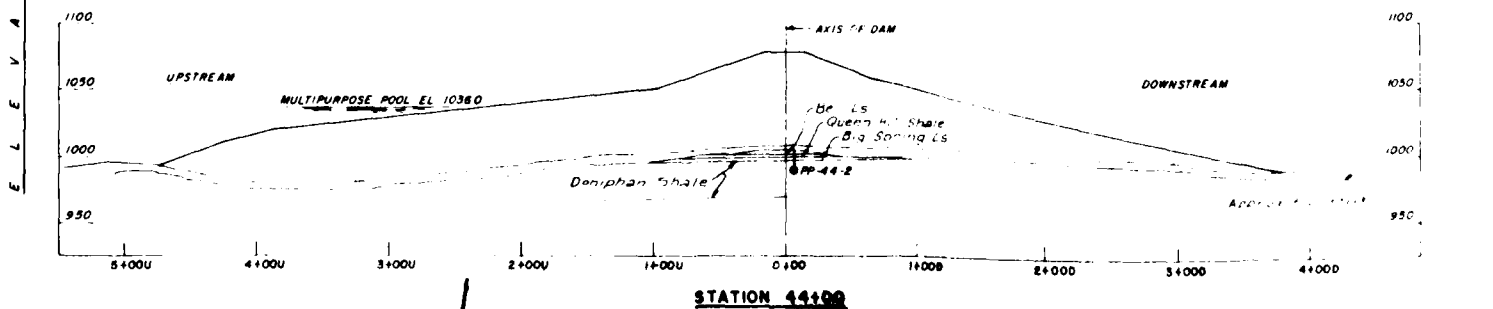
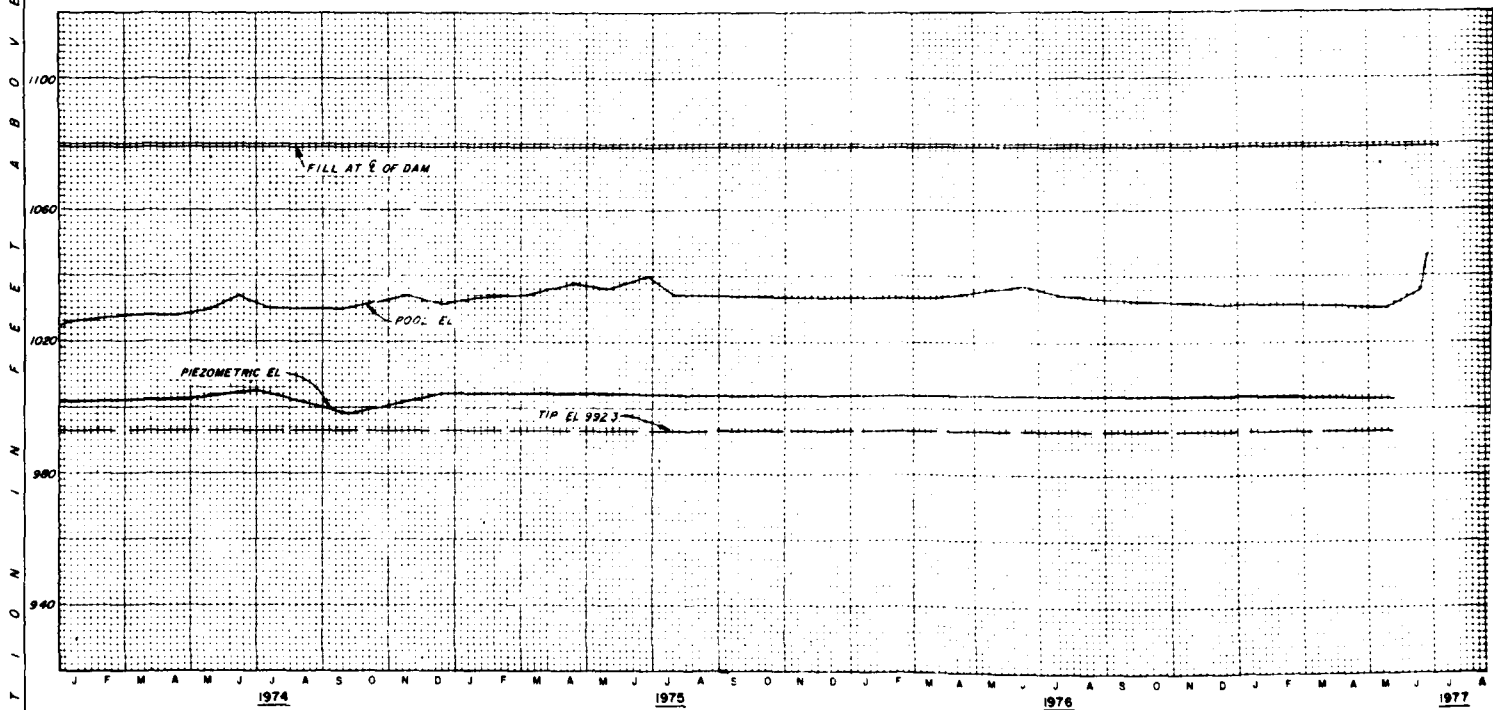
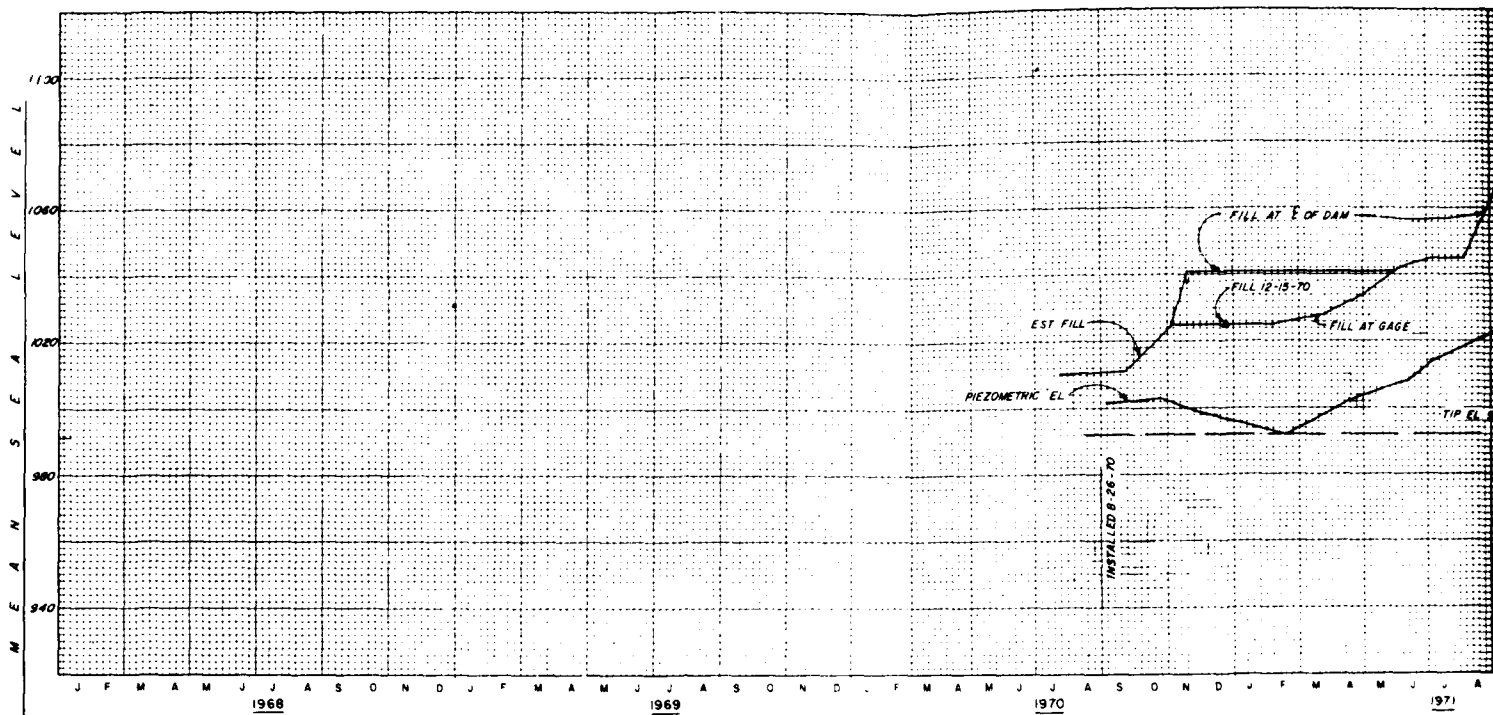
In 1 sheet

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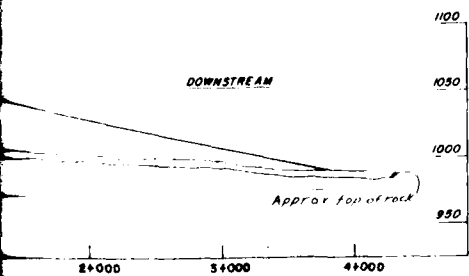
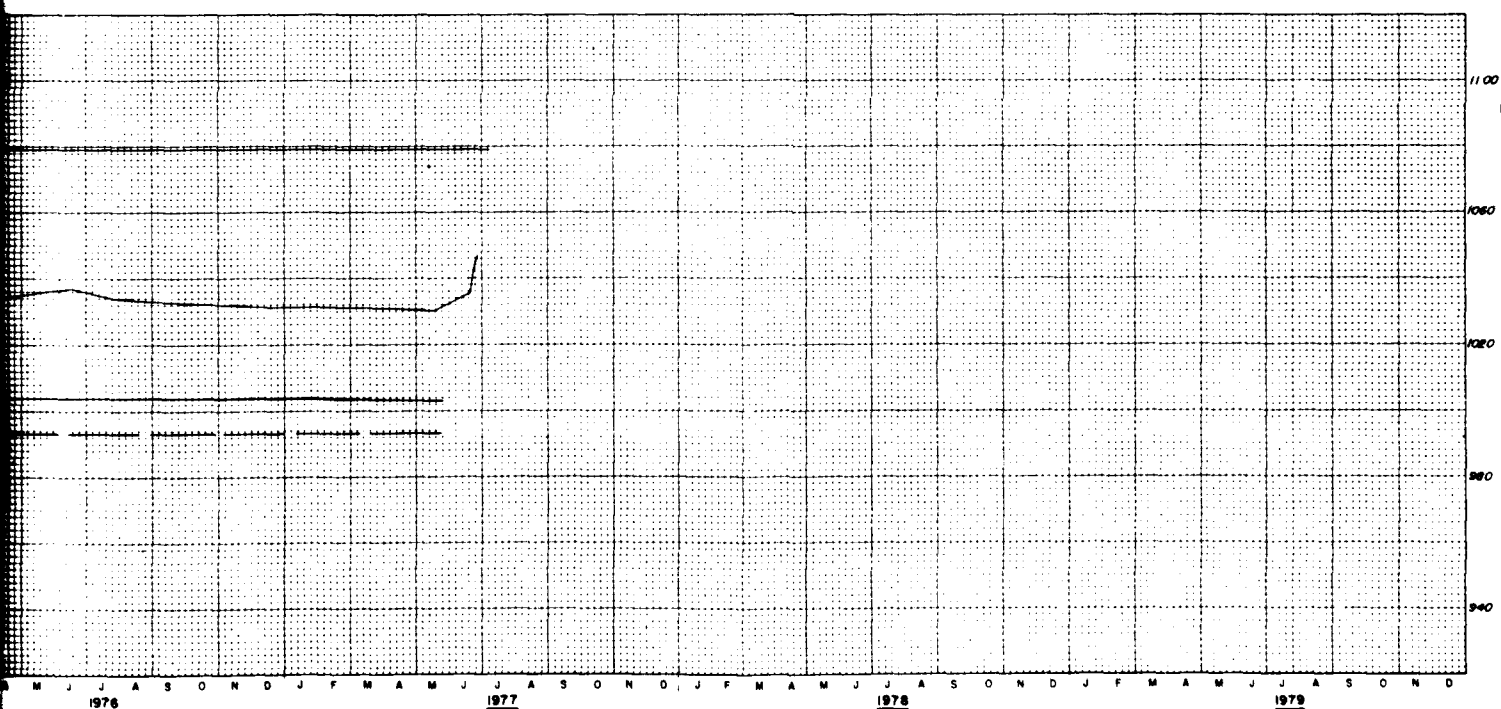
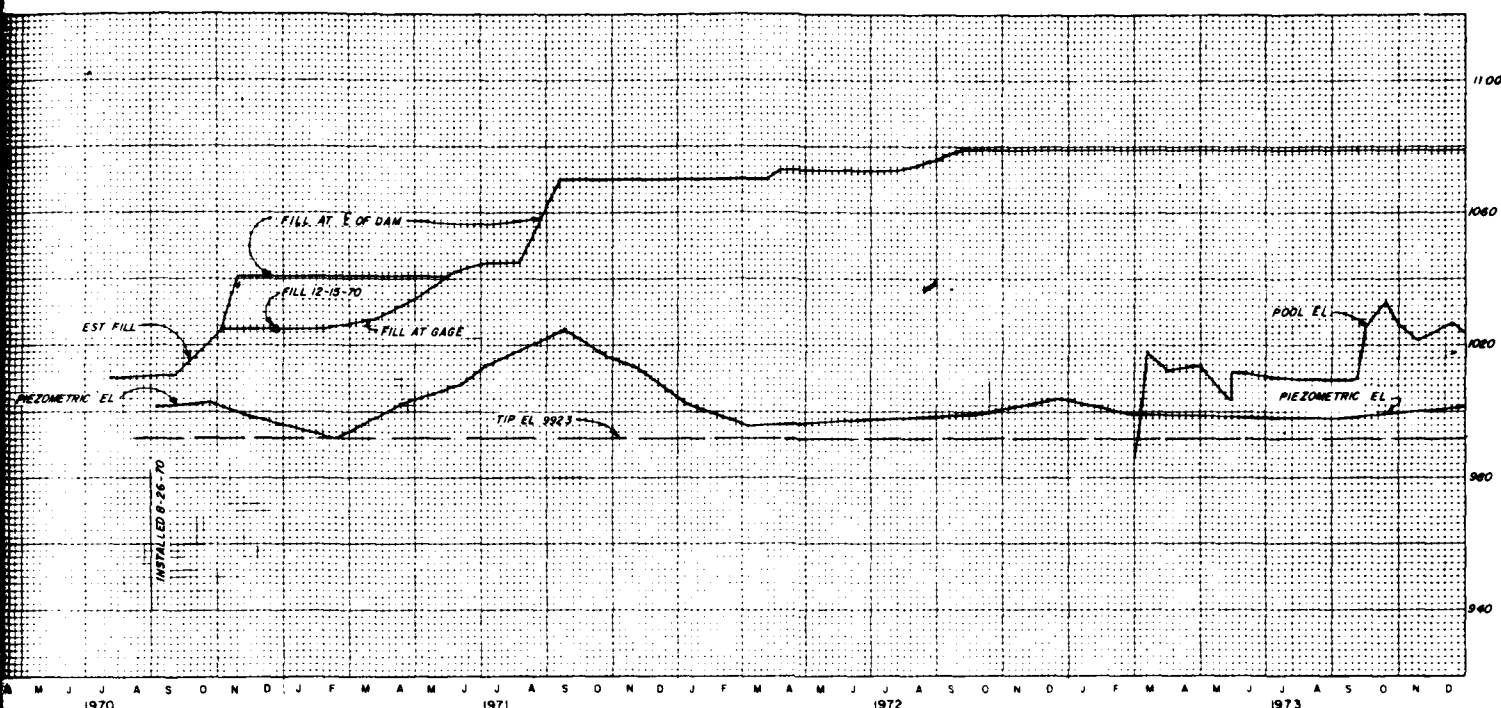
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KANSAS CITY DISTRICT

FILE NO. O-5-1264
AUGUST 1975



STATION 4400

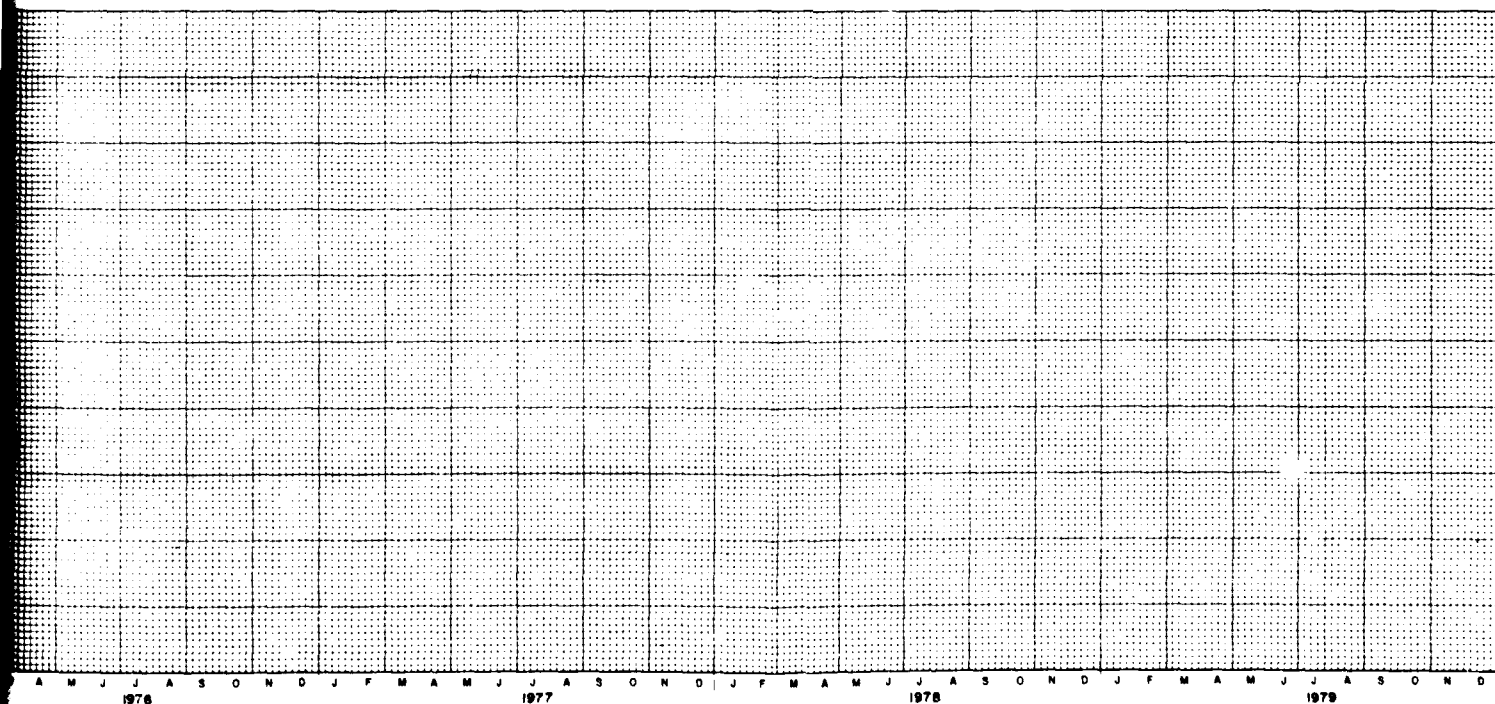
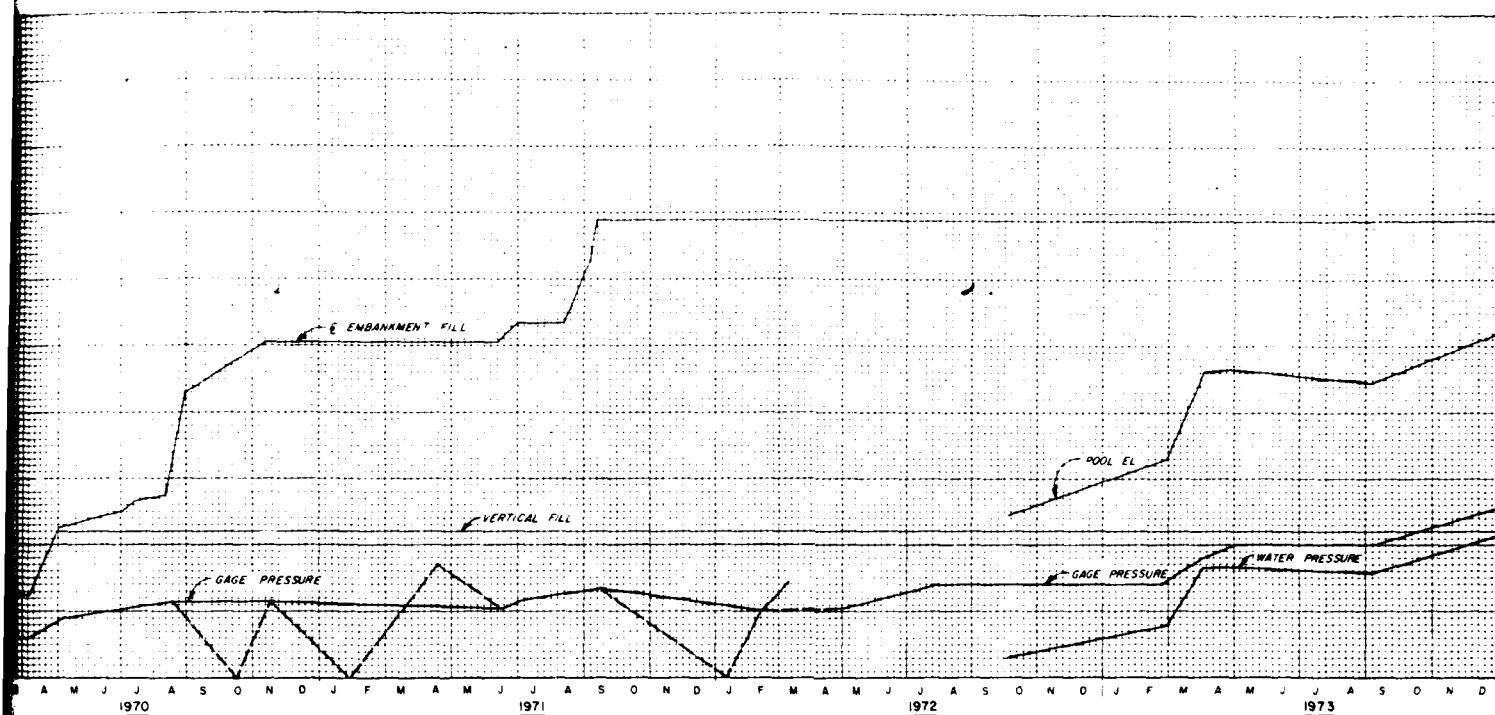


LEGEND
 OPEN TUBE ○
 PNEUMATIC CELLS ●

NOTE
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 MARAIS DES CYGNES RIVER KANSAS
MELVERN LAKE
 INSTRUMENTATION PLOTS
 PP-44-2 (SHANNON-WILSON CELL)

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MARAIS DES CYGNES RIVER KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
EP-45-1 (GLOETZL CELL)

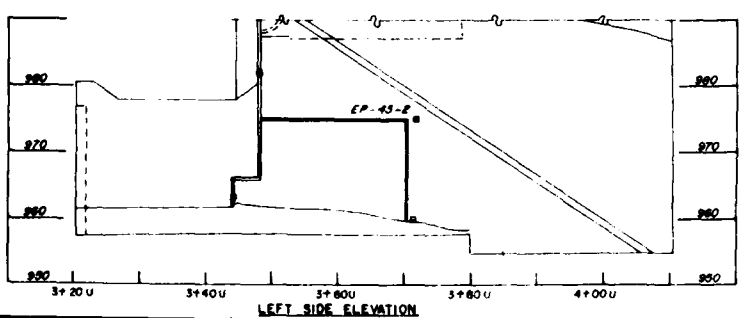
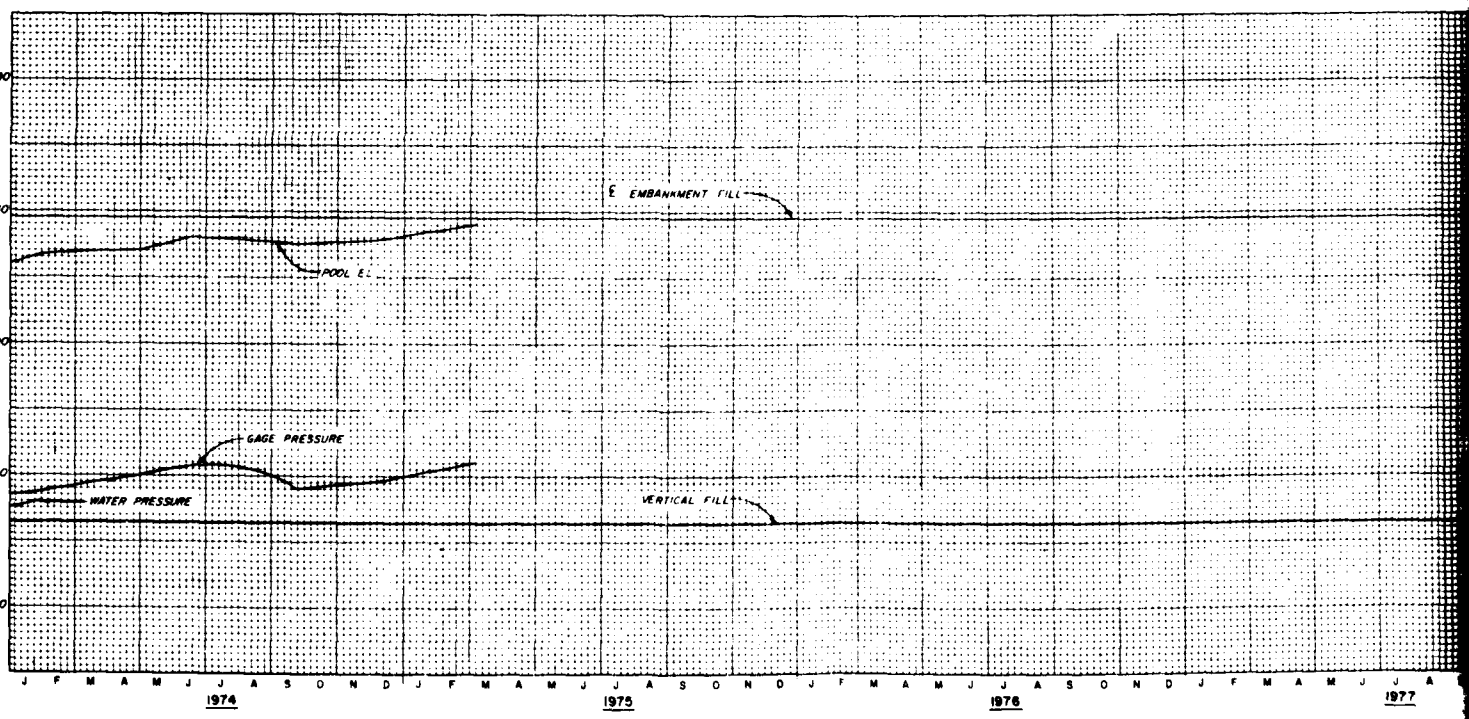
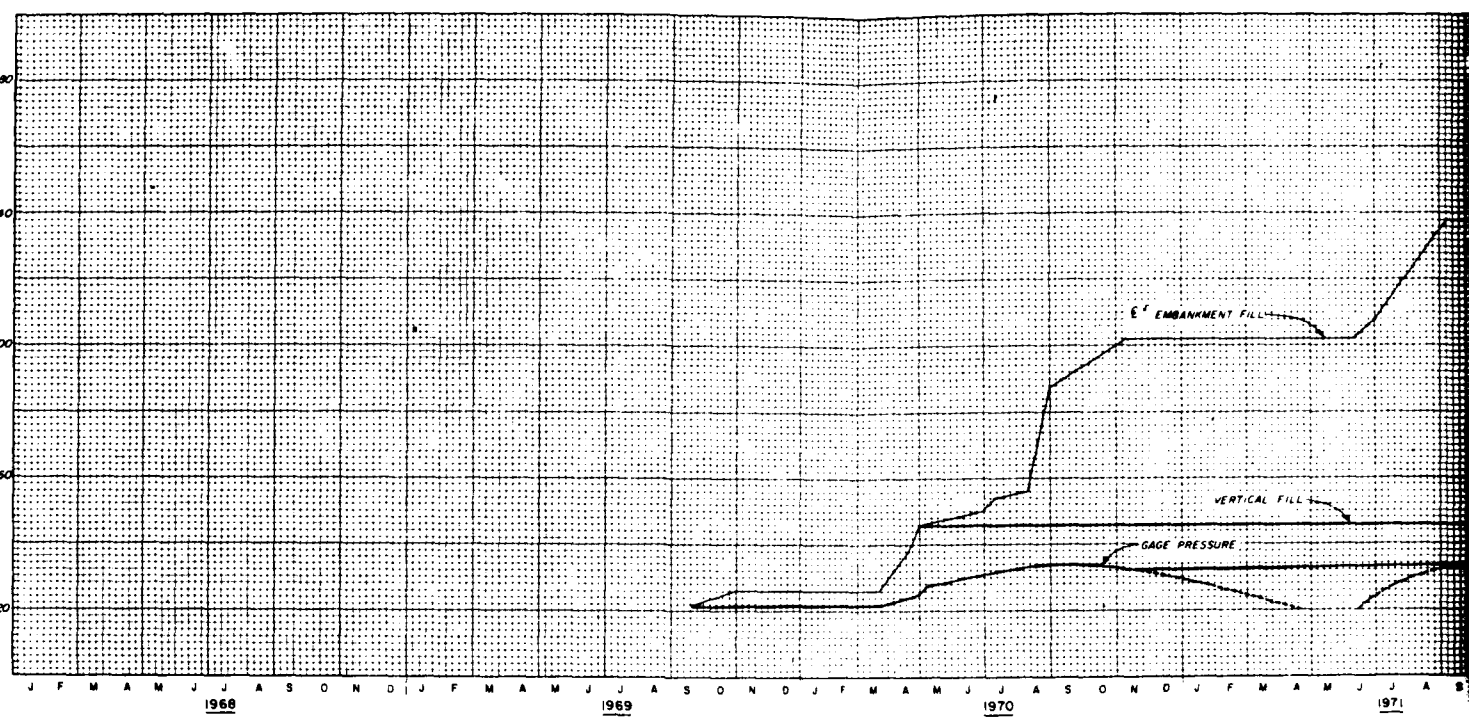
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KANSAS CITY DISTRICT

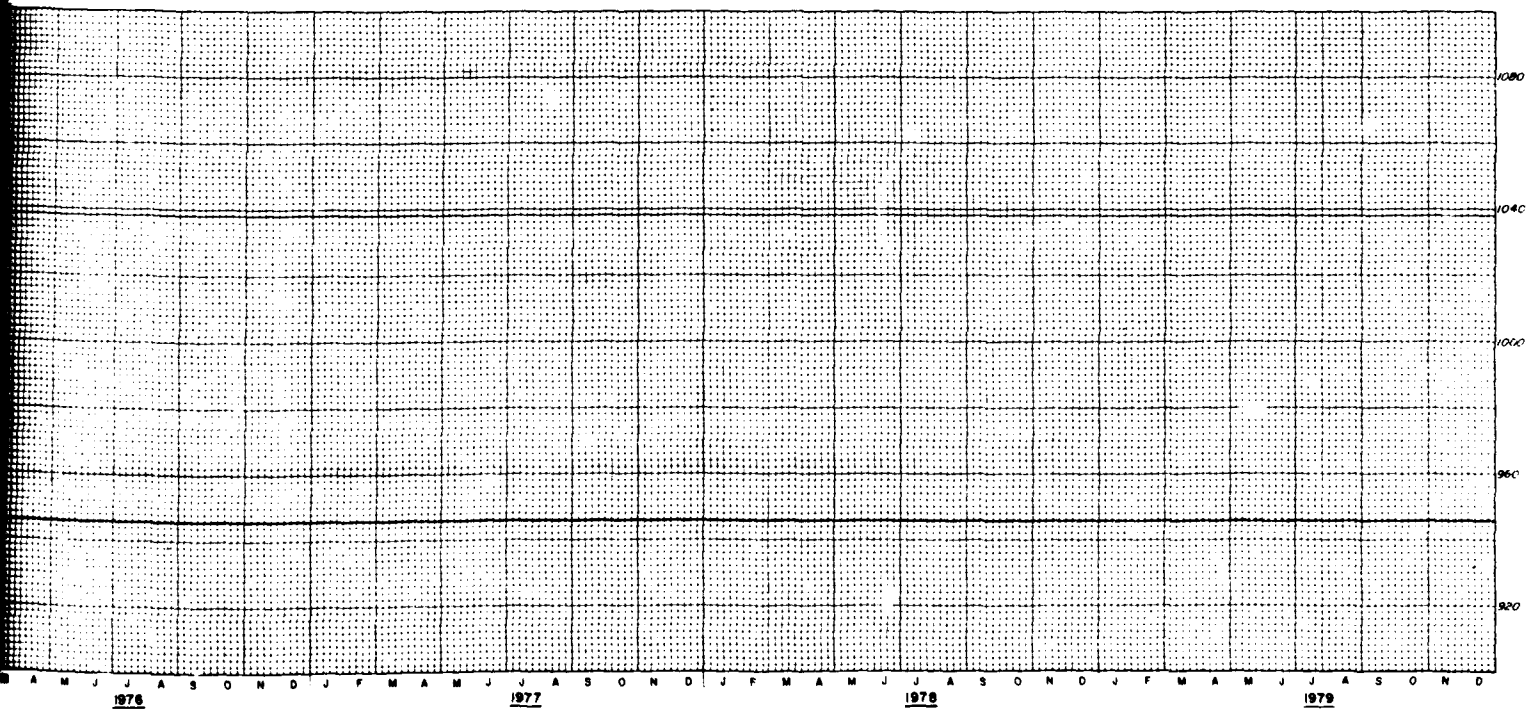
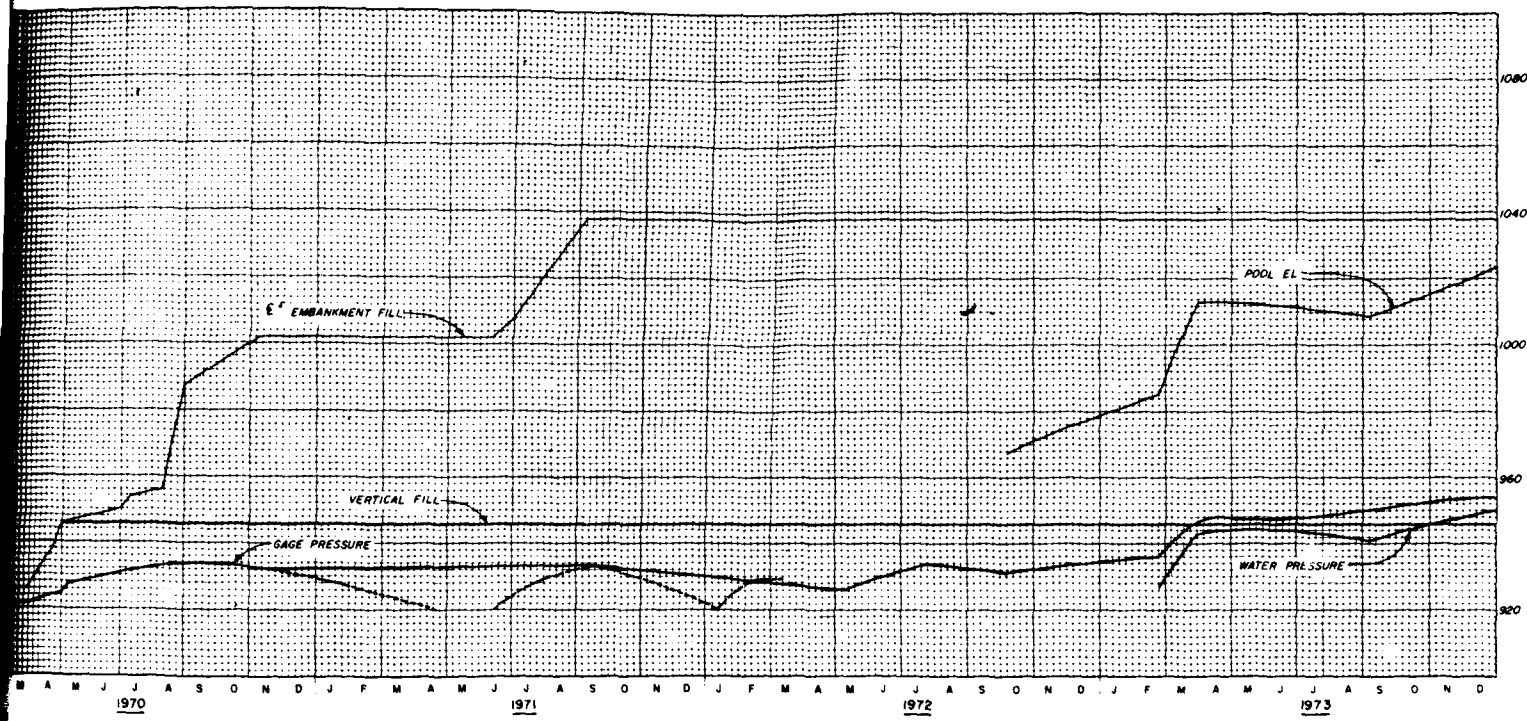
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LEFT SIDE ELEVATION

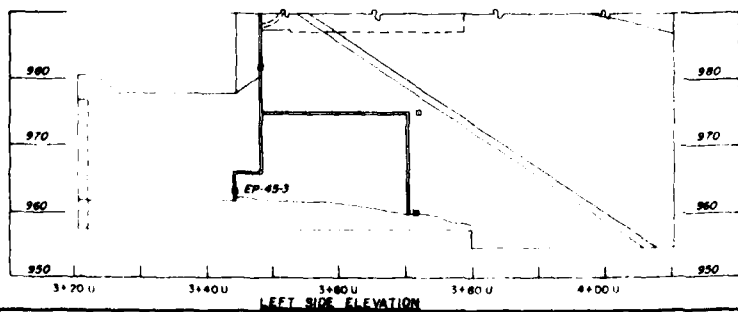
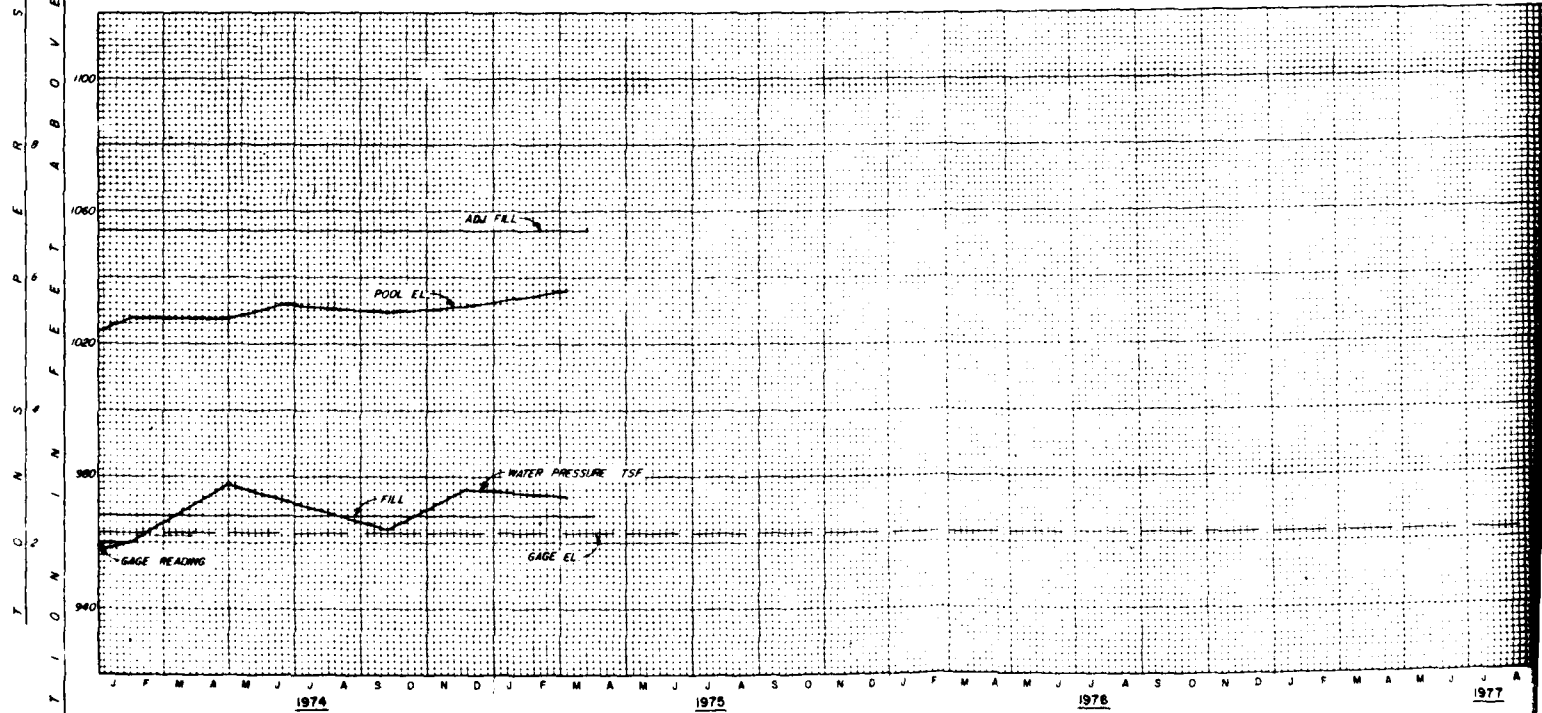
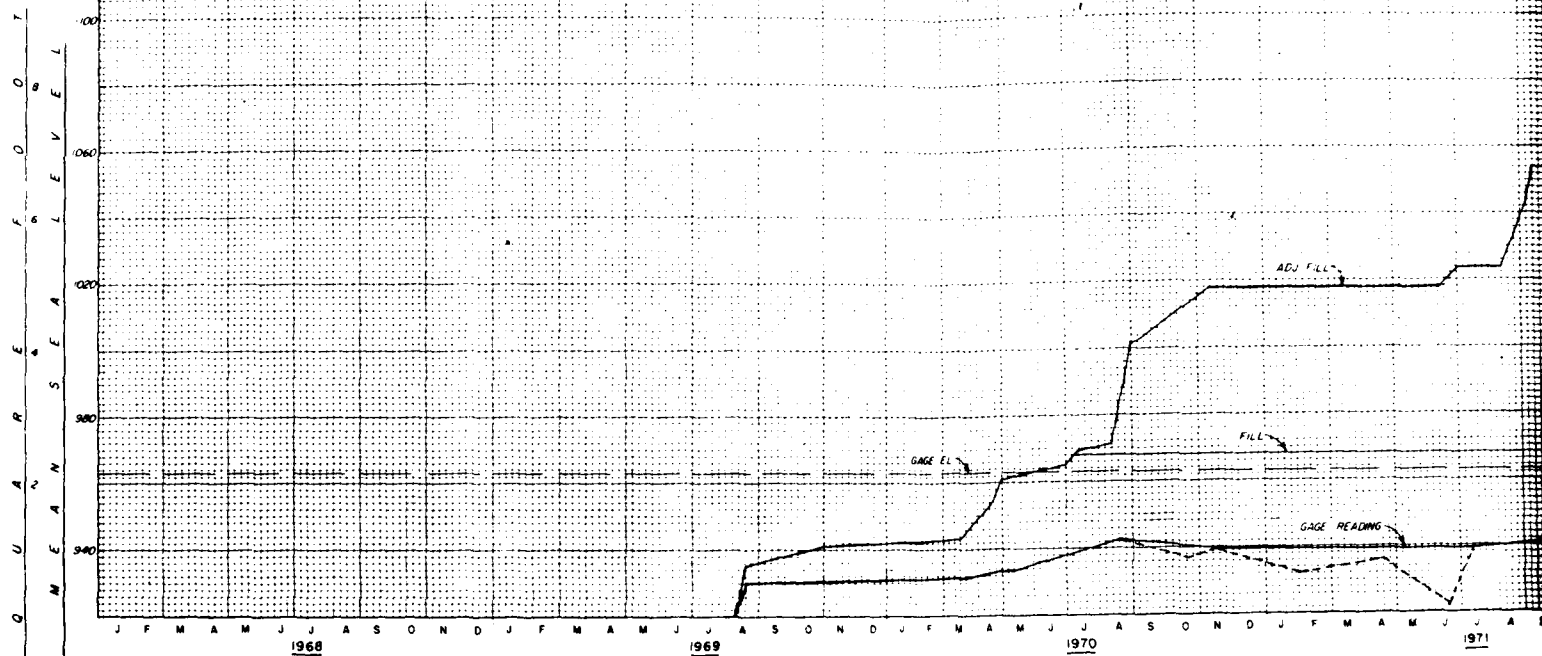


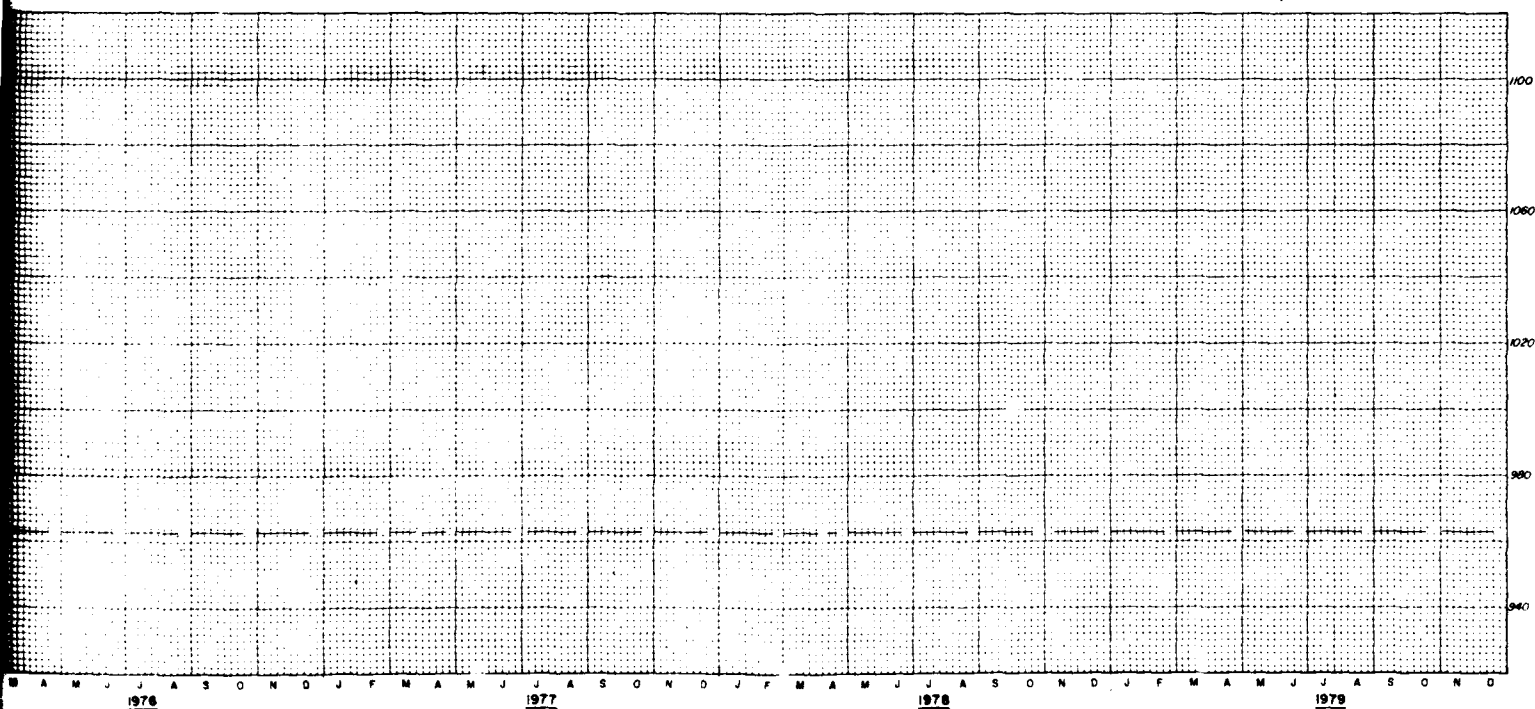
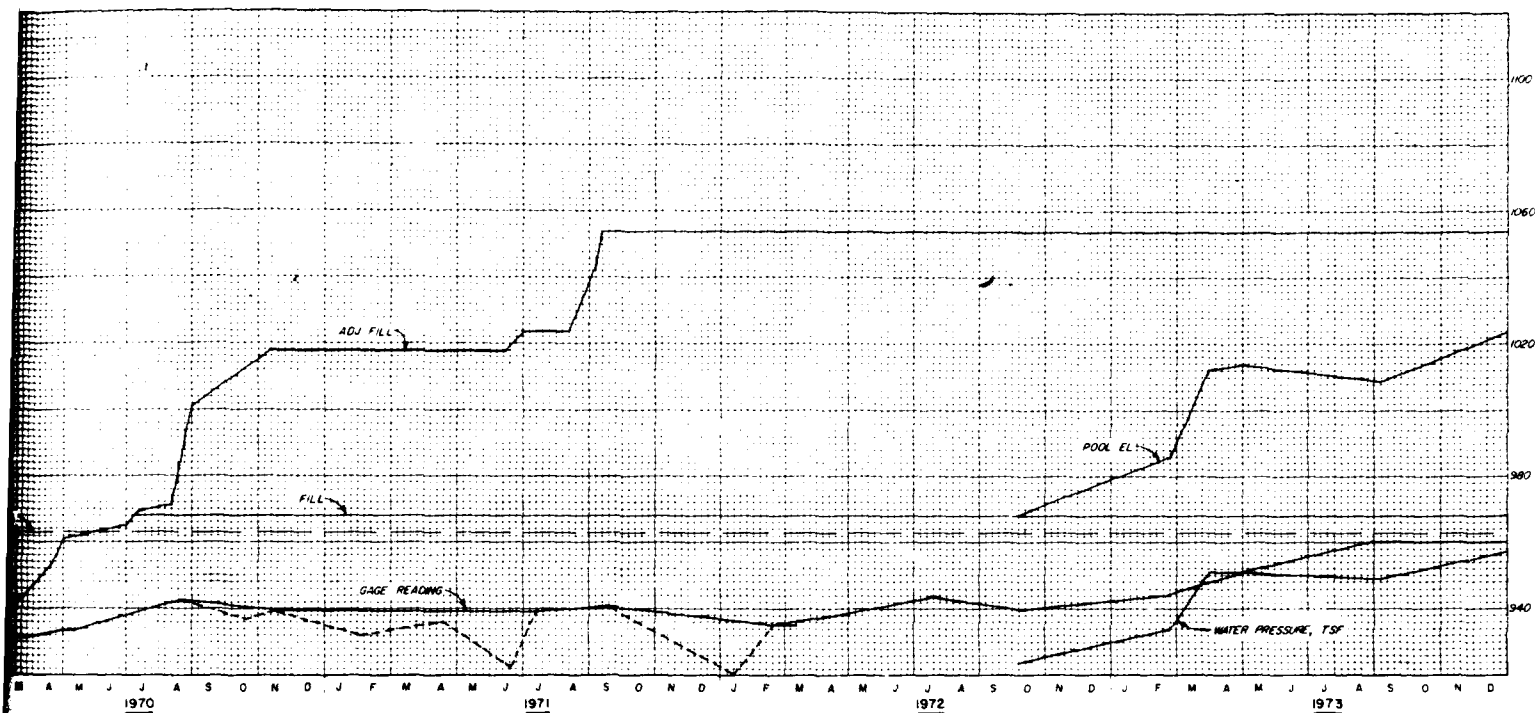
NOTE
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MELVERN LAKE

INSTRUMENTATION PLOTS
 EP-45-2 GLOETZEL CELL

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 KANSAS CITY DISTRICT
FILE NO. 0-5-1267
 AUGUST 1975

2





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INSTRUMENTATION PLOTS
EP-45-3(GLOETZL CELL)

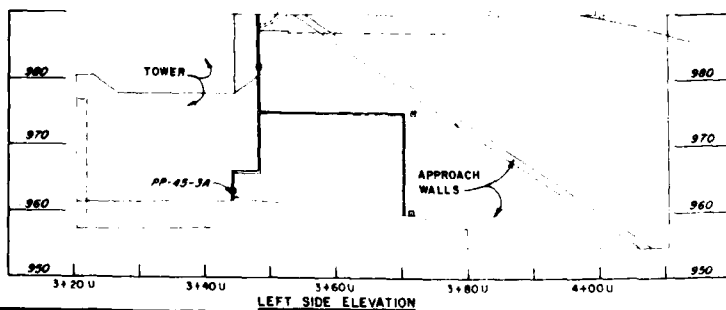
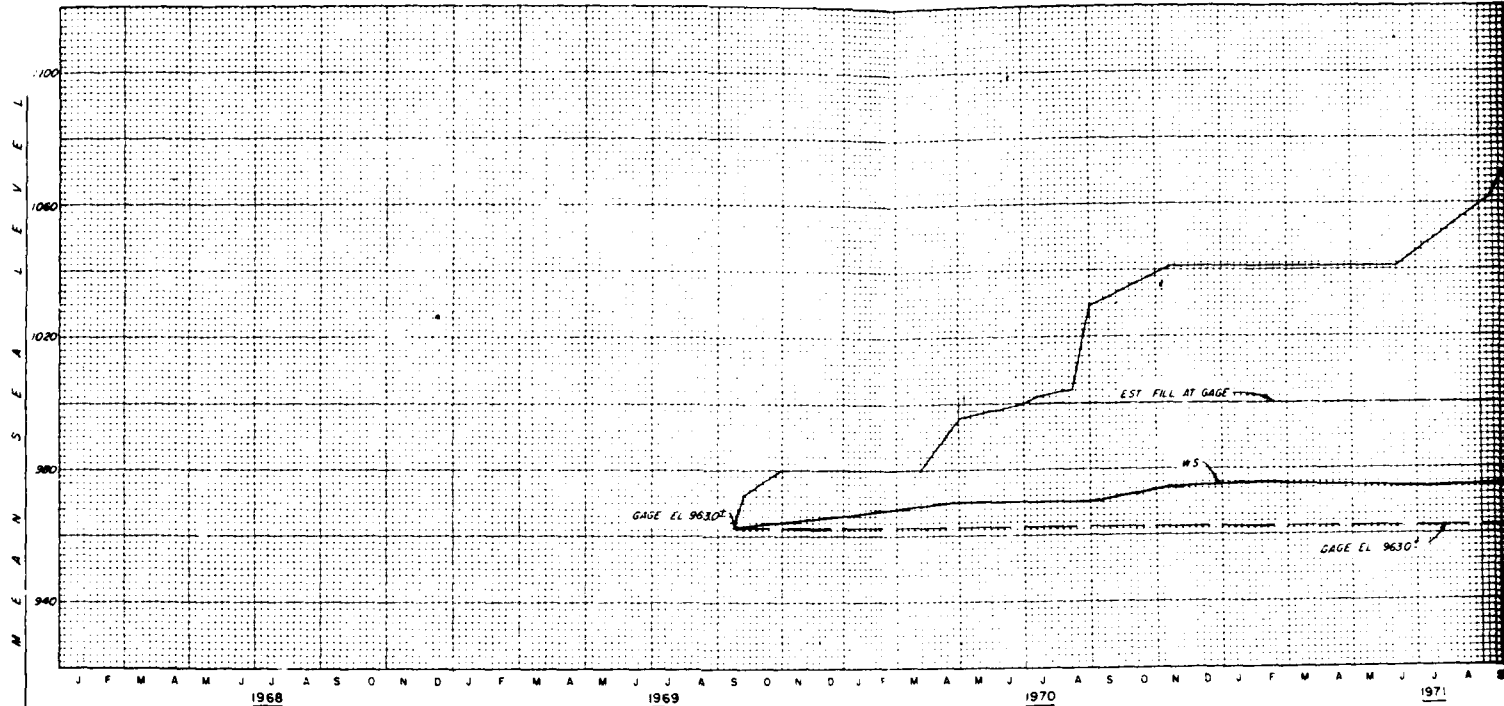
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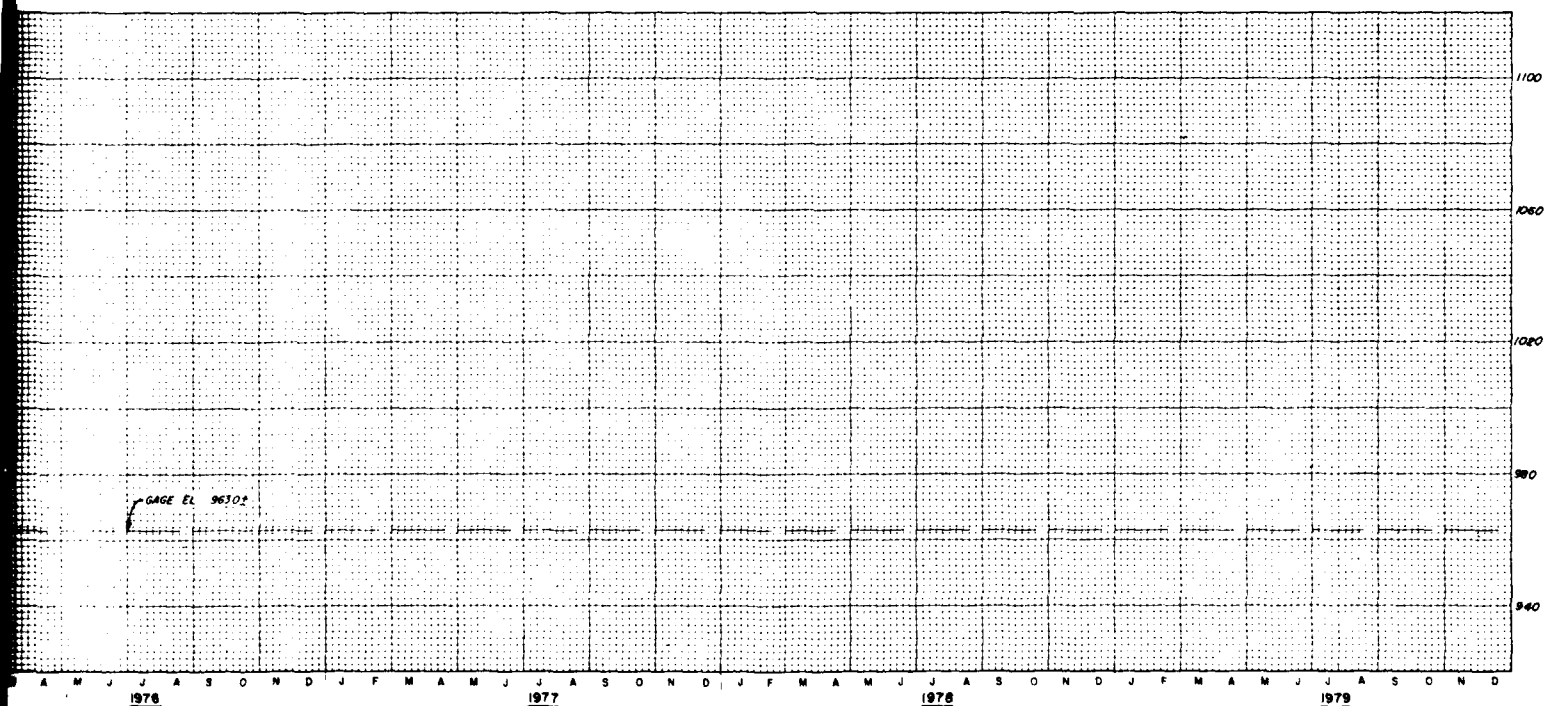
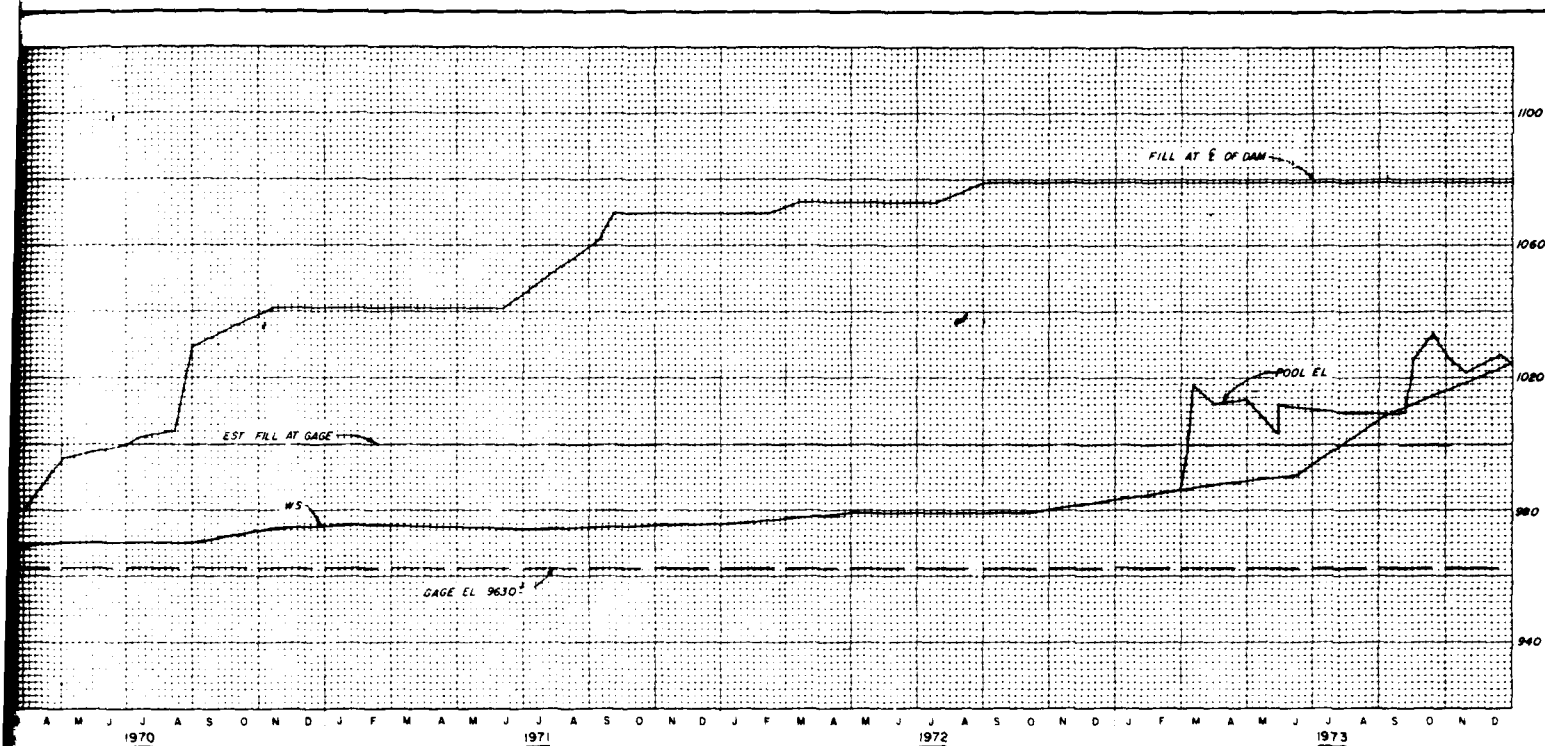
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Scale as shown

C. H. ENGINEERS U. S. ARMY
KANSAS CITY DISTRICT

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AUGUST 1975





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MARAI DES CYGNES RIVER KANSAS
MELVERN LAKE

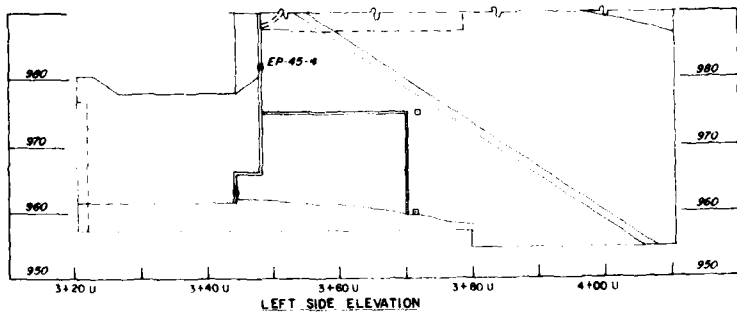
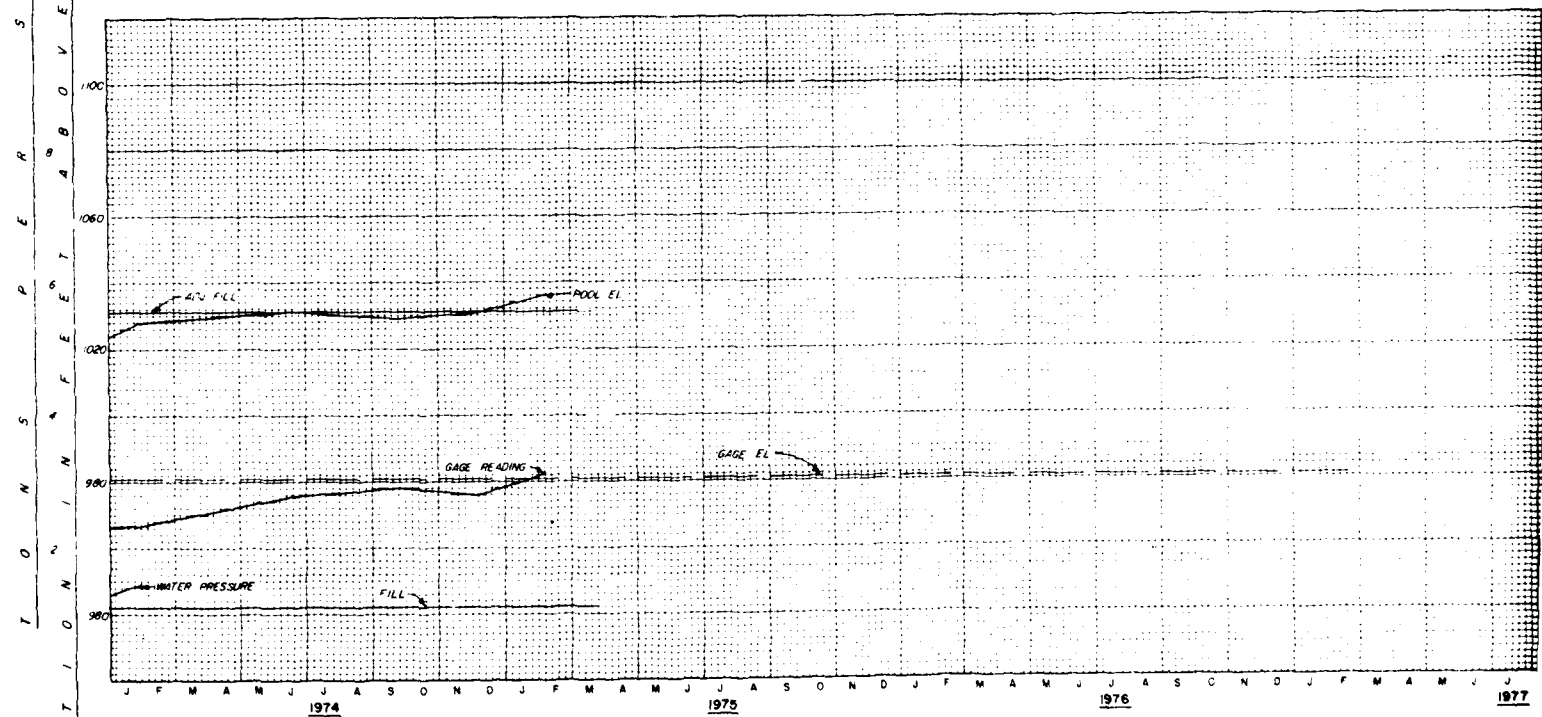
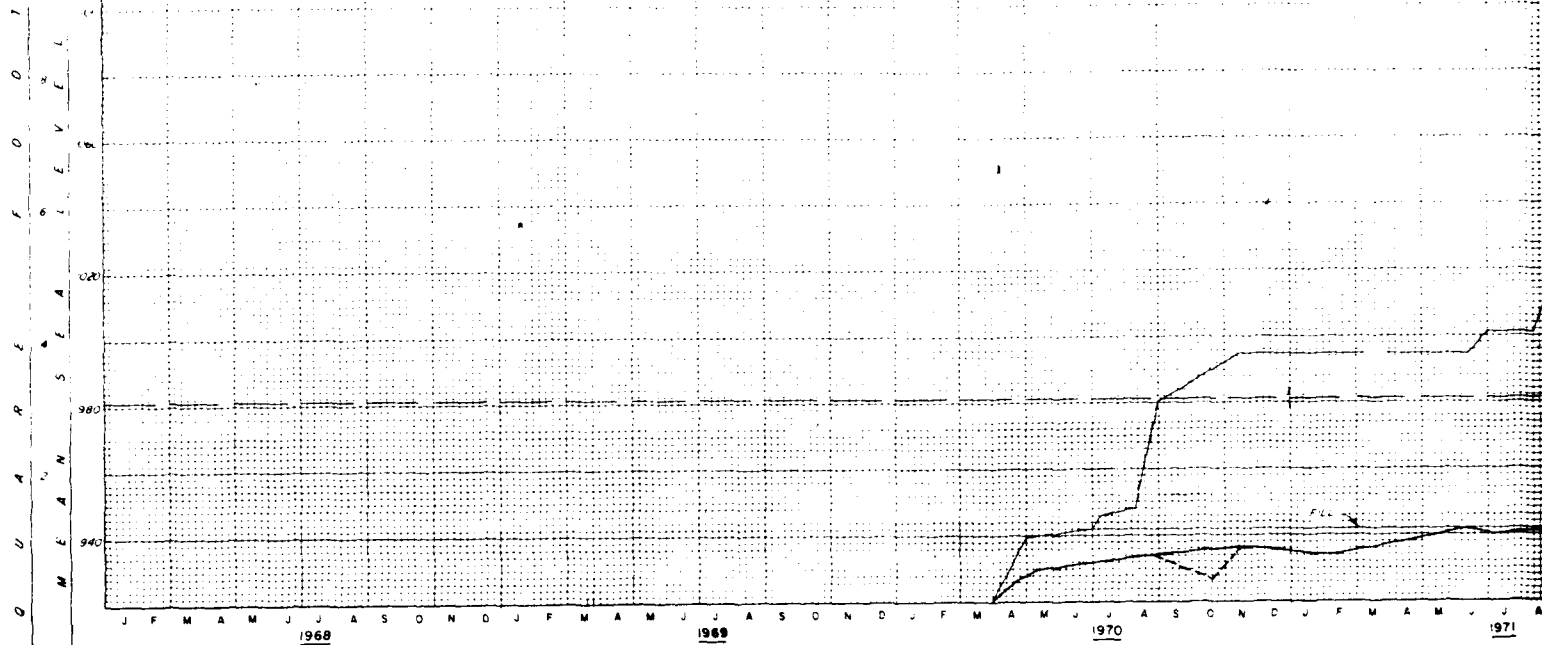
INSTRUMENTATION PLOTS
PP-45-3A (SHANNON-WILSON CELL)

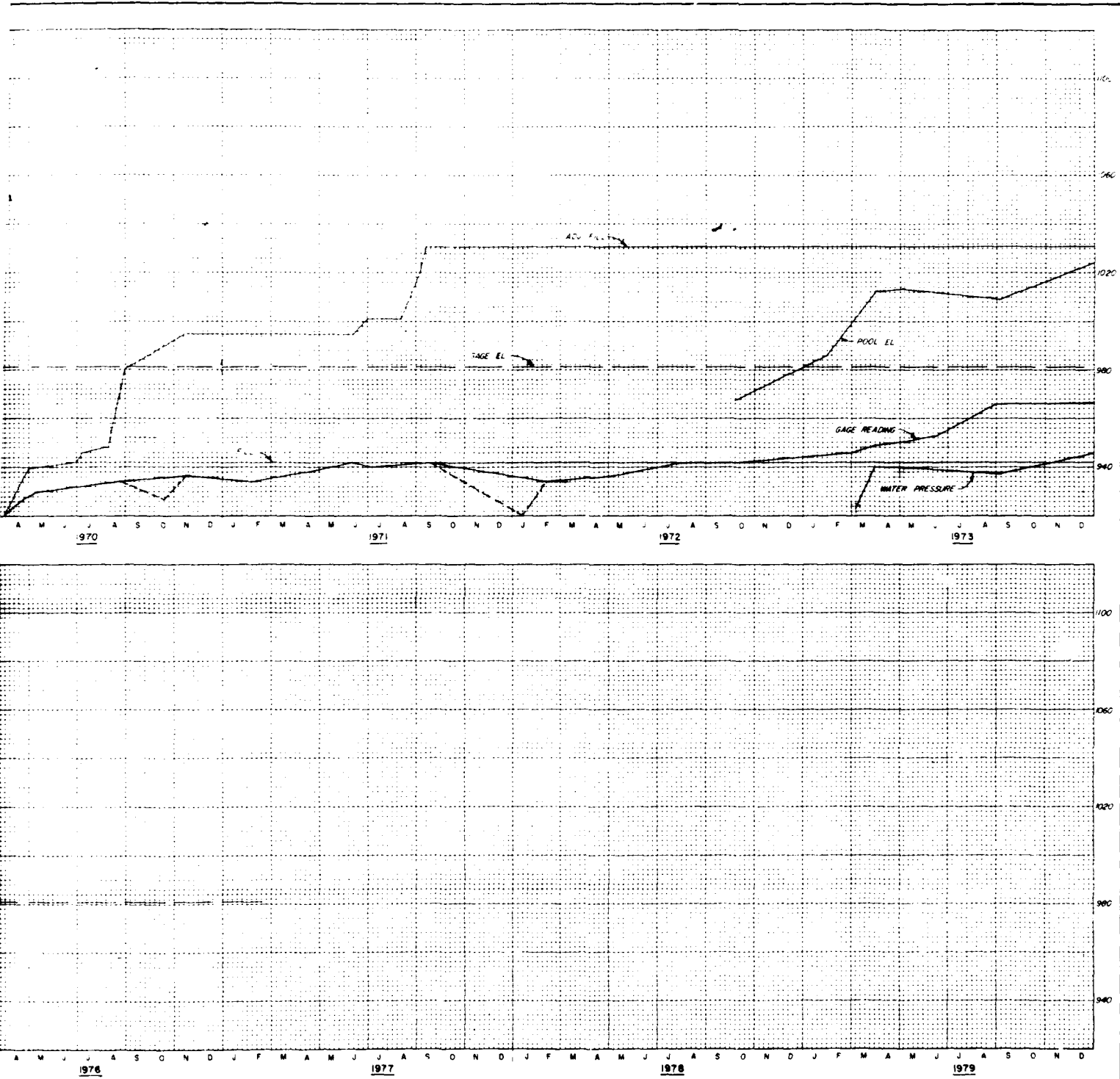
In 1 sheet

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KANSAS CITY DISTRICT

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FILE NO. O-5-1269
AUGUST 1975

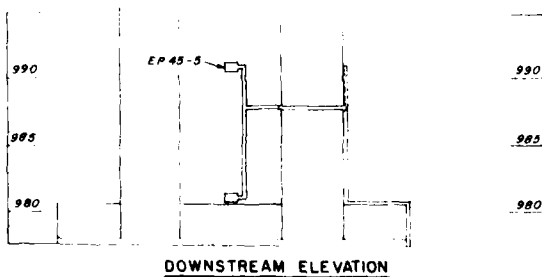
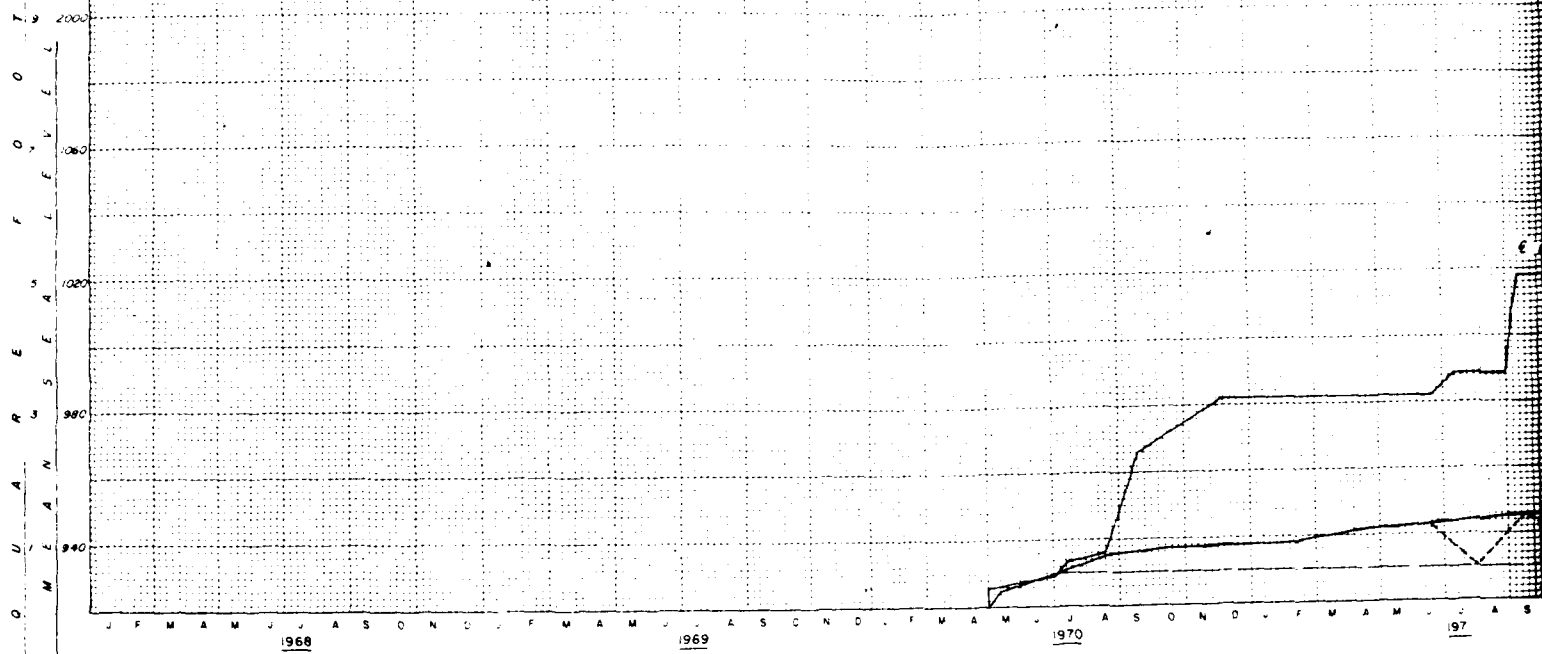


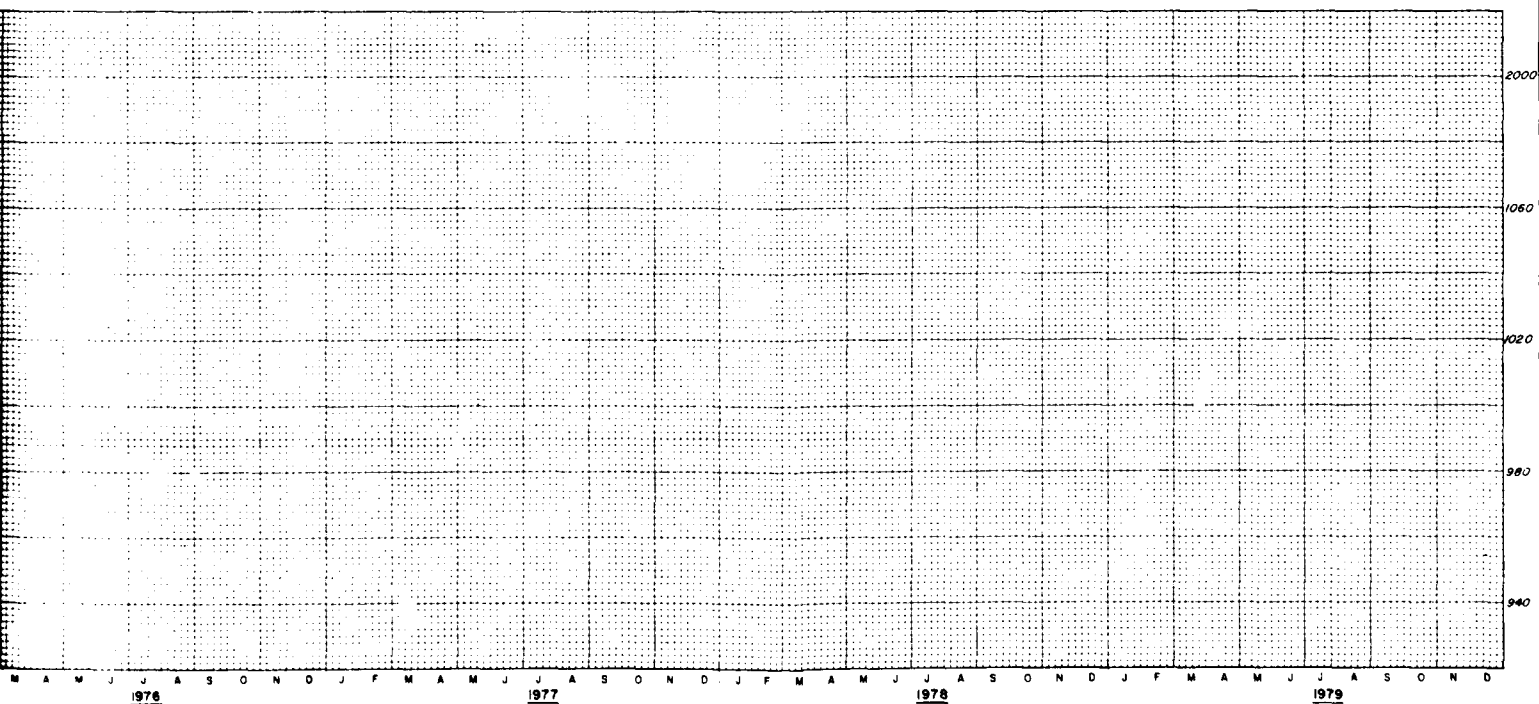
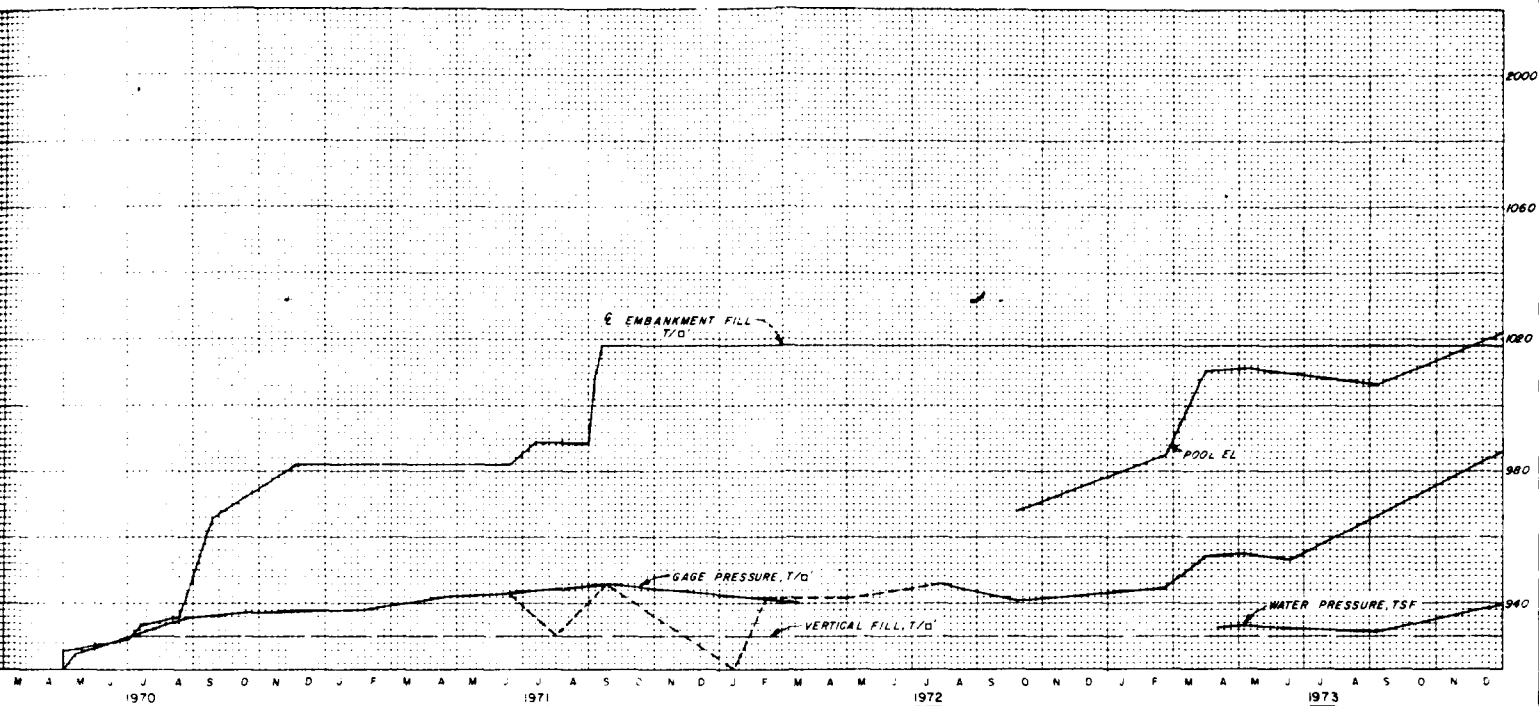


NOTE:
NOT READ FOR THIS REPORT.
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MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
EP-45-4 (GLOETZL CELL)

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KANSAS CITY DISTRICT
FILE NO. O-5-1270
AUGUST 1975



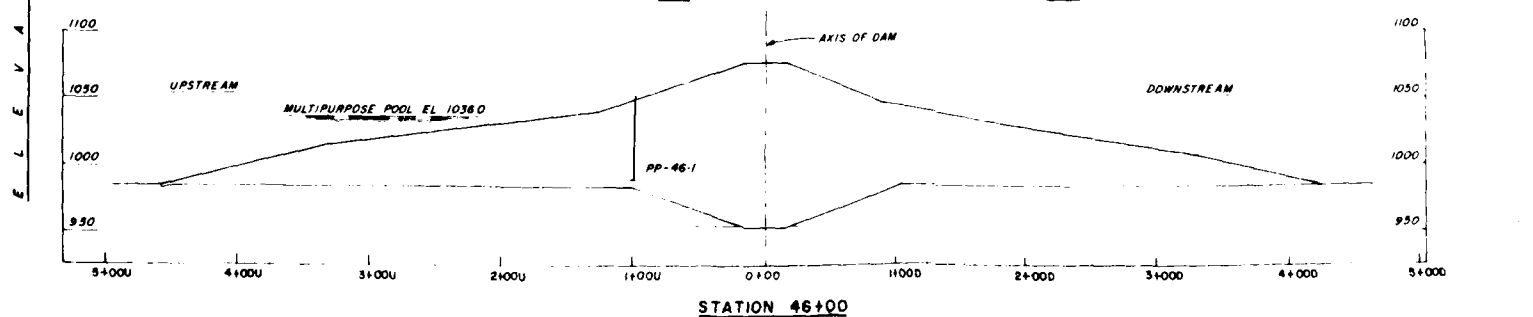
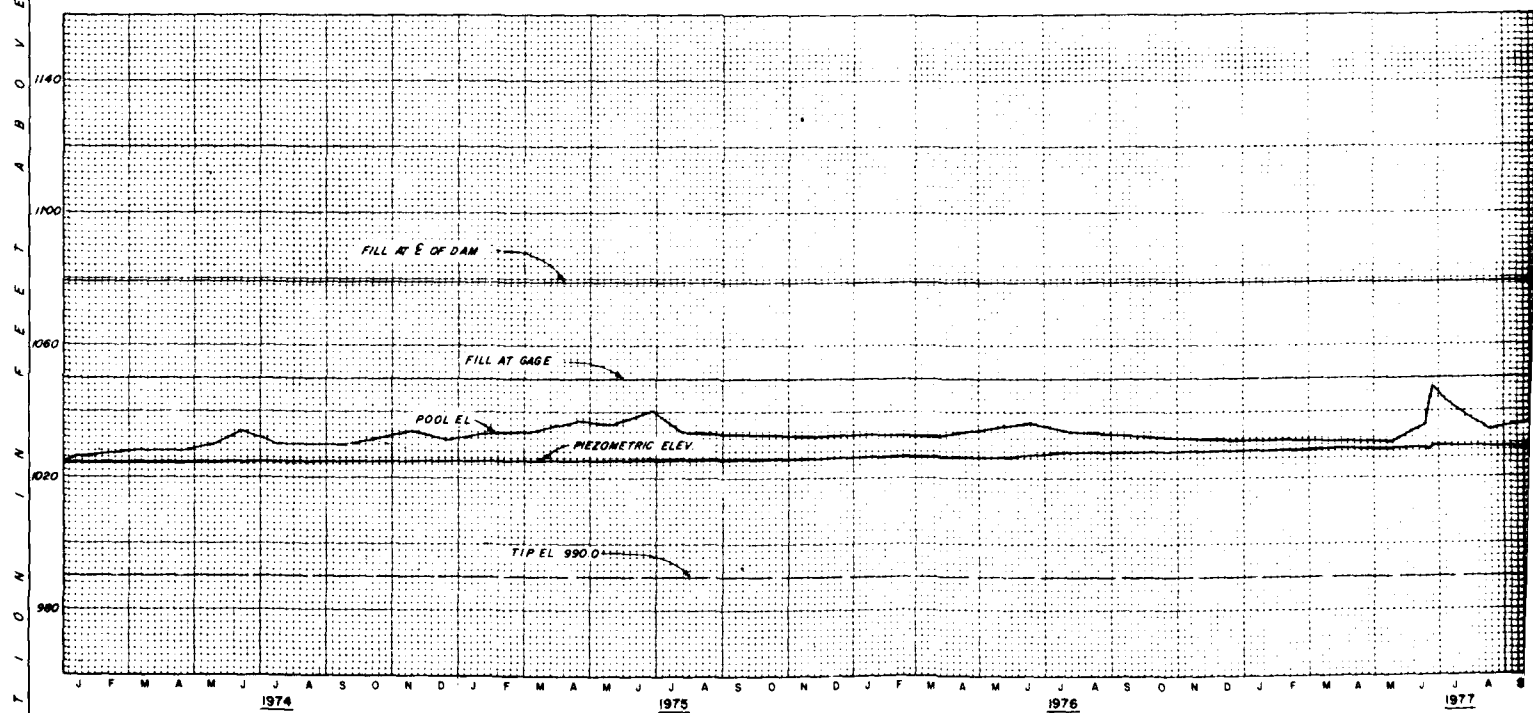
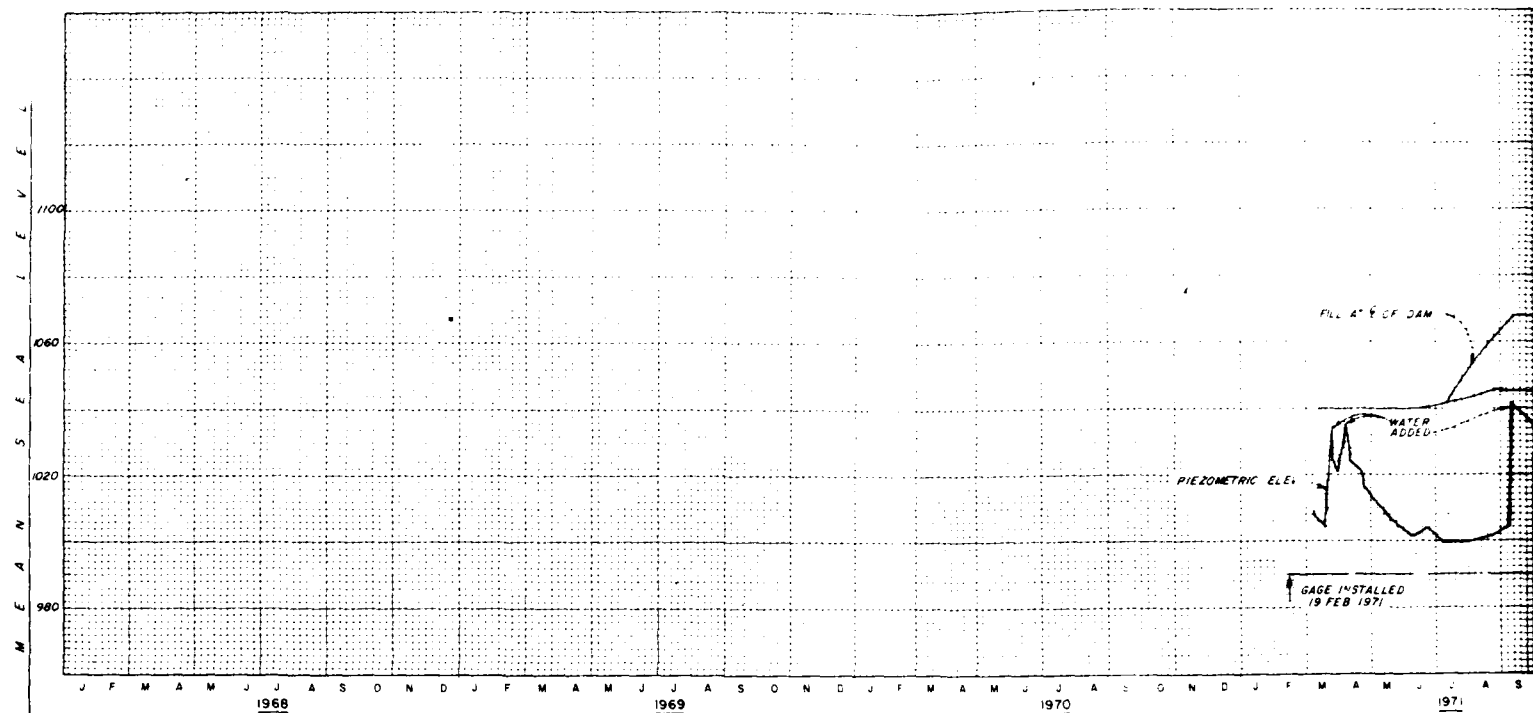


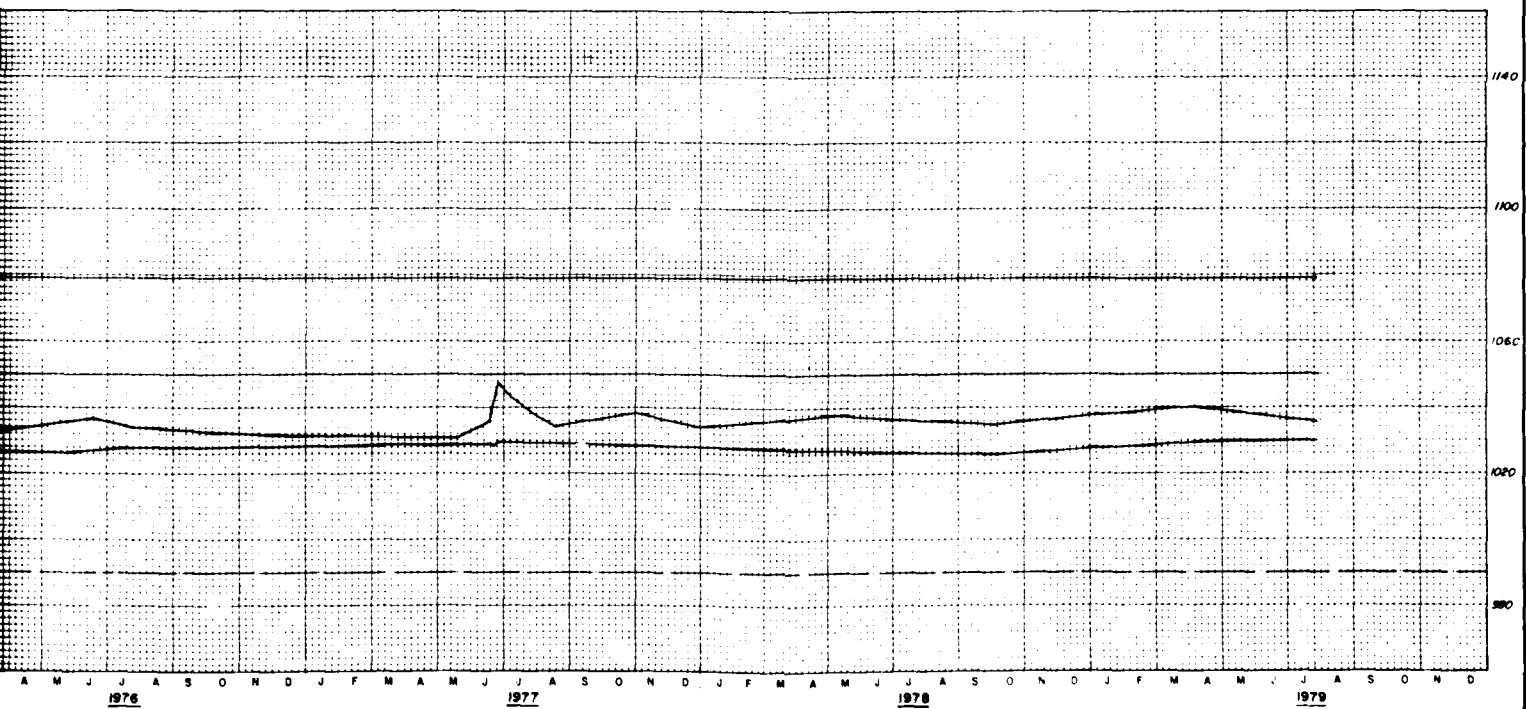
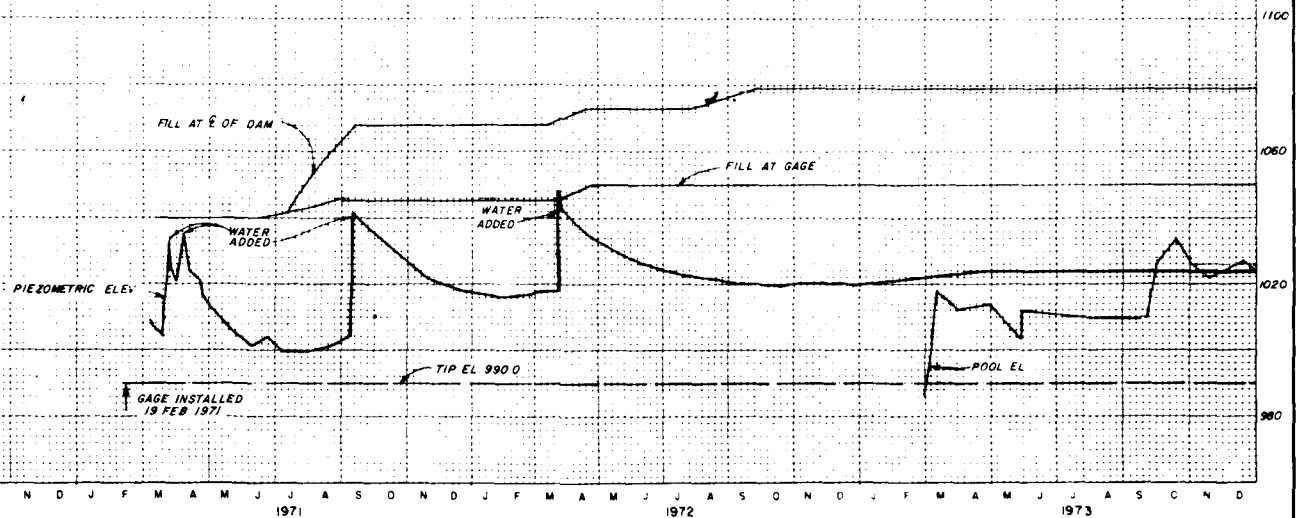
NOTE
NOT READ FOR THIS REPORT
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MARAI DES CYGNES RIVER KANSAS
MELVERN LAKE
INSTRUMENTATION PLOTS
EP 45-5 (GLOETZL CELL)

In 1 sheet

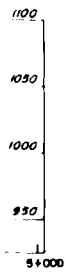
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CORPS OF ENGINEERS U. S. ARMY
KANSAS CITY DISTRICT
FILE NO. 0-5-1271
AUGUST 1975

Scale as shown





DOWNSTREAM



LEGEND
 OPEN TUBE ○
 PNEUMATIC CELLS ●

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MELVERN LAKE

INSTRUMENTATION PLOTS
 PP-46-1 (OPEN TUBE)

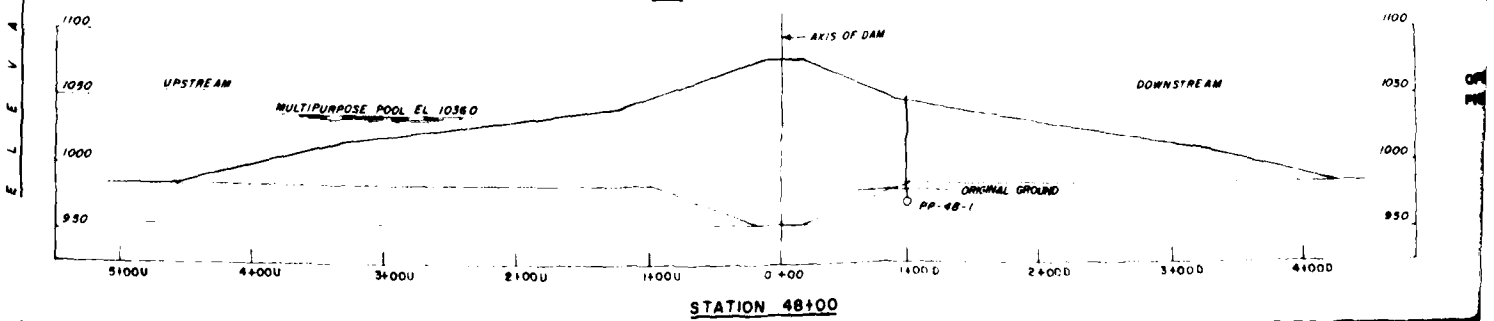
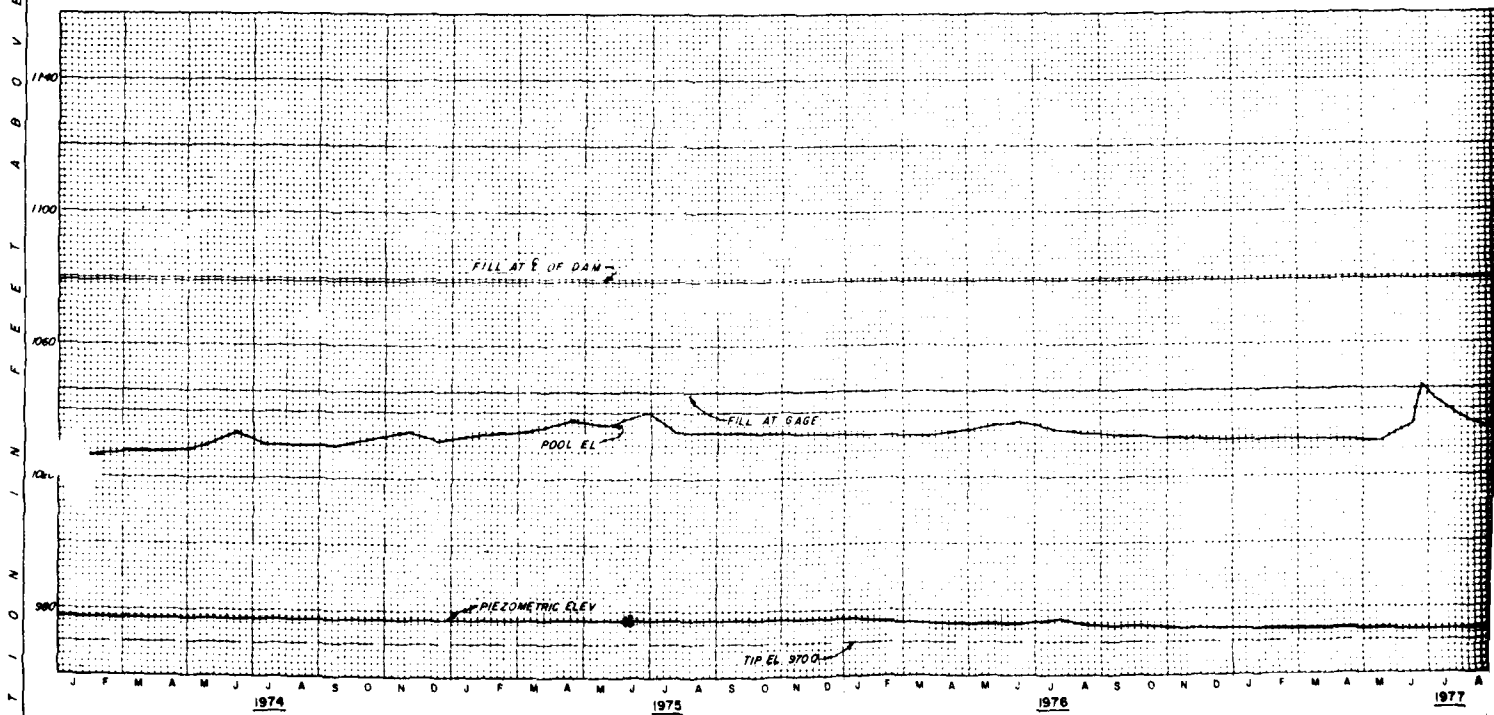
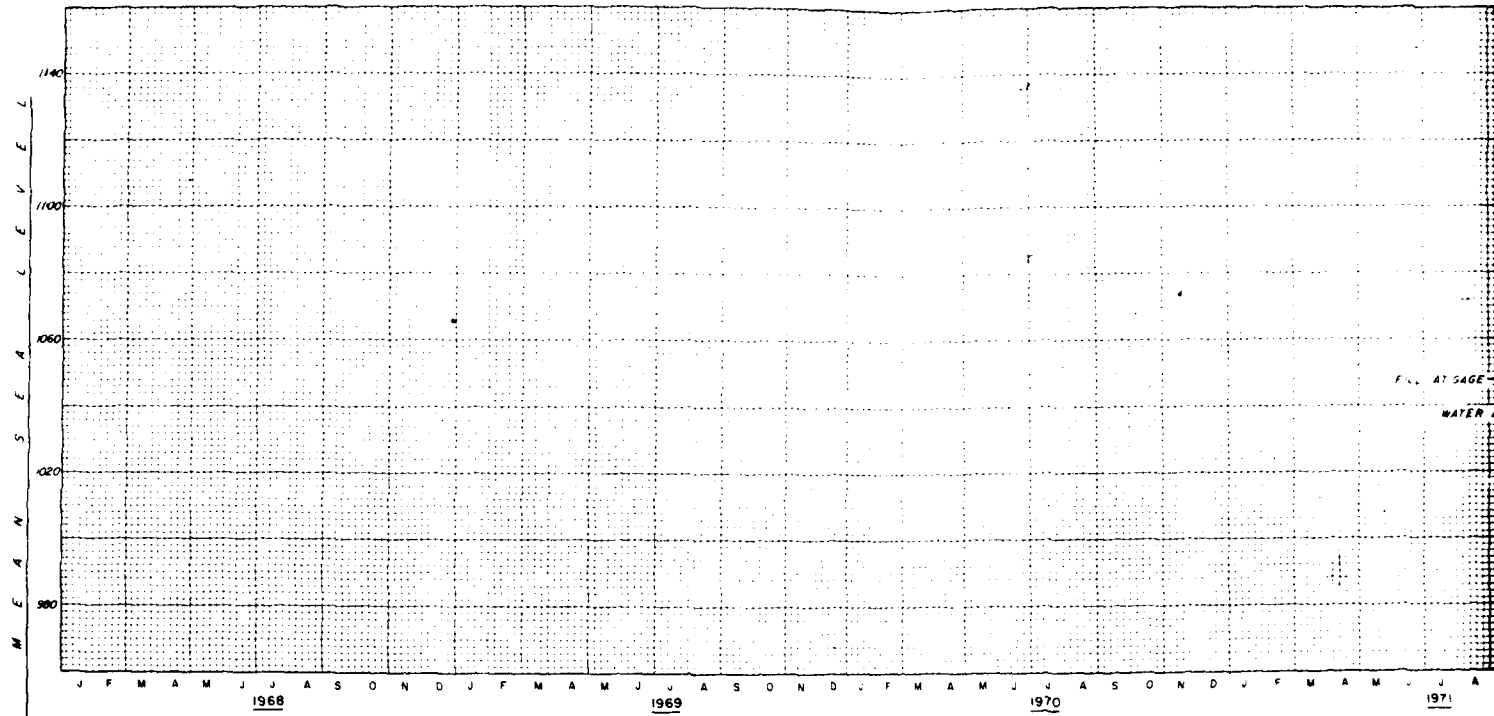
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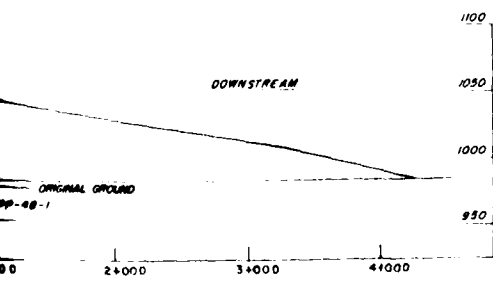
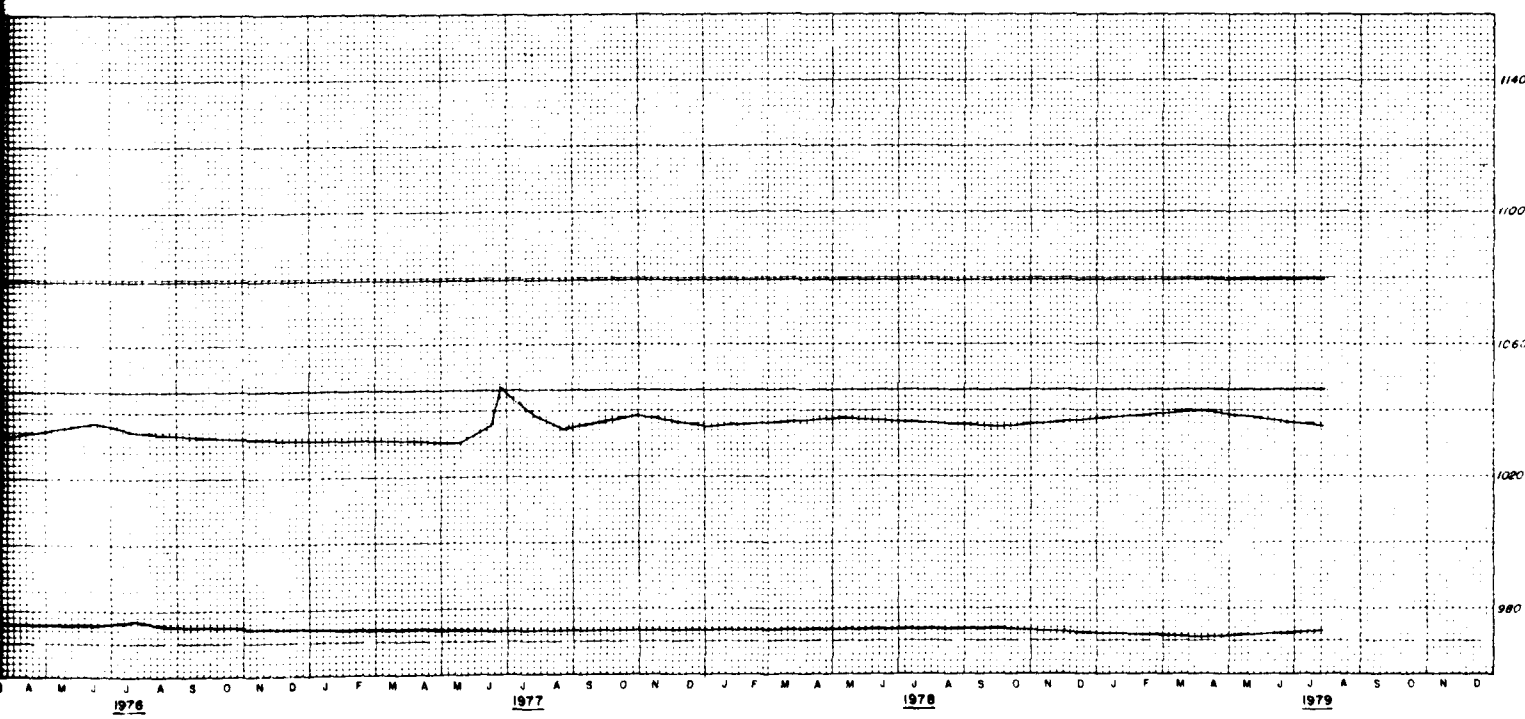
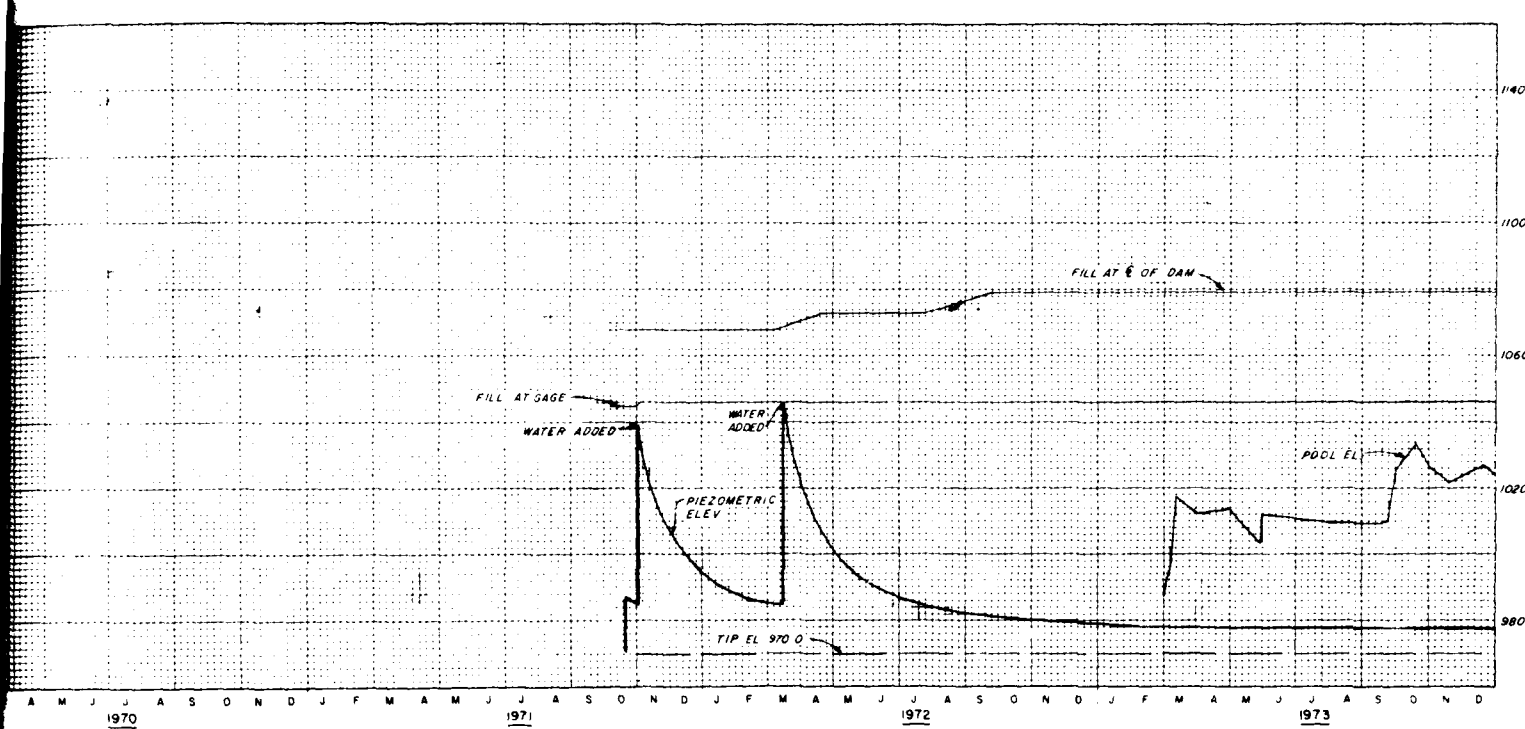
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Scale as shown

CORPS OF ENGINEERS U. S. ARMY
 KANSAS CITY DISTRICT

FILE NO 0-5-1272
 AUGUST 1975





LEGEND
 OPEN TUBE ○
 PNEUMATIC CELL ●

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MELVERN LAKE

INSTRUMENTATION PLOTS
 PP-48-1 (OPEN TUBE)

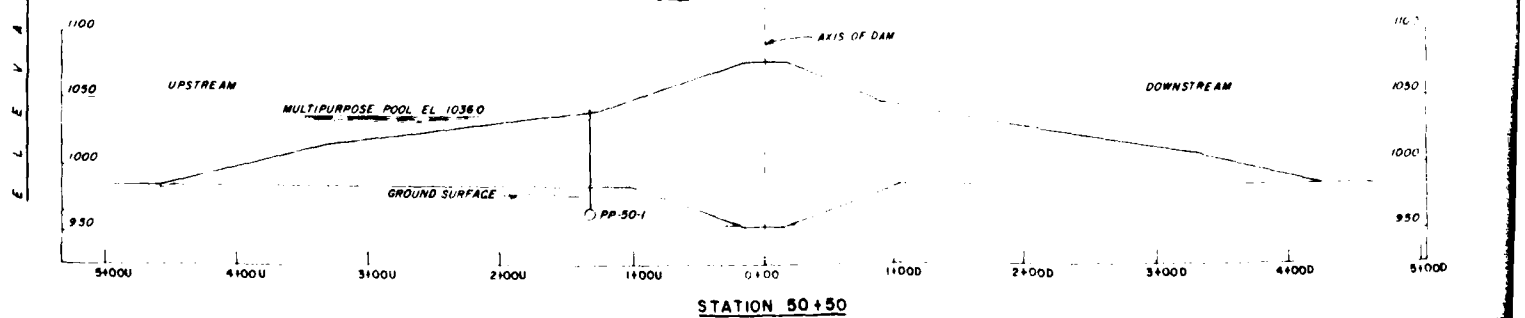
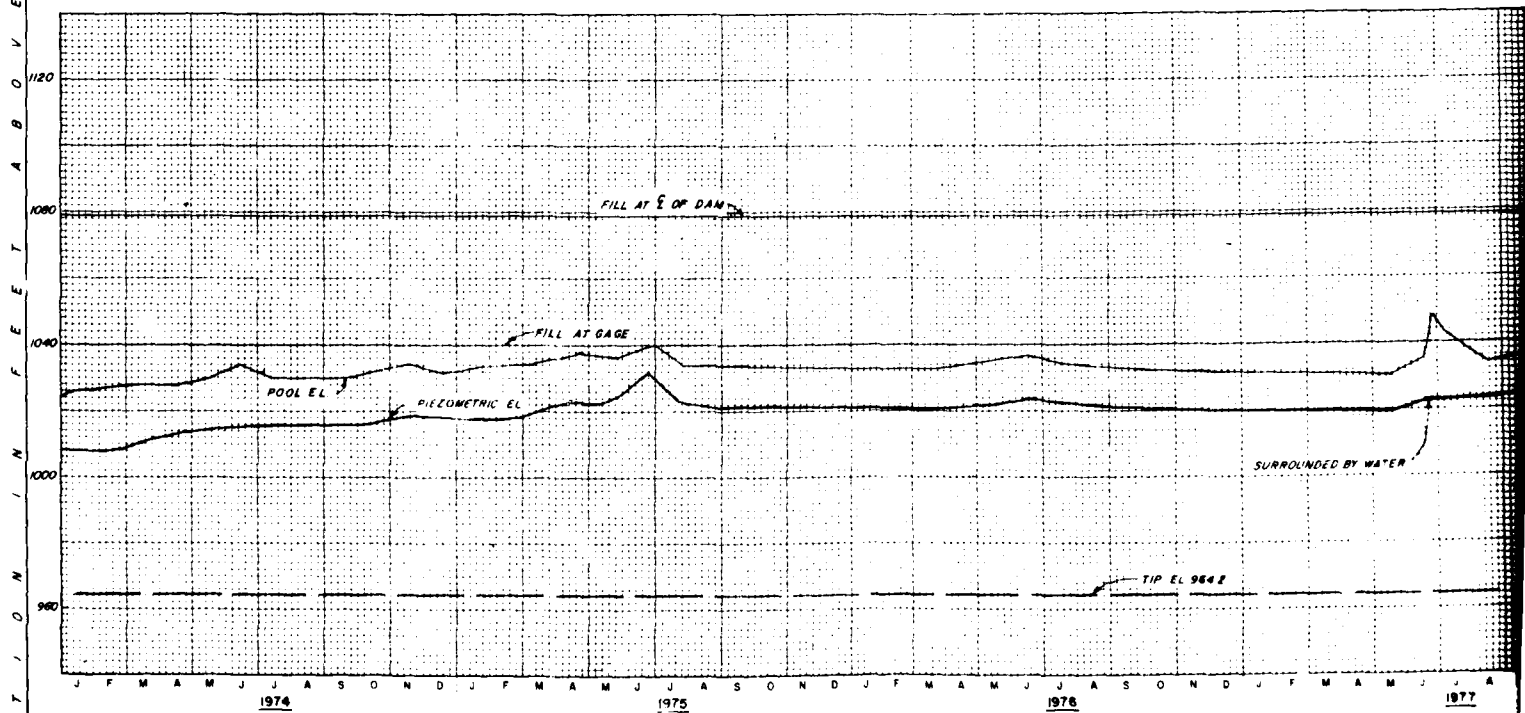
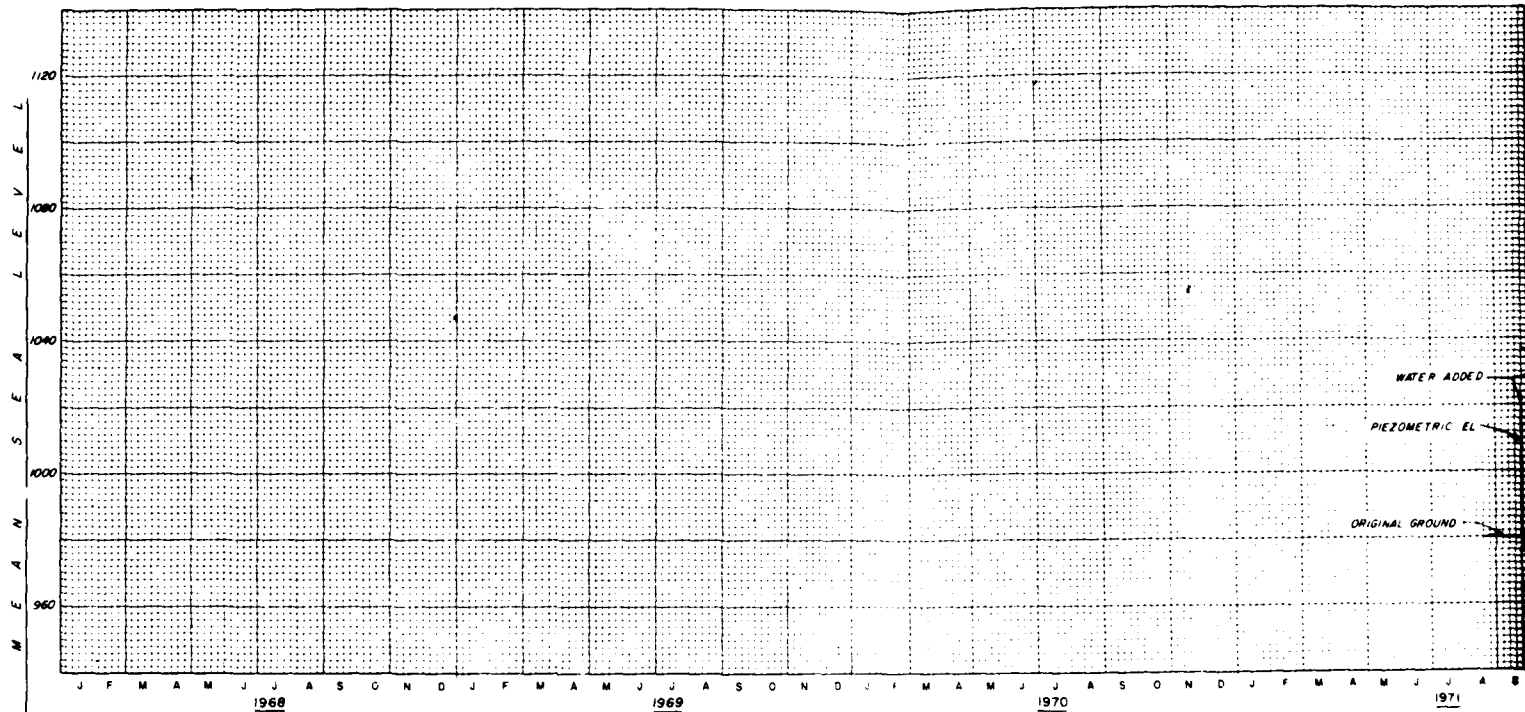
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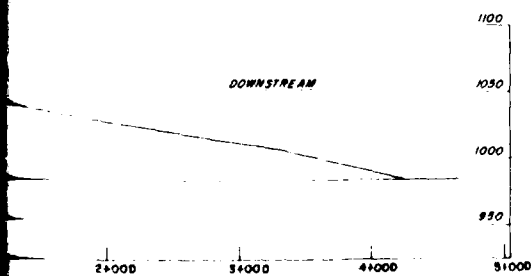
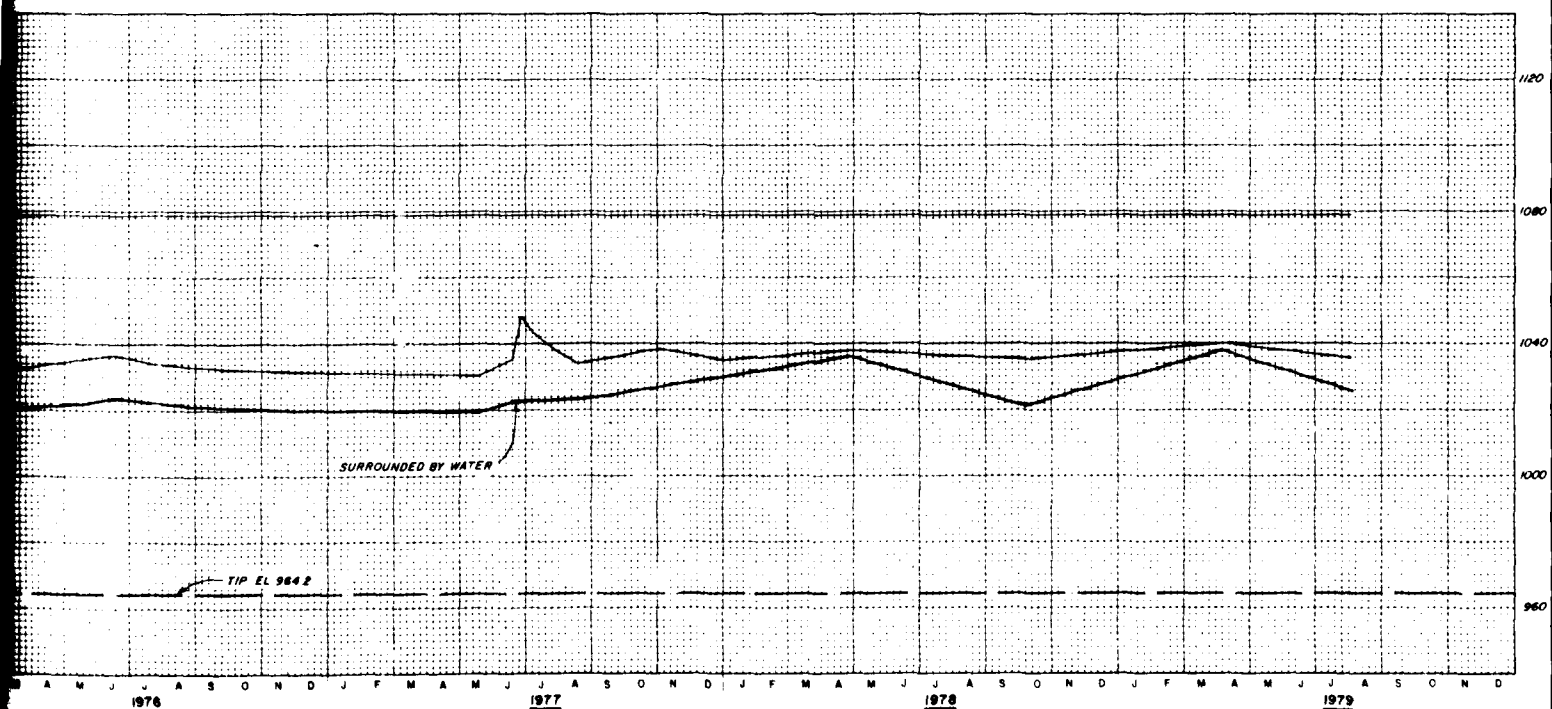
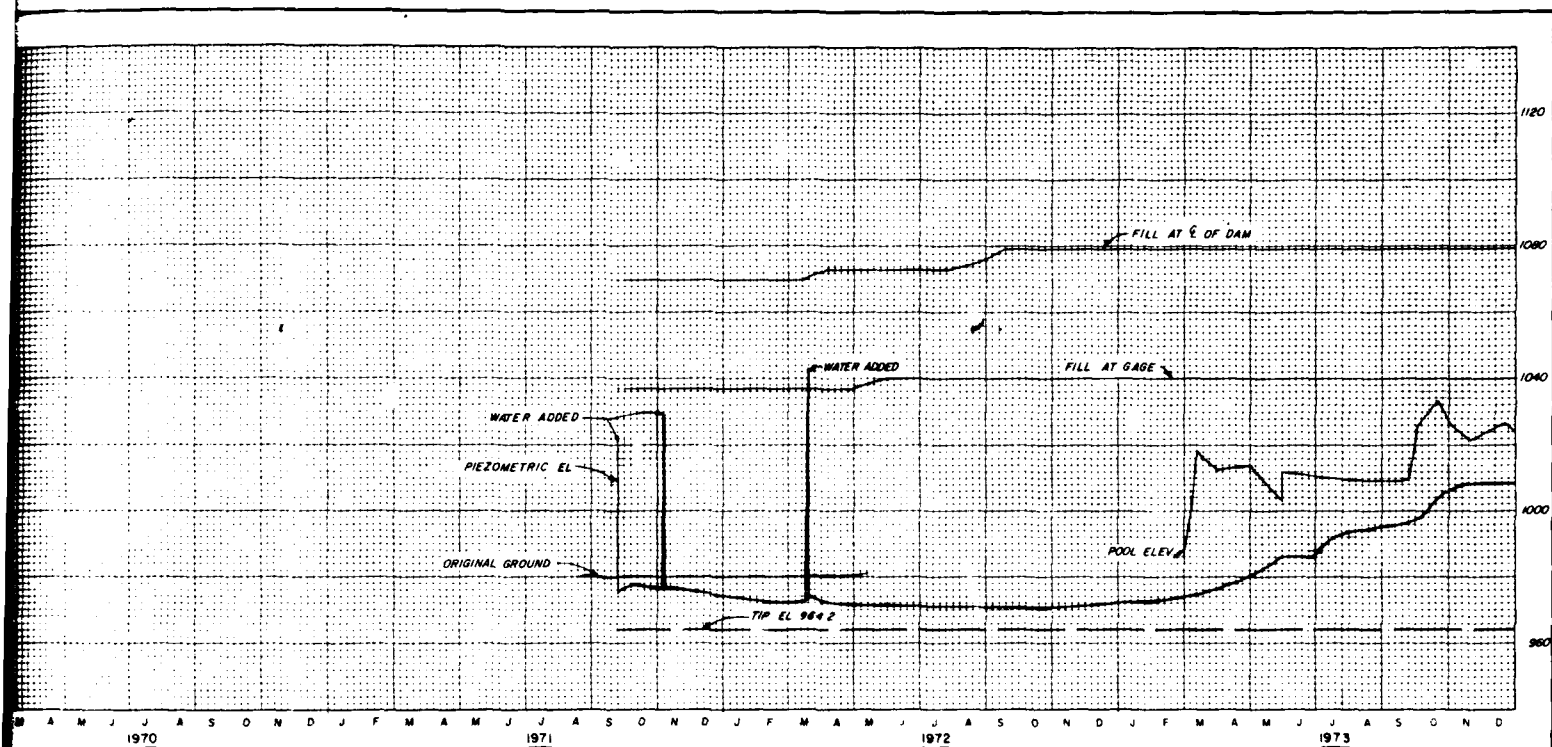
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Scale as shown

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 KANSAS CITY DISTRICT

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 AUGUST 1975





LEGEND
 OPEN TUBE ○
 PNEUMATIC CELLS ●

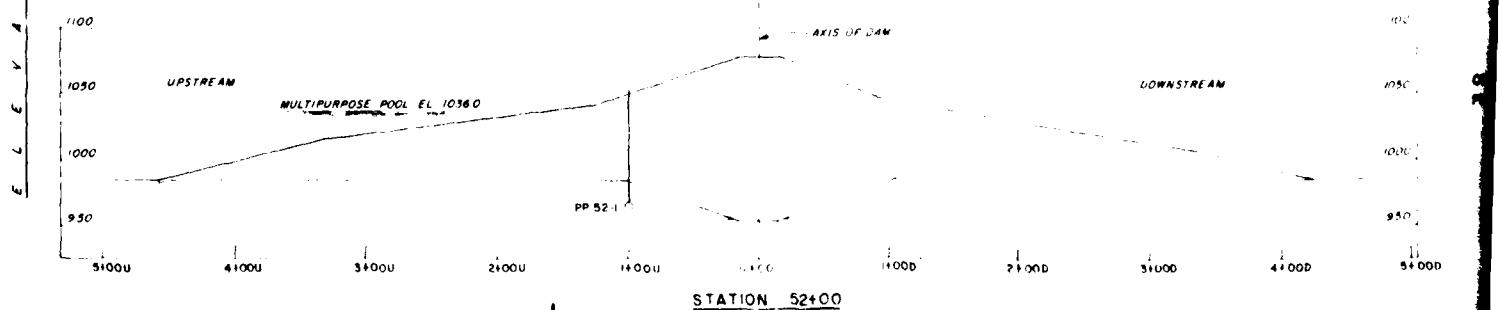
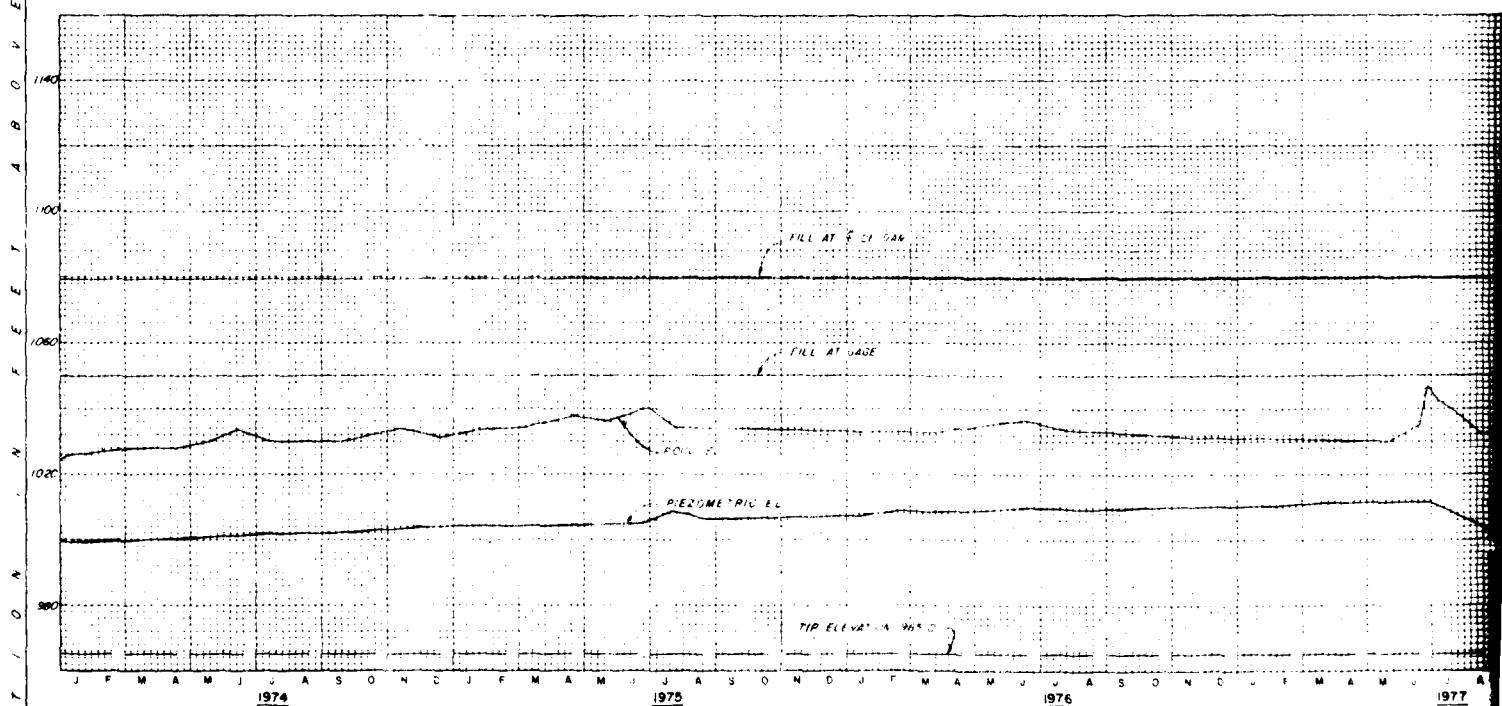
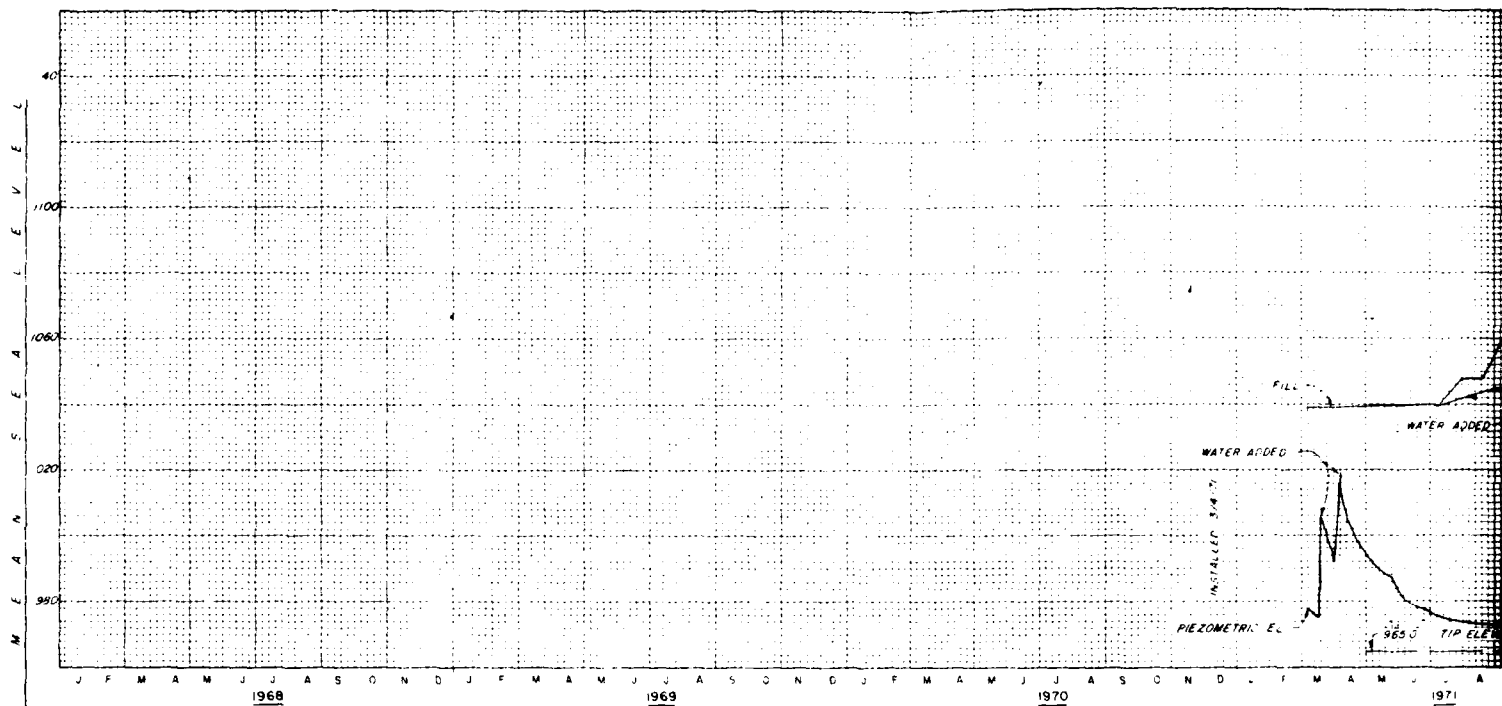
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MELVERN LAKE

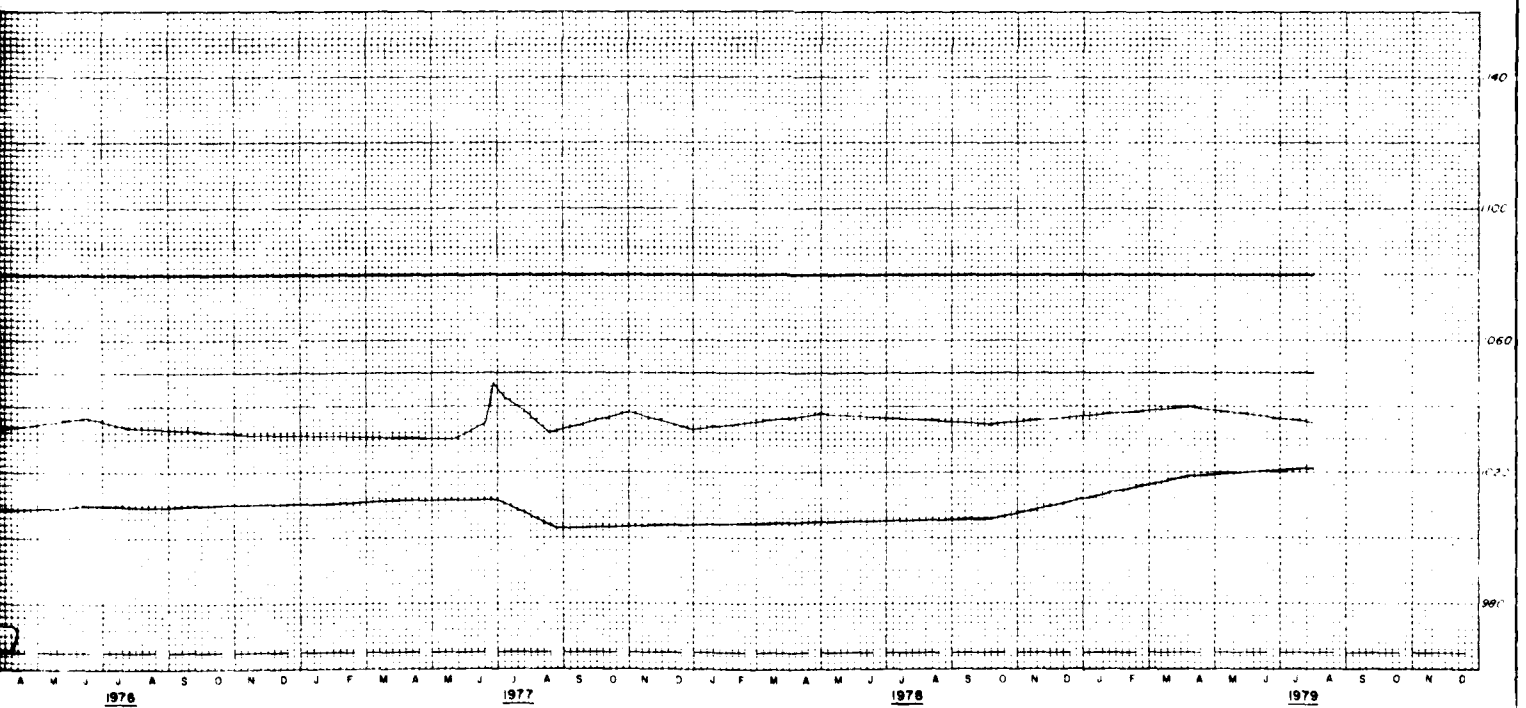
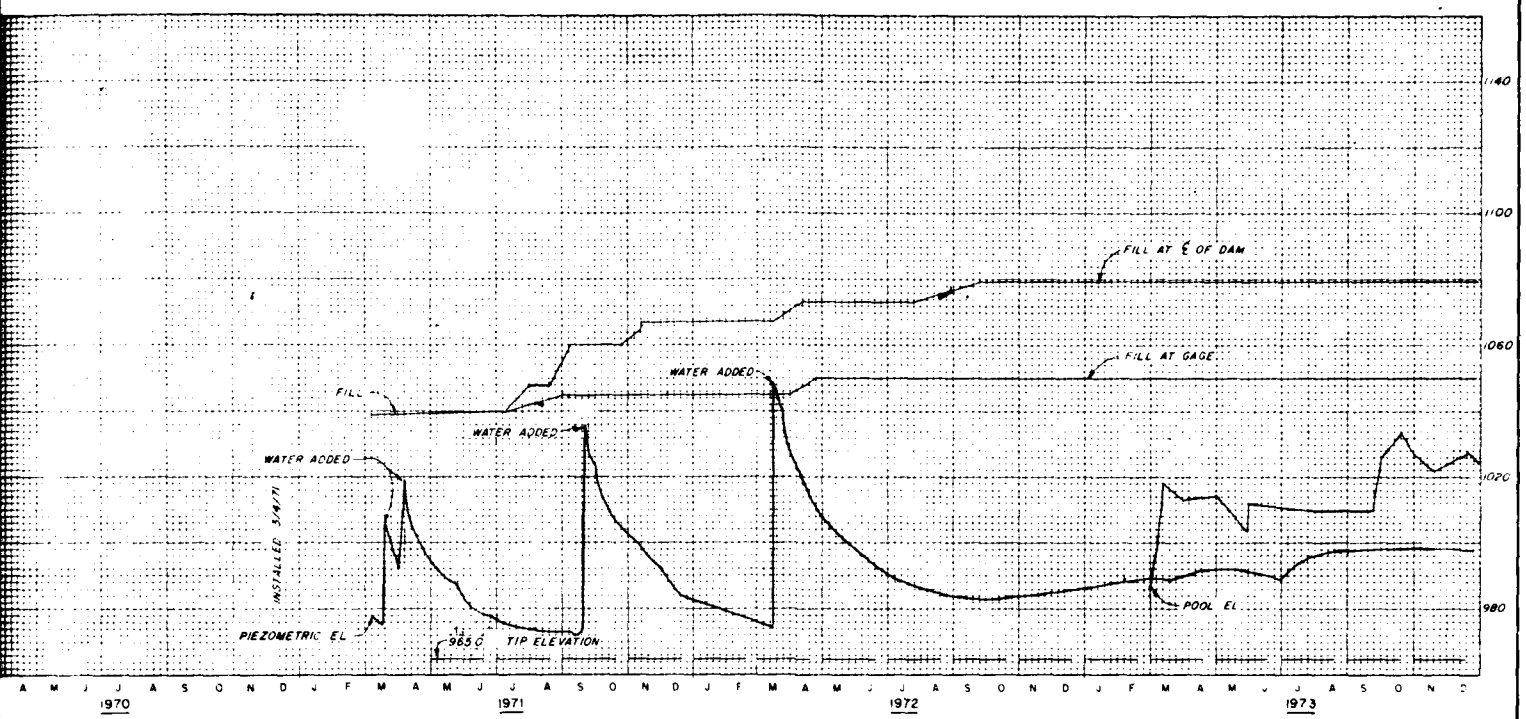
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 PP-50-1 (OPEN TUBE)

In 1 sheet

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 KANSAS CITY DISTRICT
 FILE NO. 0-5-1274
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Scale as shown





DOWNSTREAM

LEGEND

- OPEN TUBE O
- PNEUMATIC CELL •

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MELVERN LAKE

INSTRUMENTATION PLOTS
 PP-52-1 (OPEN TUBE)

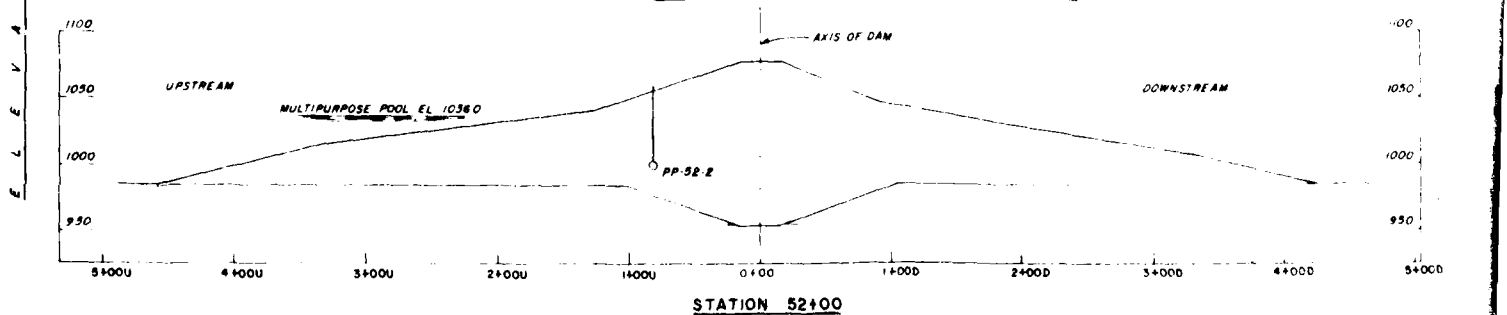
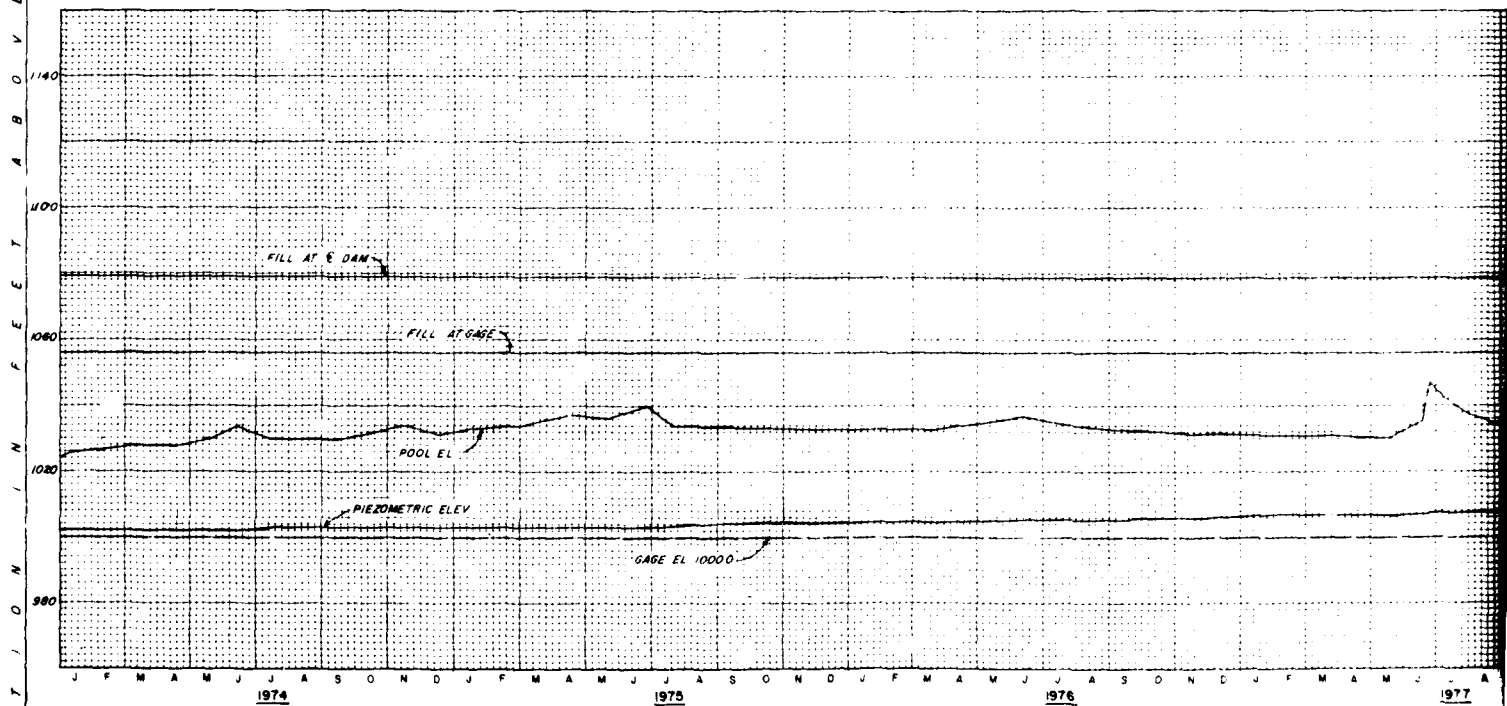
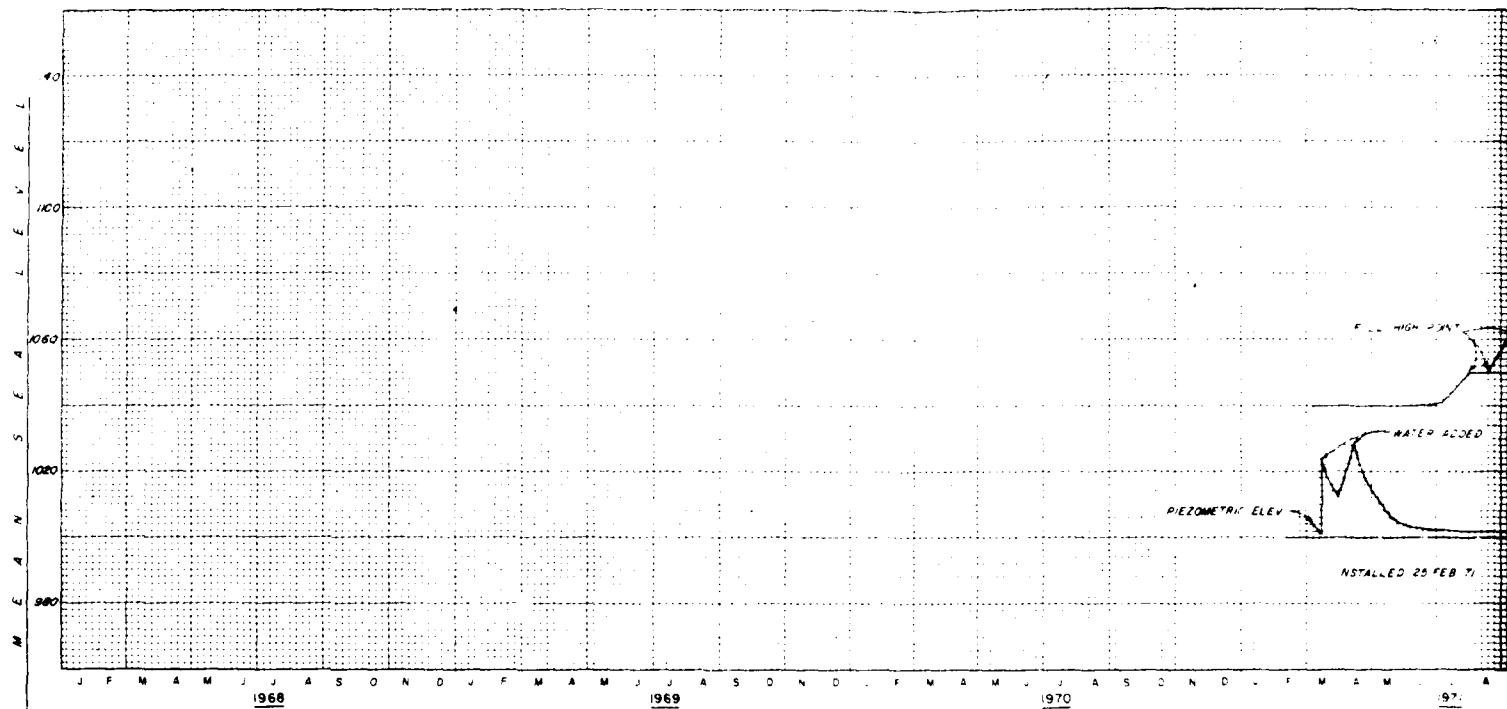
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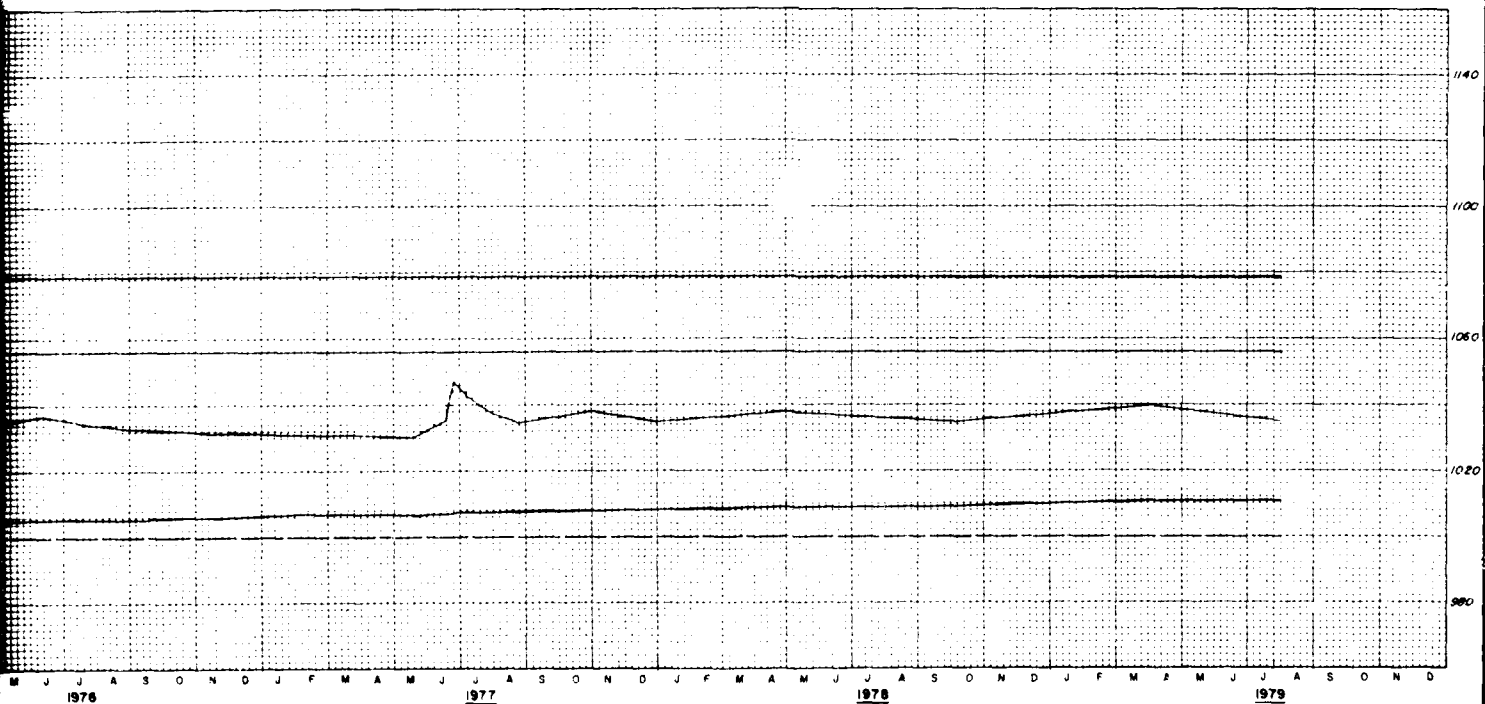
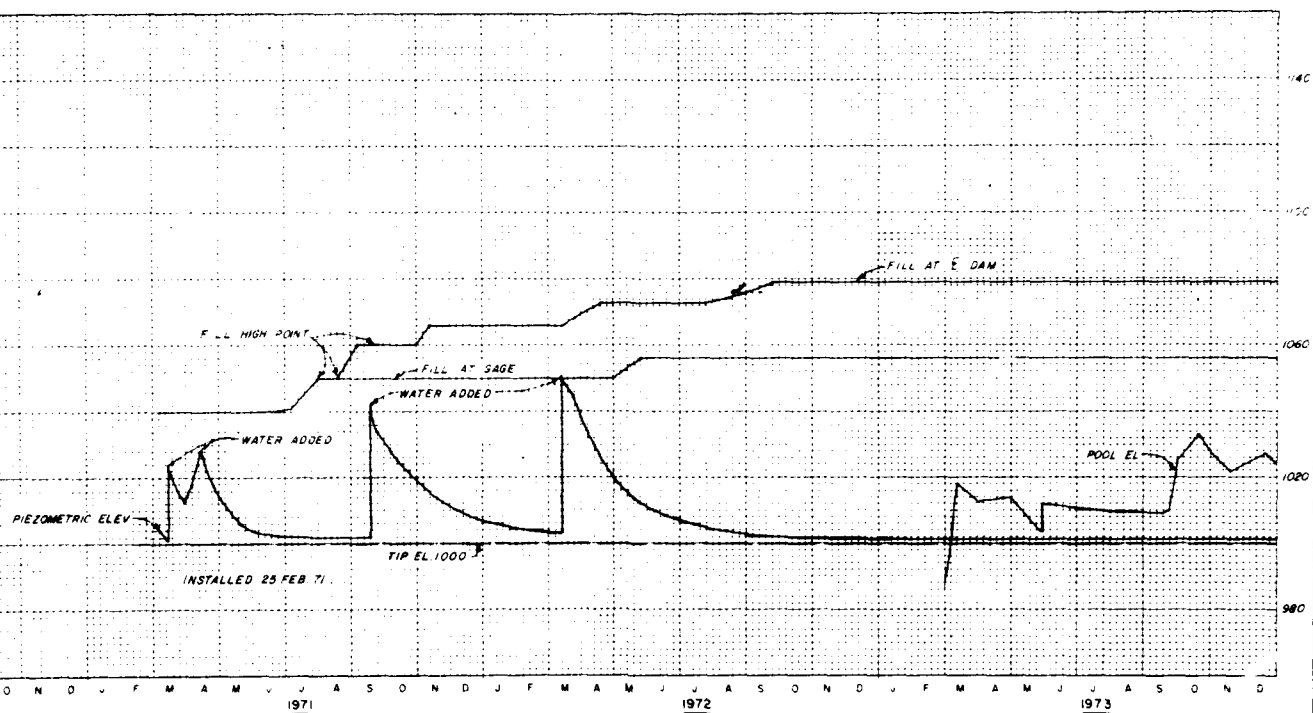
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Scale as shown

CORPS OF ENGINEERS, U.S. ARMY
 KANSAS CITY DISTRICT

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 AUGUST 1975





DOWNSTREAM



LEGEND

OPEN TUBE ———— ○

PNEUMATIC CELL ———— ●

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MELVERN LAKE

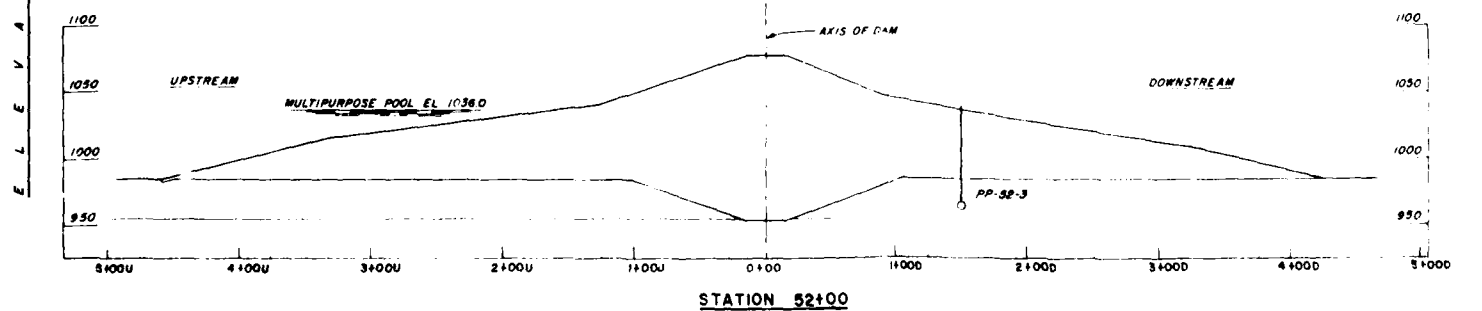
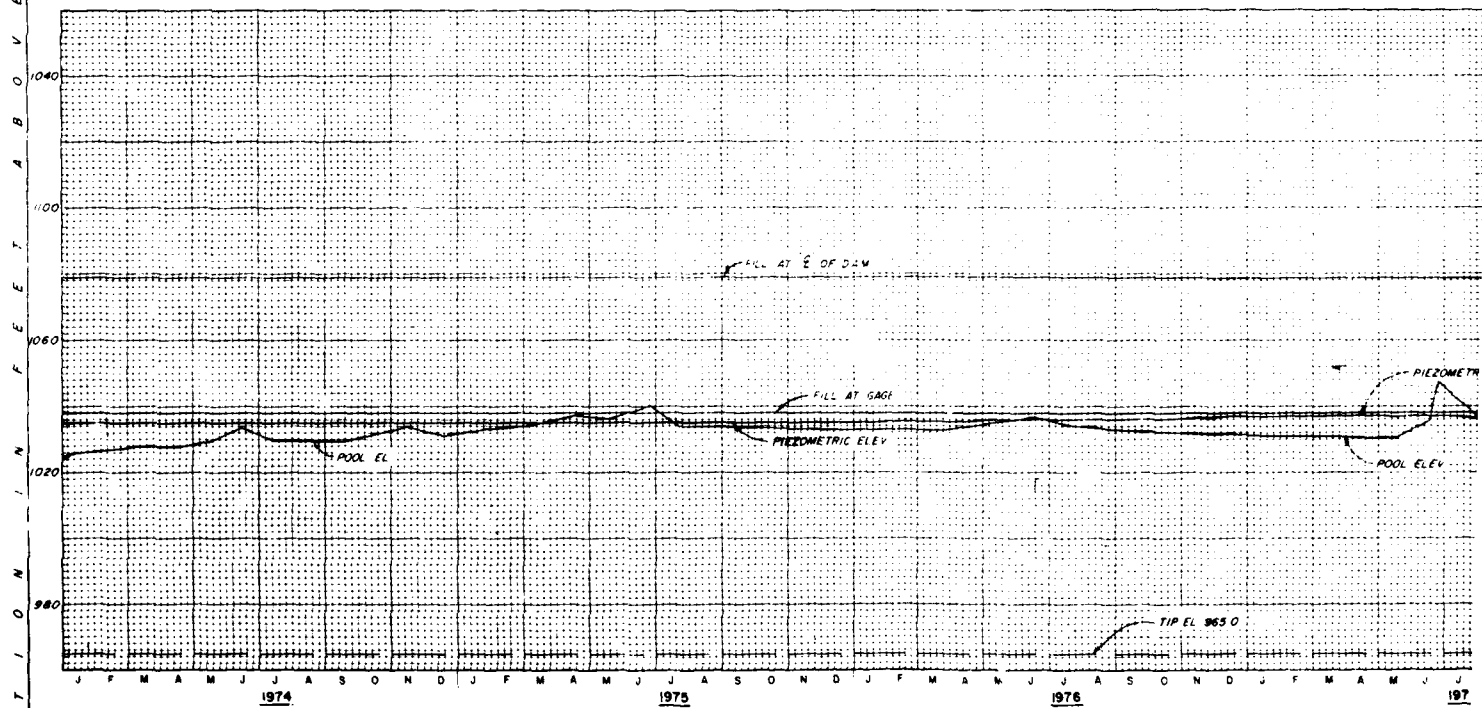
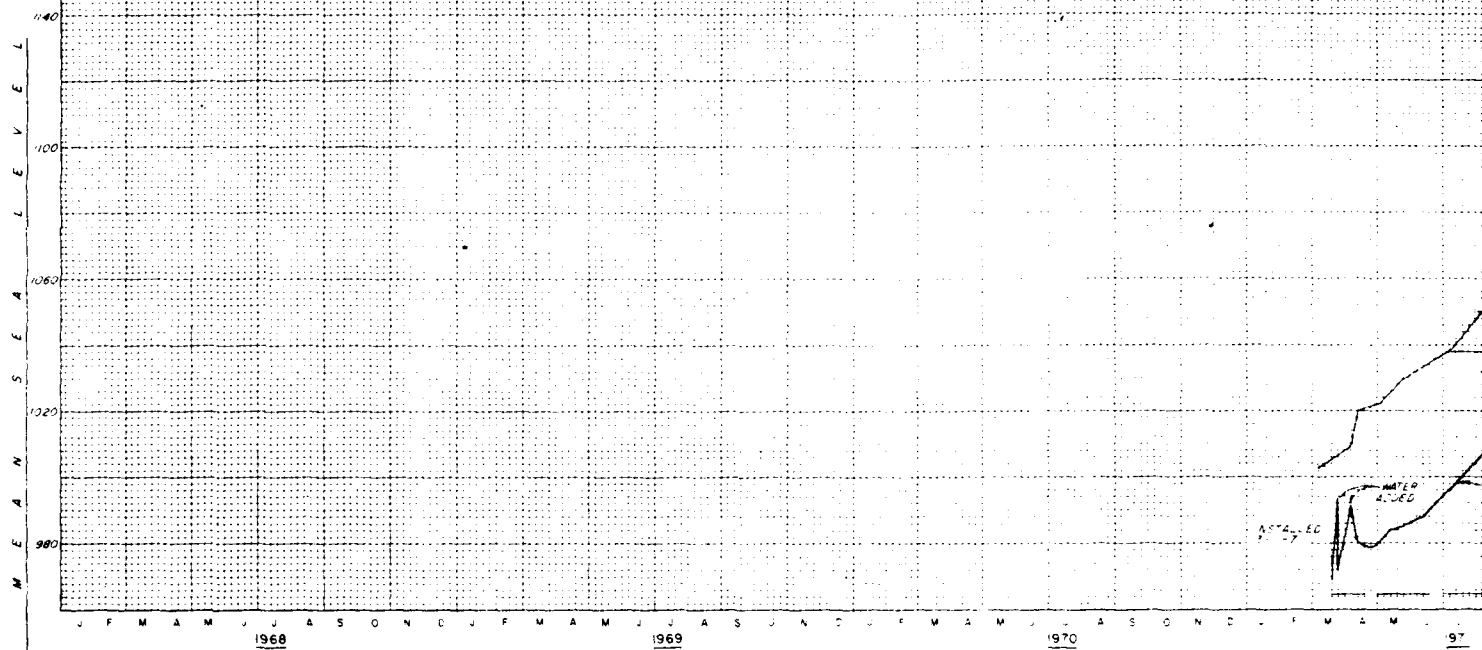
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PP-52-2 (OPEN TUBE)

In 1 sheet

Sheet No. 1
CORPS OF ENGINEERS U.S. ARMY
KANSAS CITY DISTRICT

Scale as shown

FILE NO. 0-5-1276
AUGUST 1975



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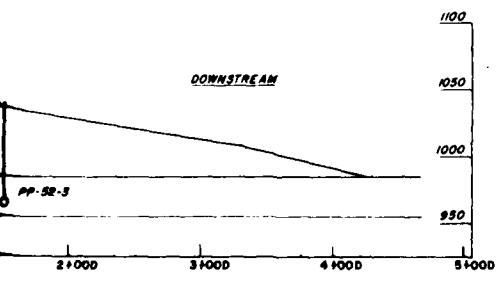
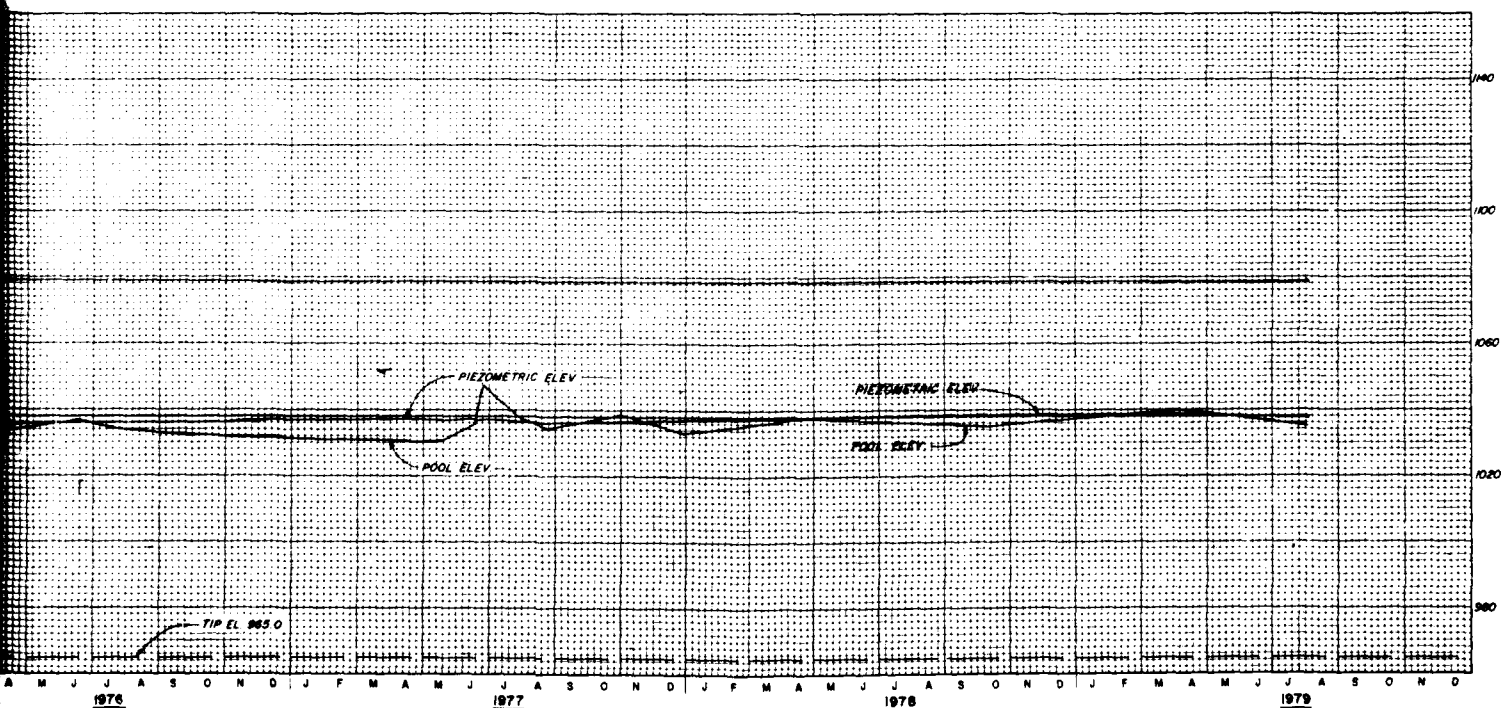
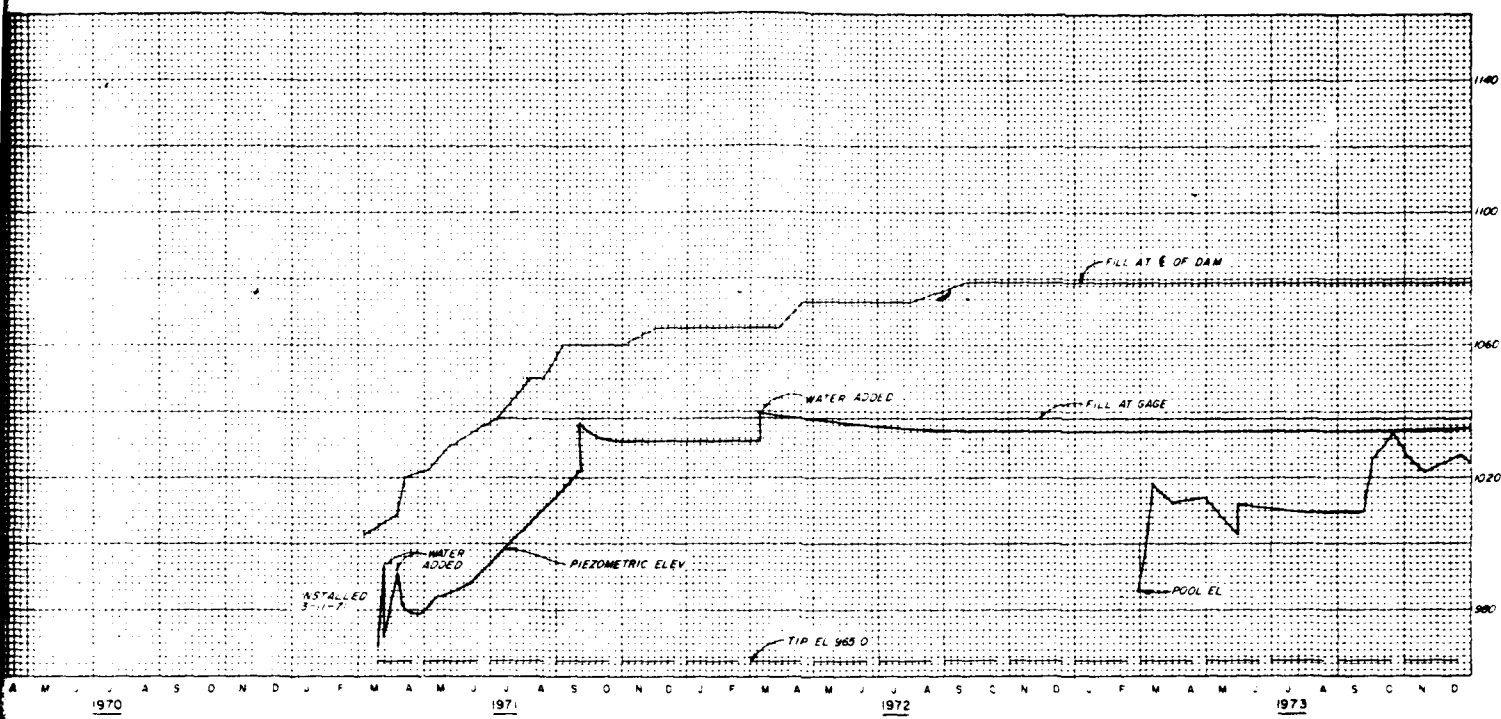
CORPS OF ENGINEERS KANSAS CITY MO KANSAS CITY DISTRICT F/6 13/2
OPERATION AND MAINTENANCE MANUAL, MELVERN LAKE, MARAIS DES CYGN--ETC(U)
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LEGEND
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 PNEUMATIC CELL ——— ●

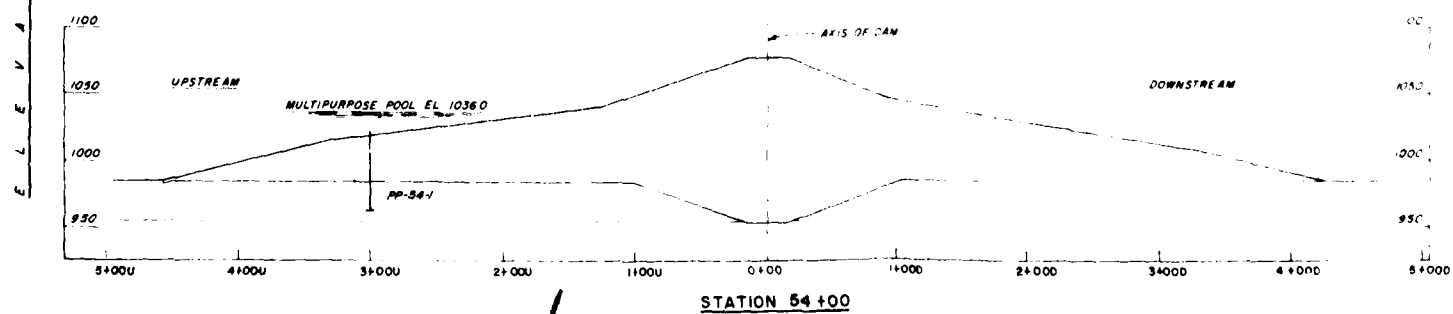
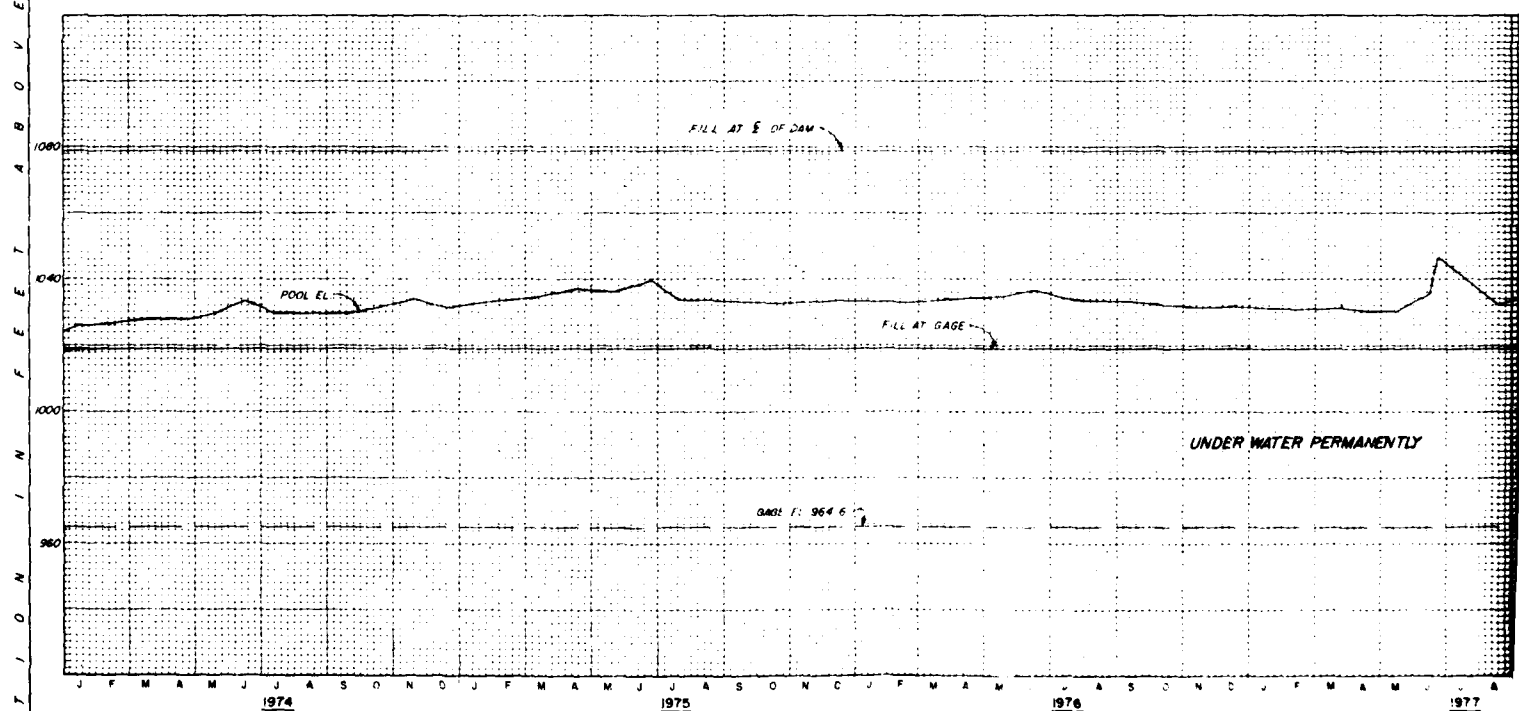
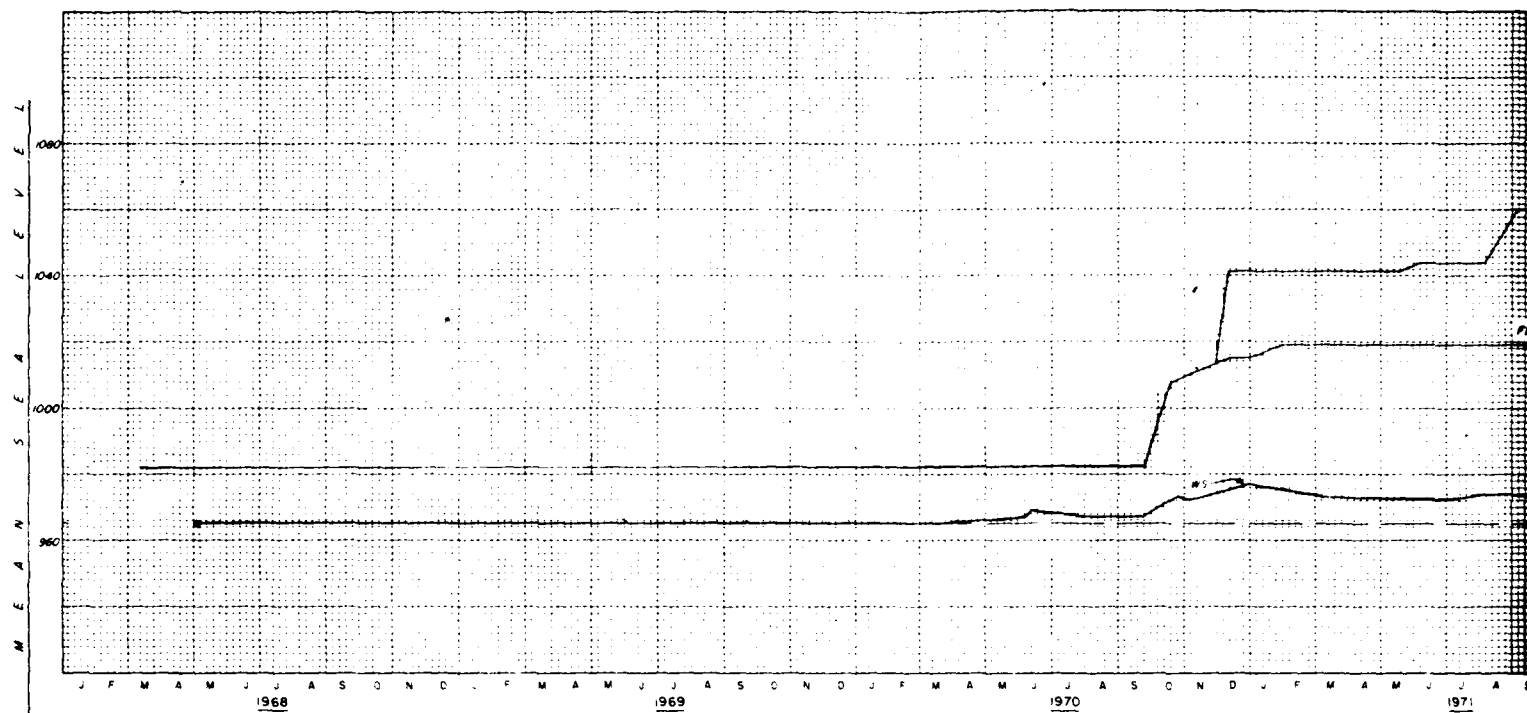
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 MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

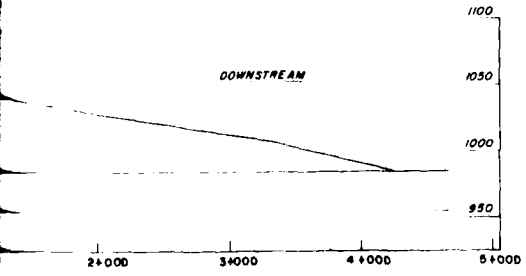
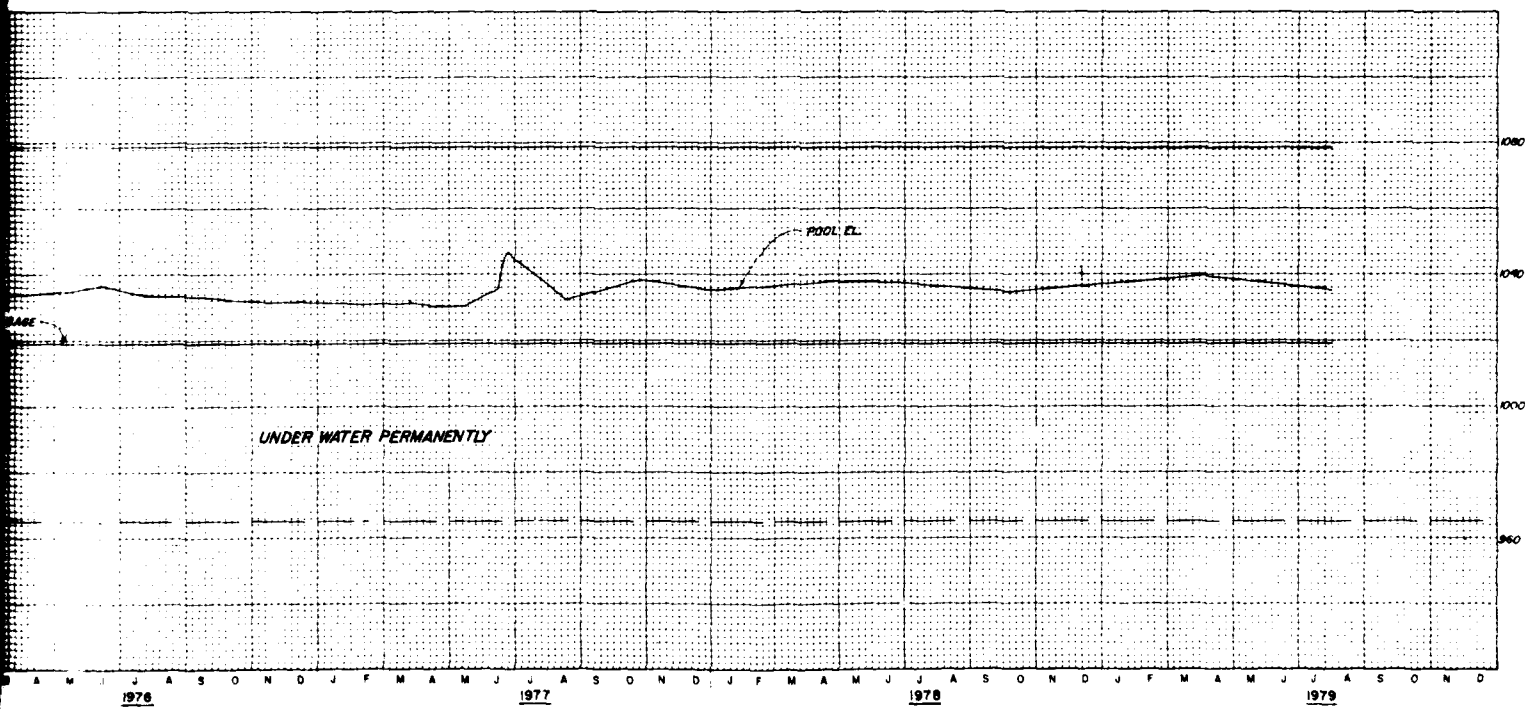
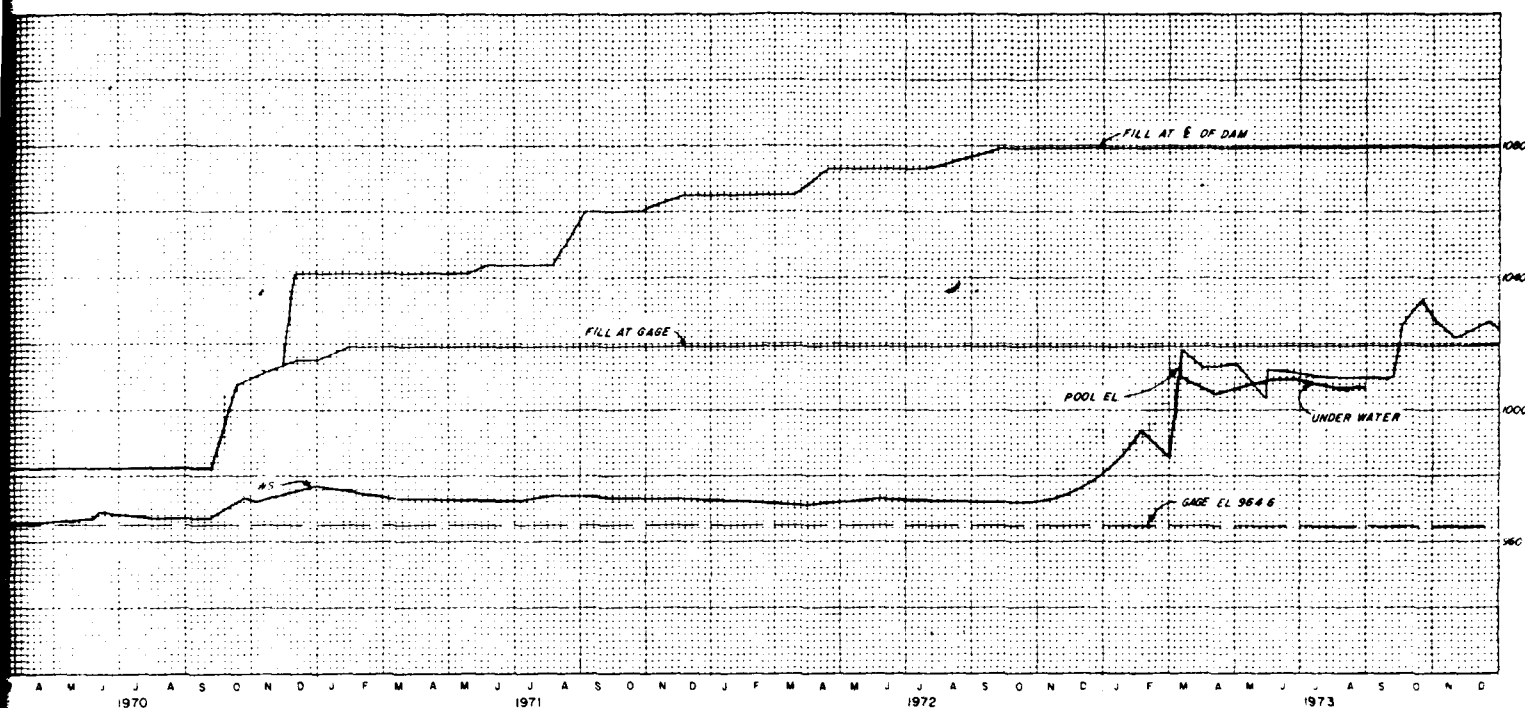
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In 1 sheet

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 KANSAS CITY DISTRICT
 FILE NO. O-5-1277
 AUGUST 1975

Scale as shown

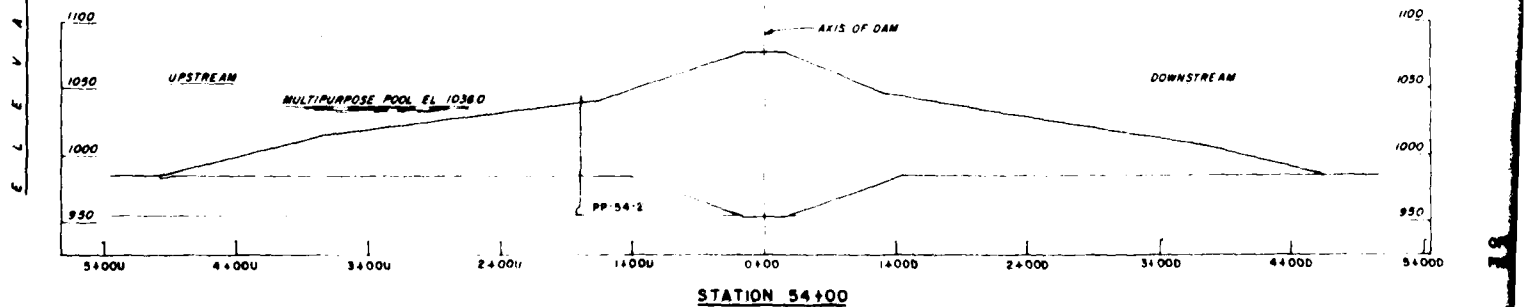
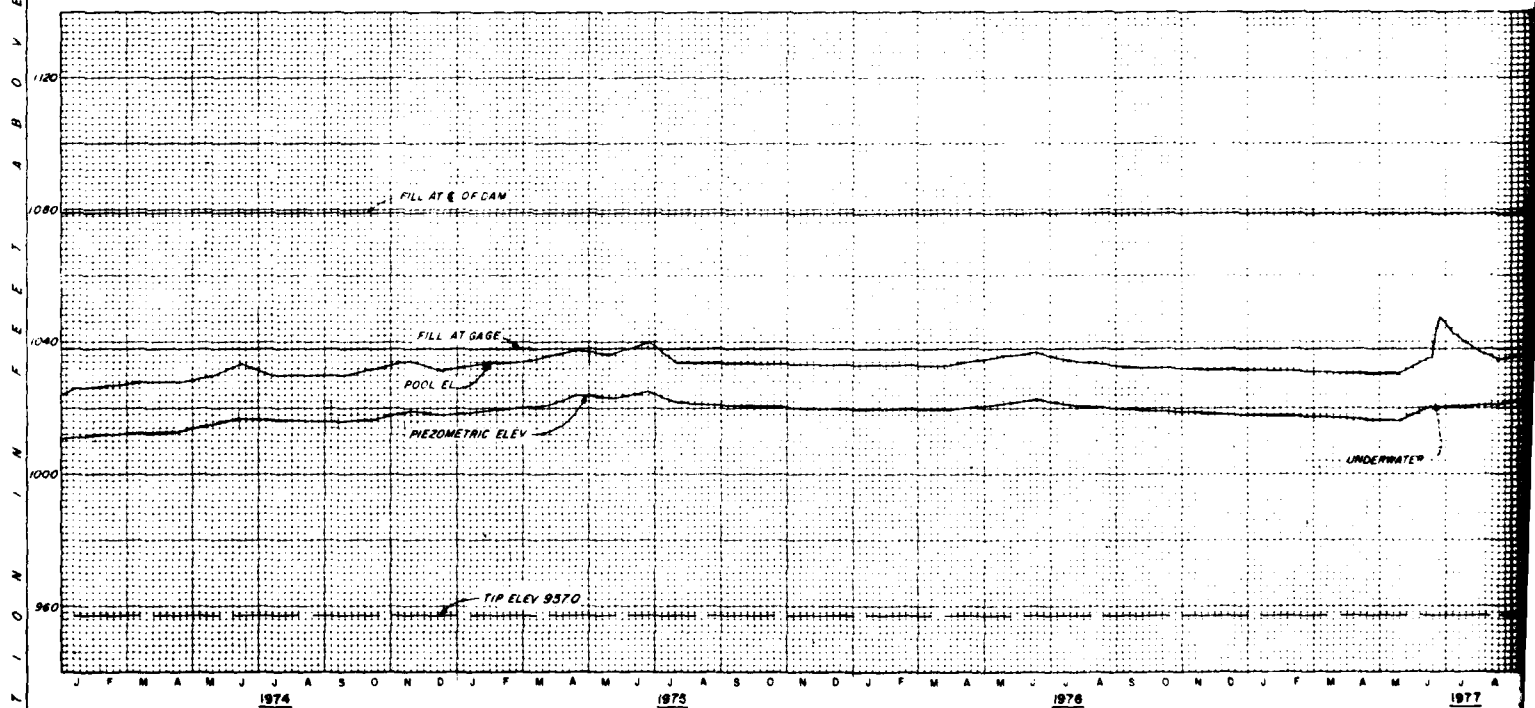
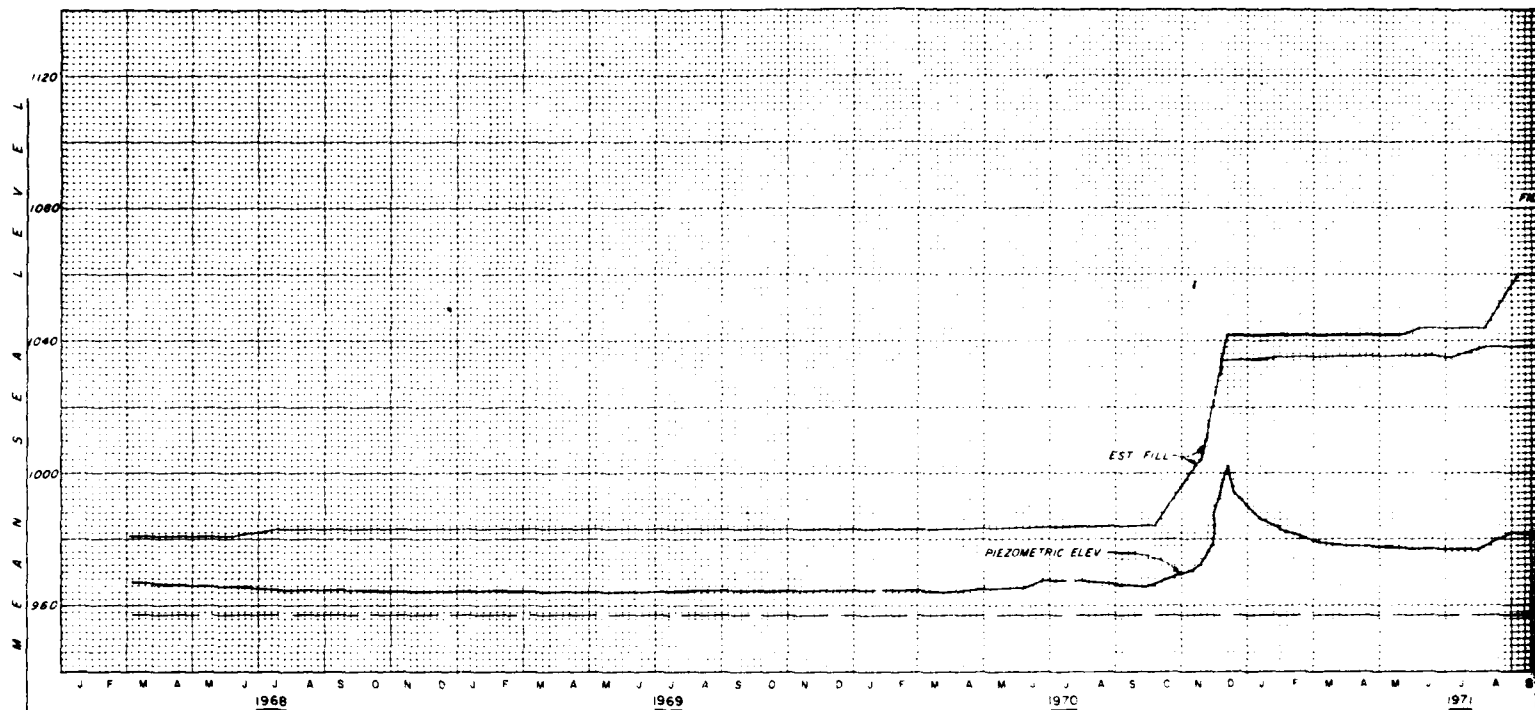


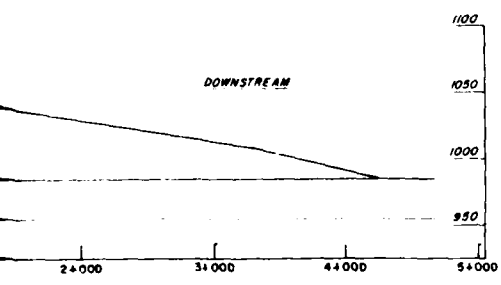
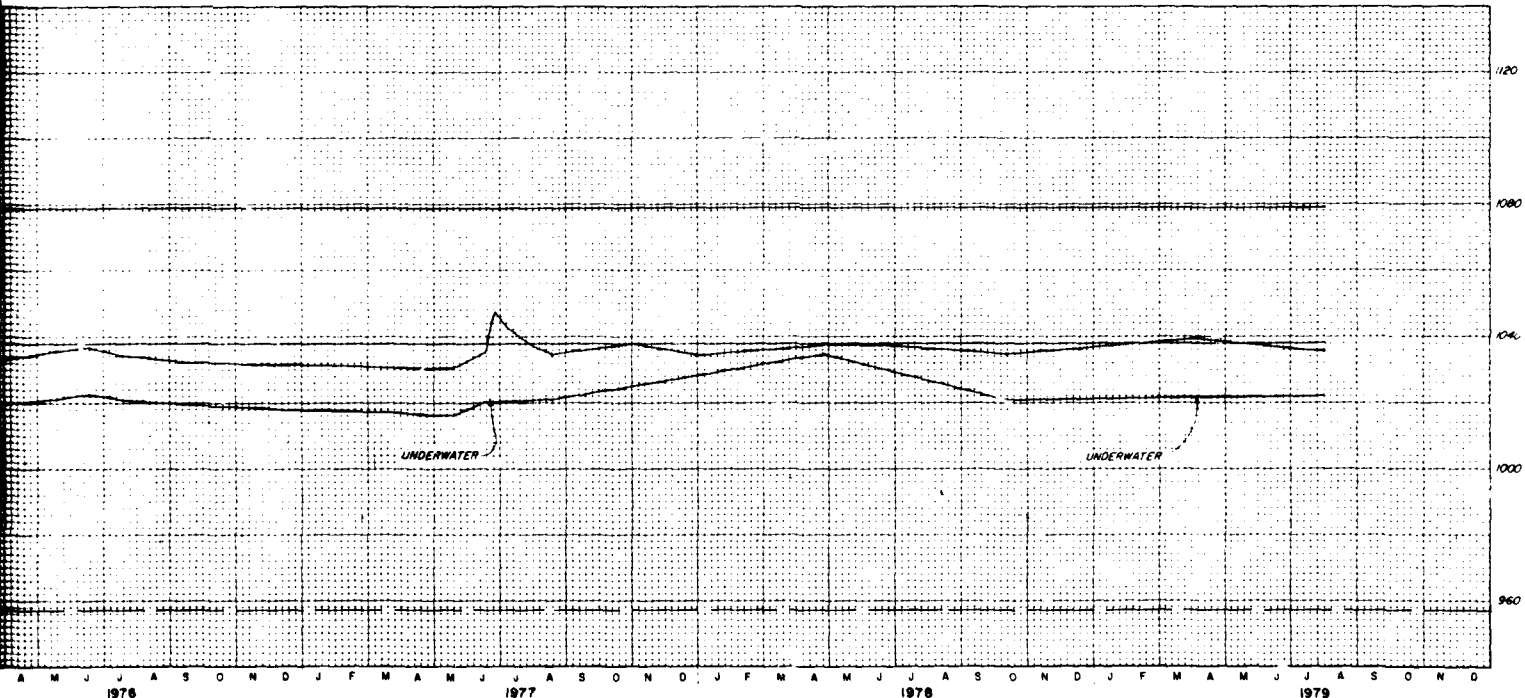
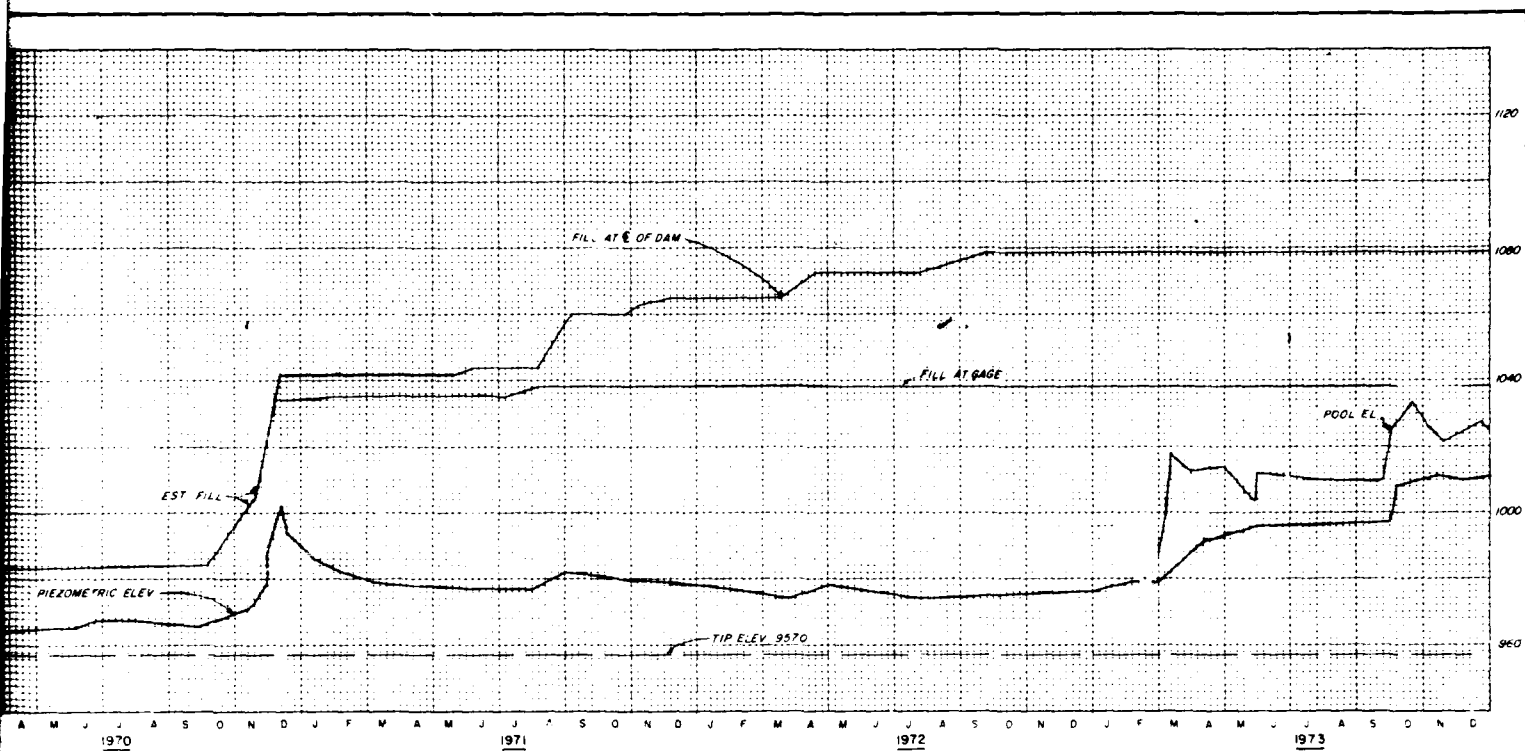


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MELVERN LAKE

INSTRUMENTATION PLOTS
 PP-54-1 (OPEN TUBE)

In 1 sheet
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 KANSAS CITY DISTRICT
 FILE NO. 0-5-1278
 AUGUST 1975





LEGEND
 OPEN TUBE ———— ○
 PNEUMATIC CELL ———— ●

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MELVERN LAKE

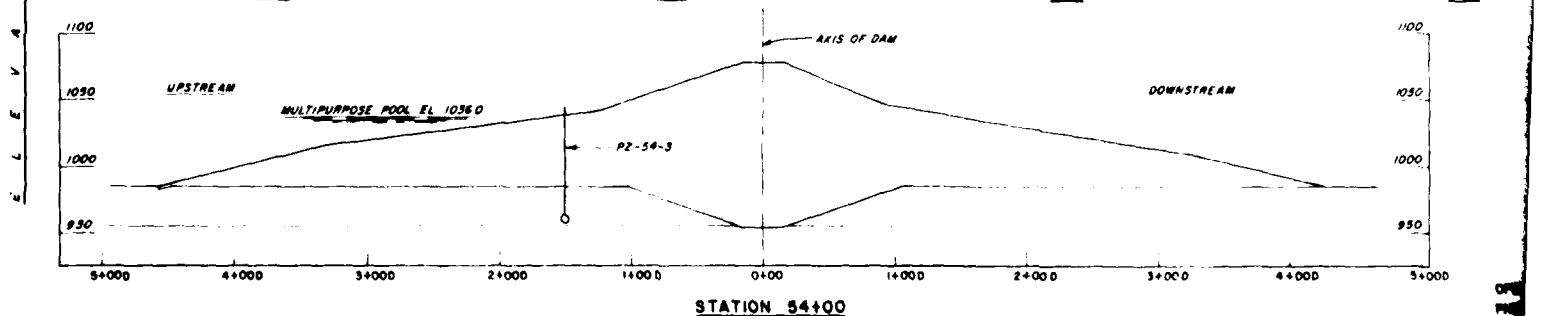
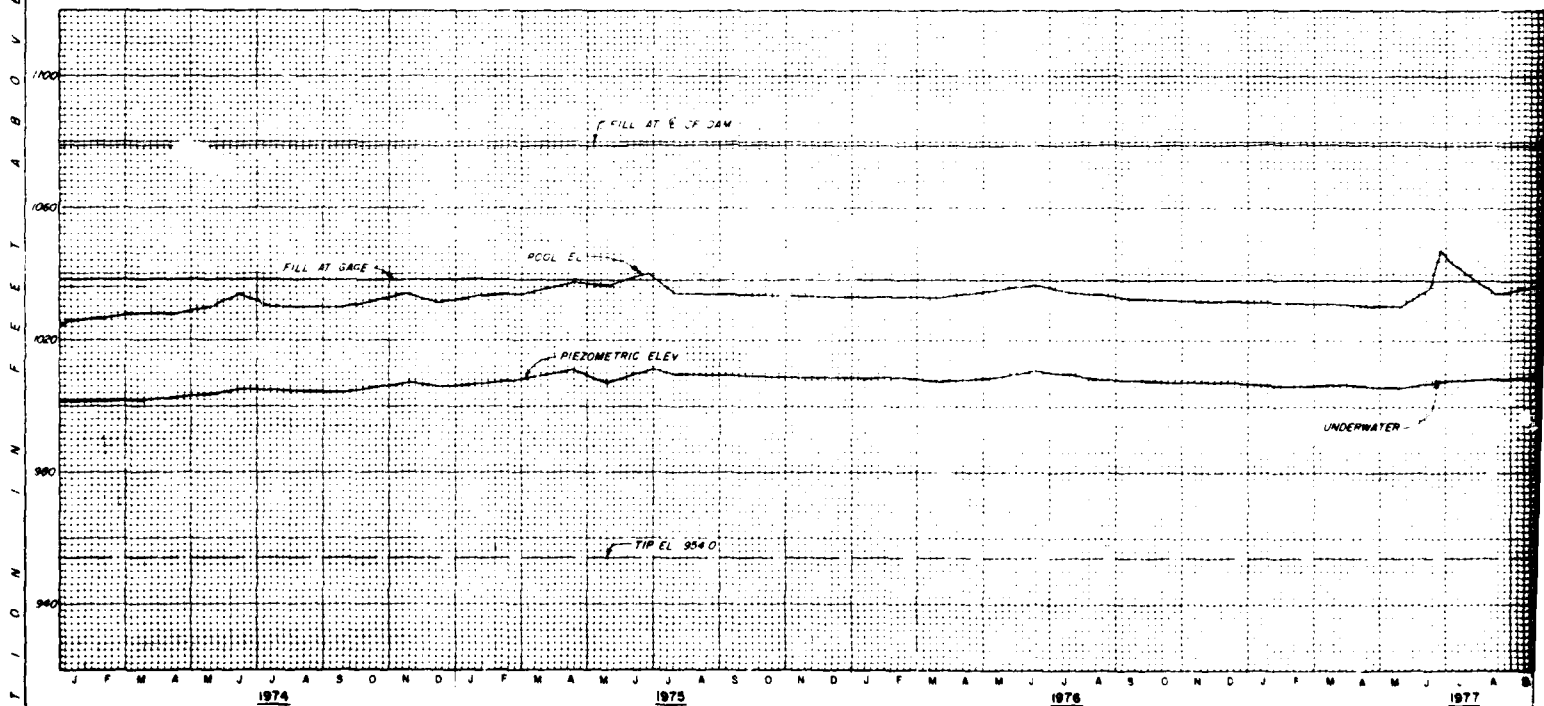
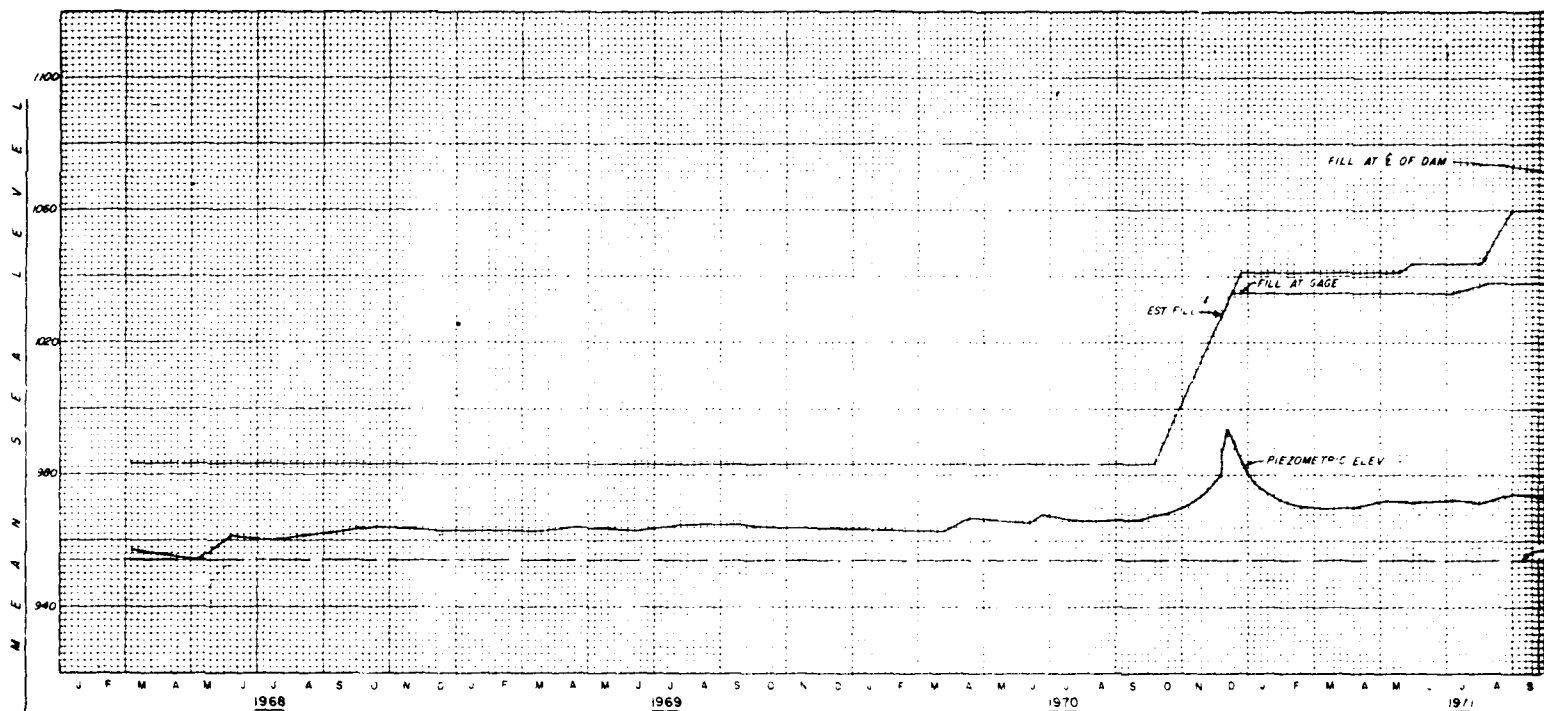
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In 1 sheet

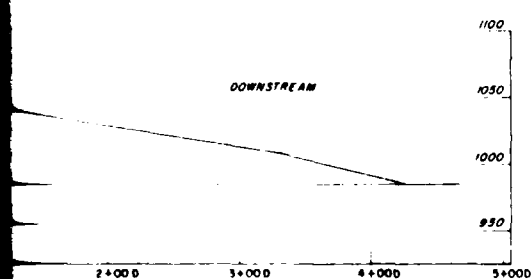
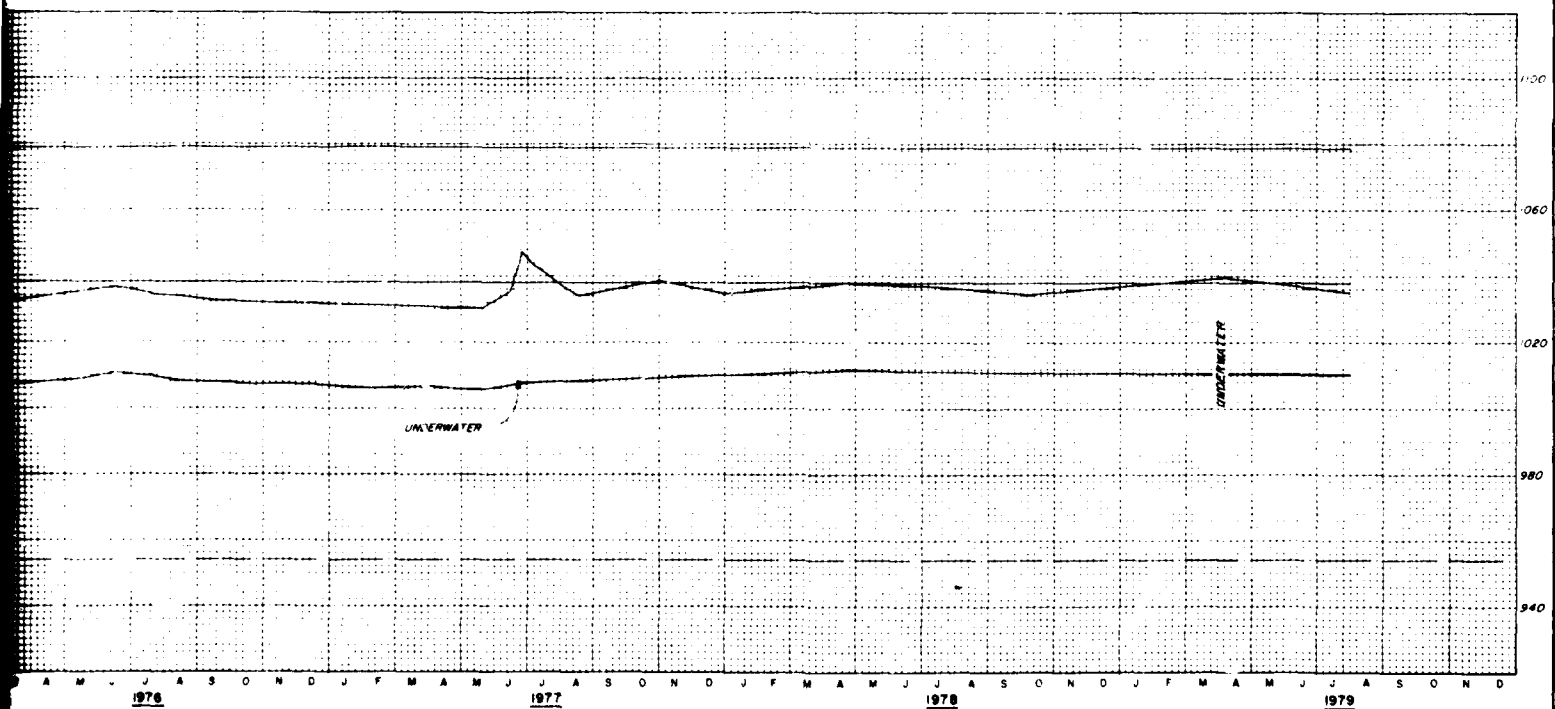
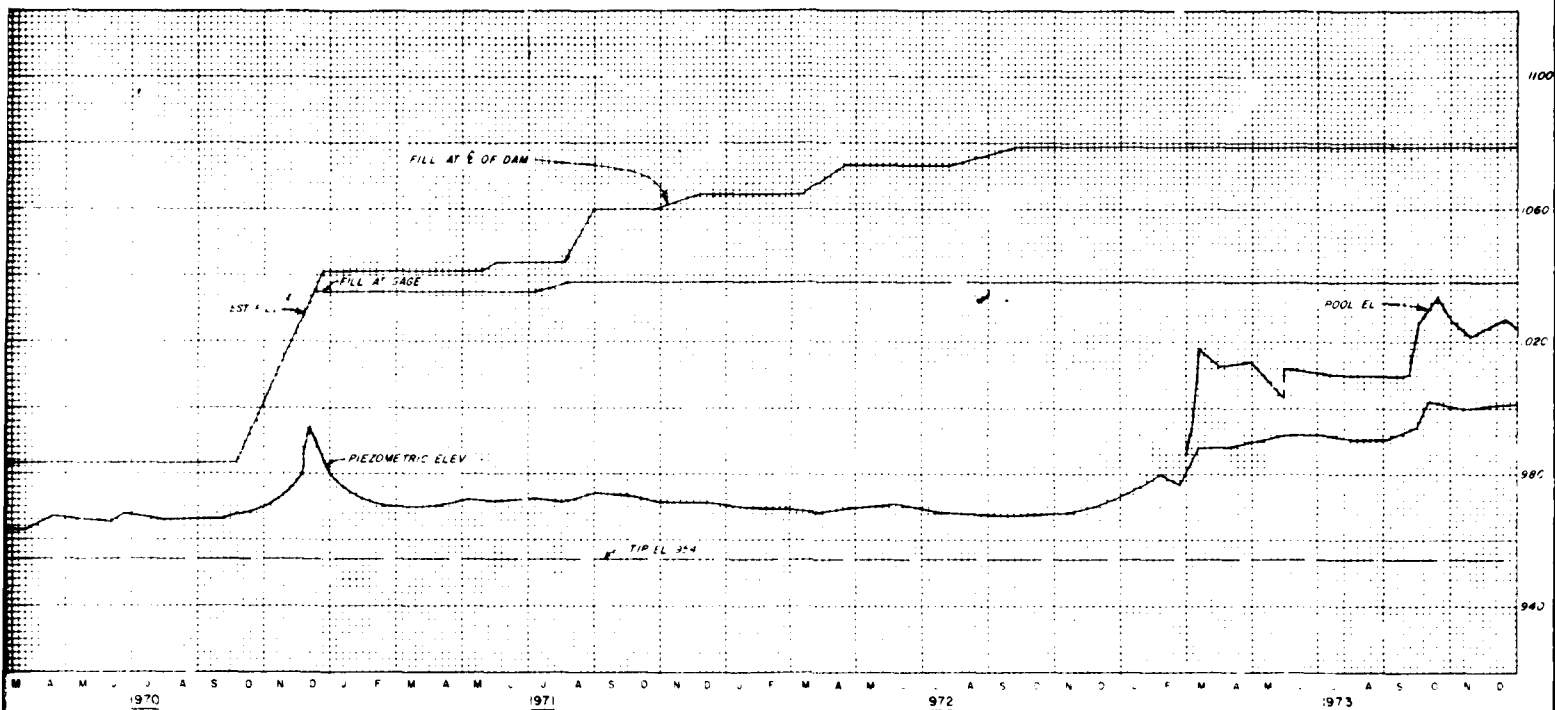
Sheet No. 1

Scale as shown

CORPS OF ENGINEERS U.S. ARMY
 KANSAS CITY DISTRICT
 FILE NO. 0-5-1279
 AUGUST 1975



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LEGEND
 OPEN TUBE ○
 PNEUMATIC CELLS ●

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 MARAIS DES CYGNES RIVER KANSAS
MELVERN LAKE

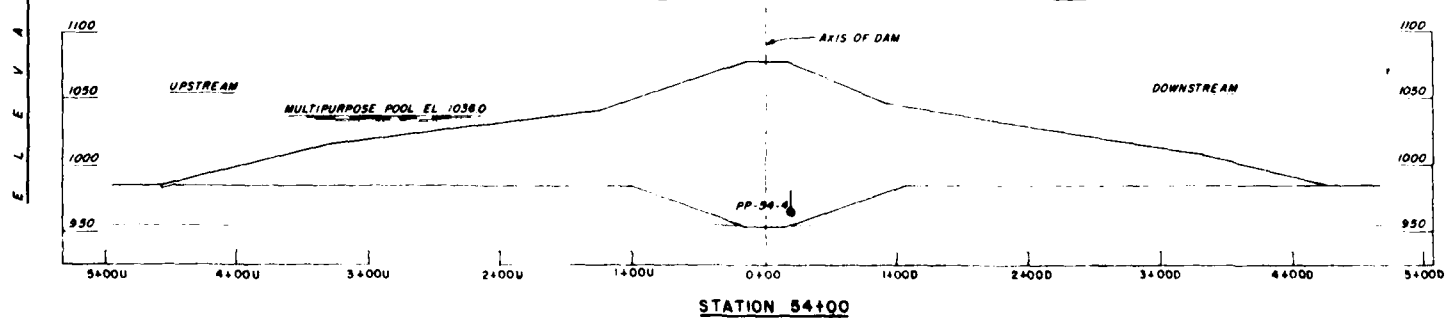
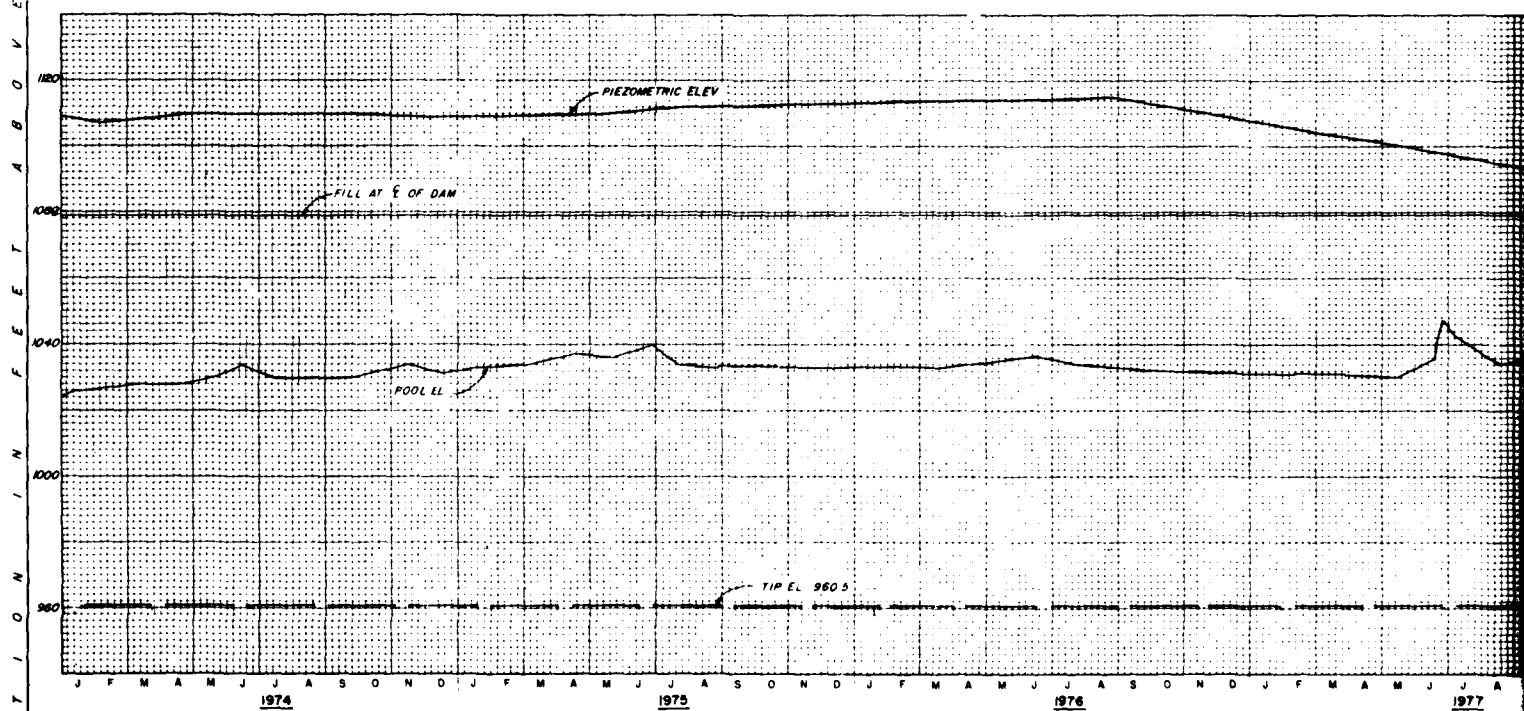
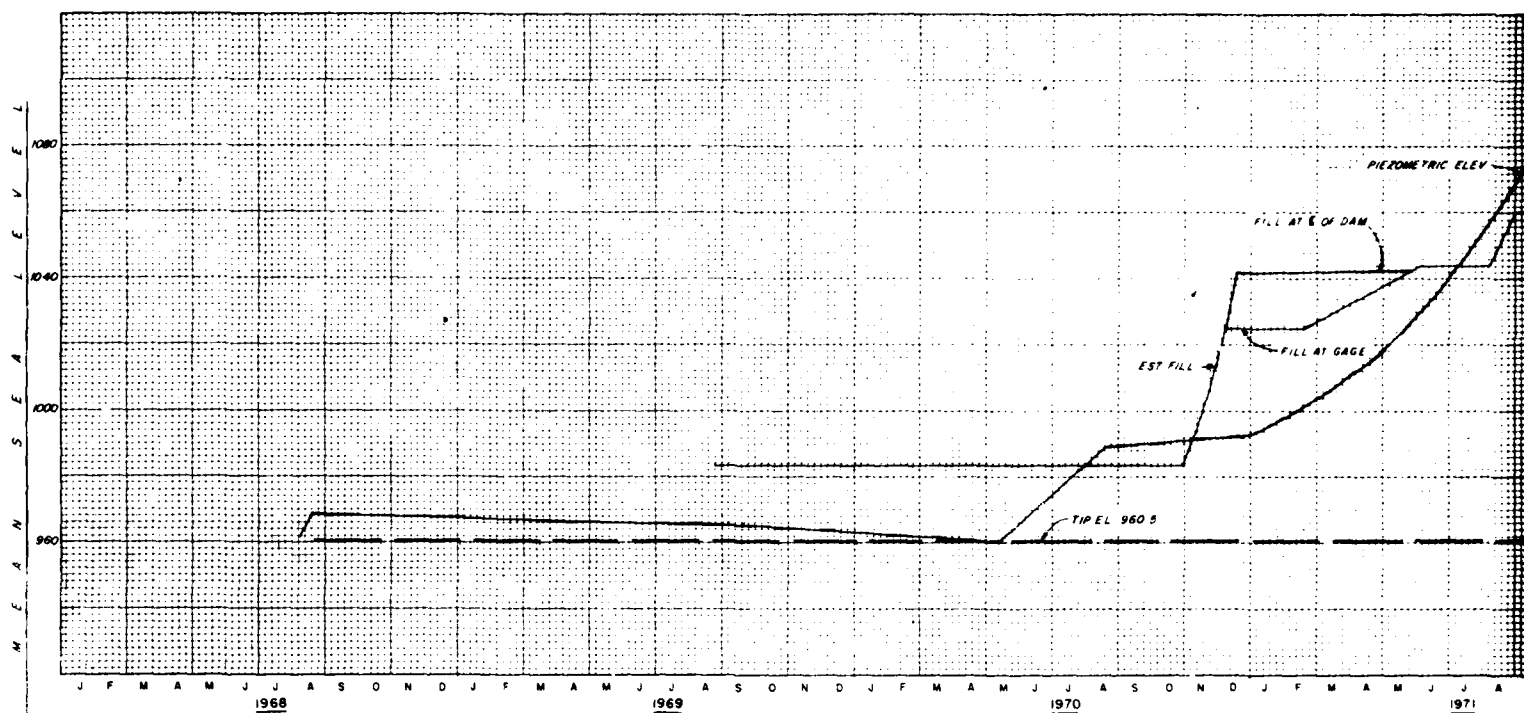
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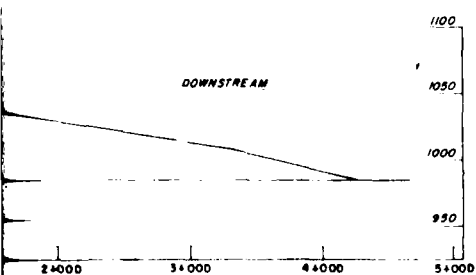
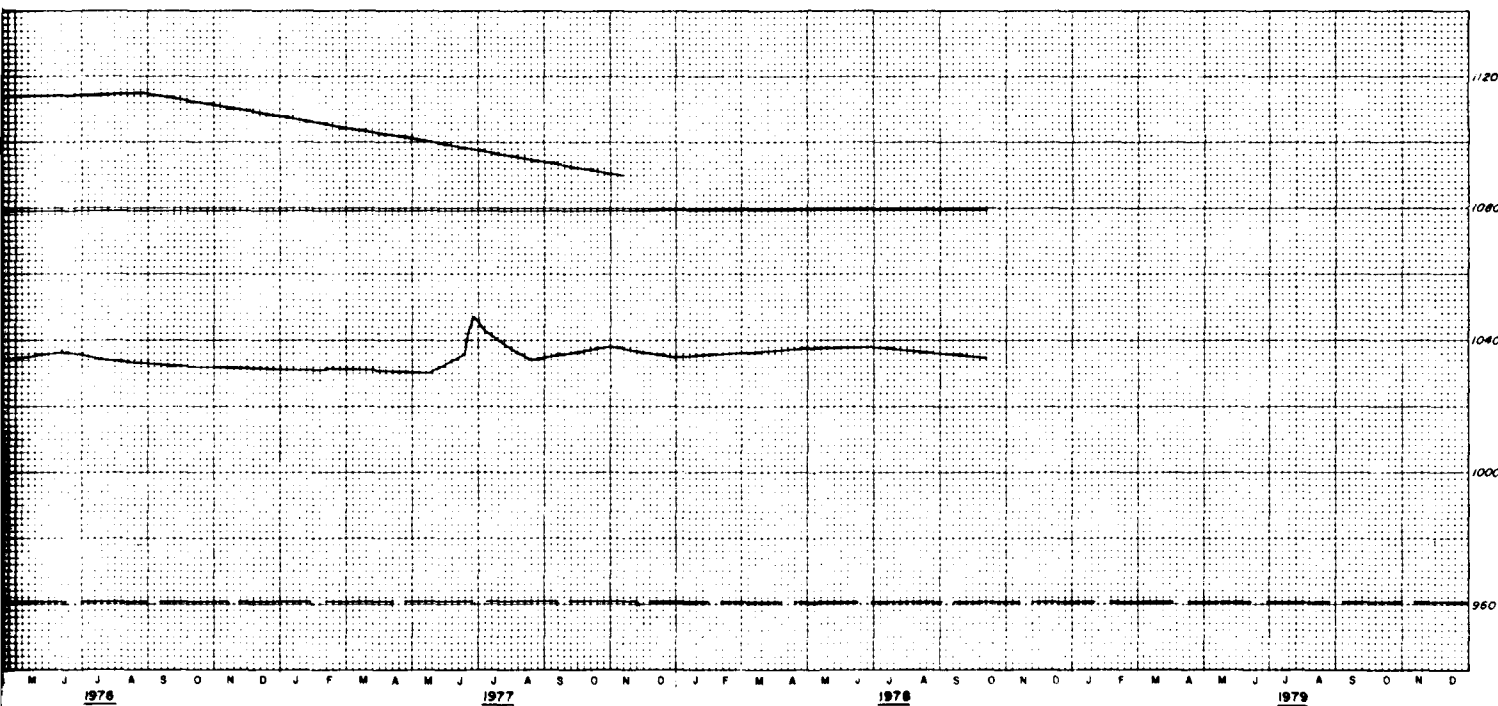
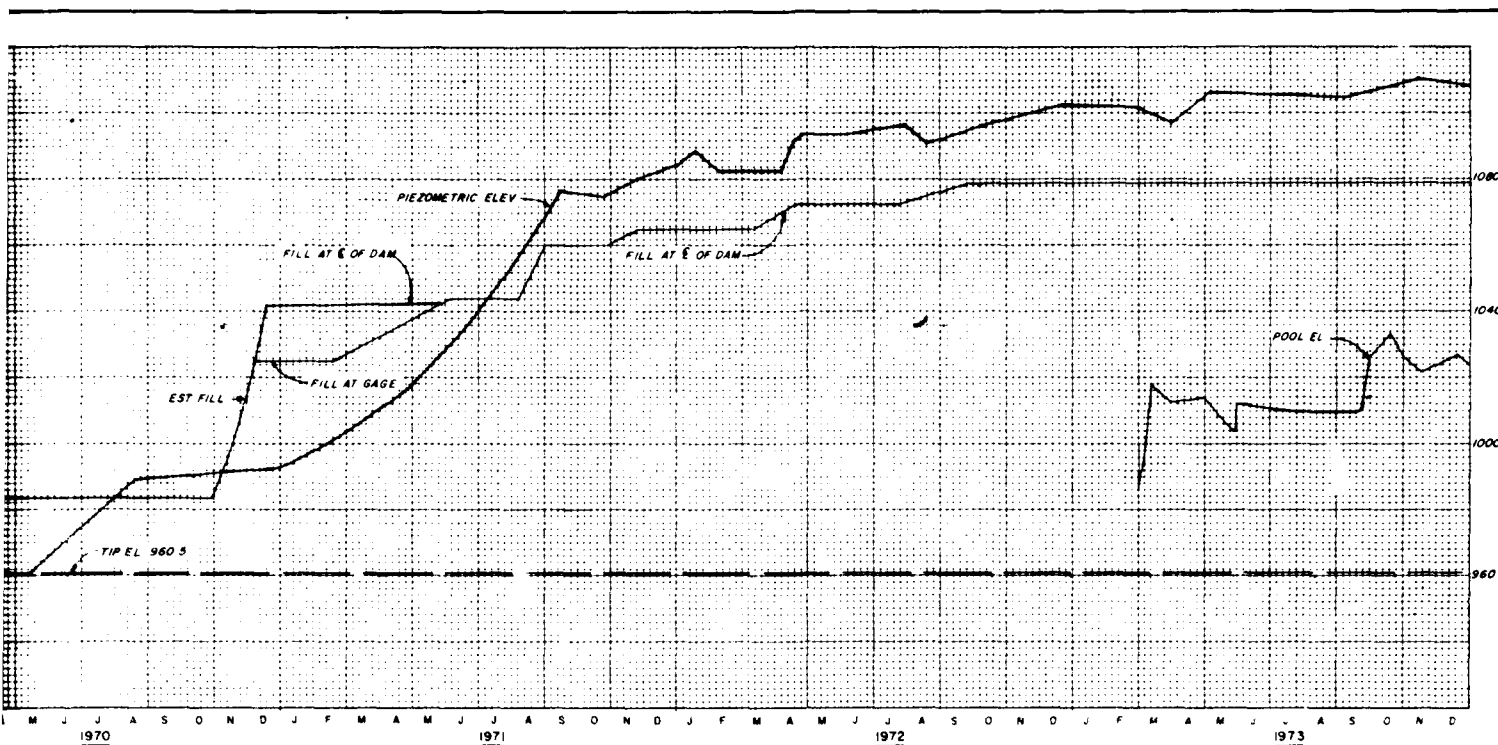
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 CORPS OF ENGINEERS U.S. ARMY
 KANSAS CITY DISTRICT

Scale as shown

FILE NO. 0-5-1280
 AUGUST 1975





LEGEND

OPEN TOBE ————○
PNEUMATIC CELL ————●

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MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

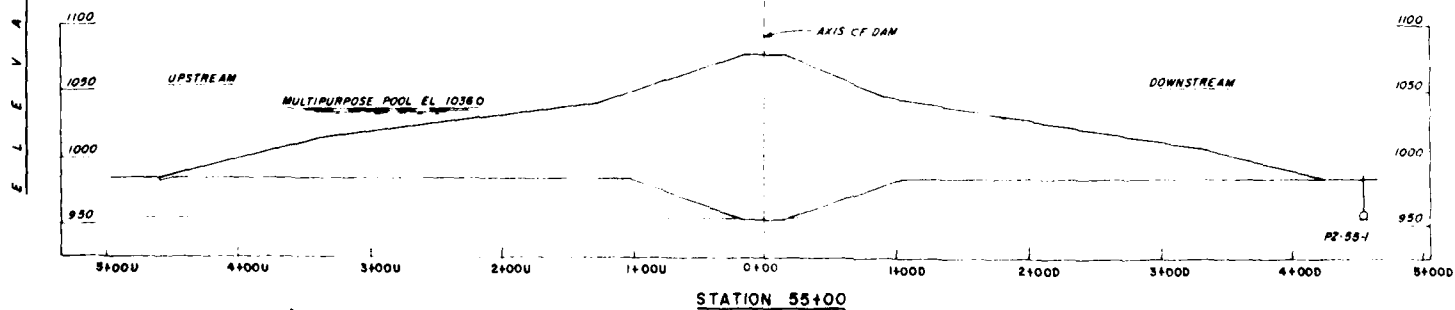
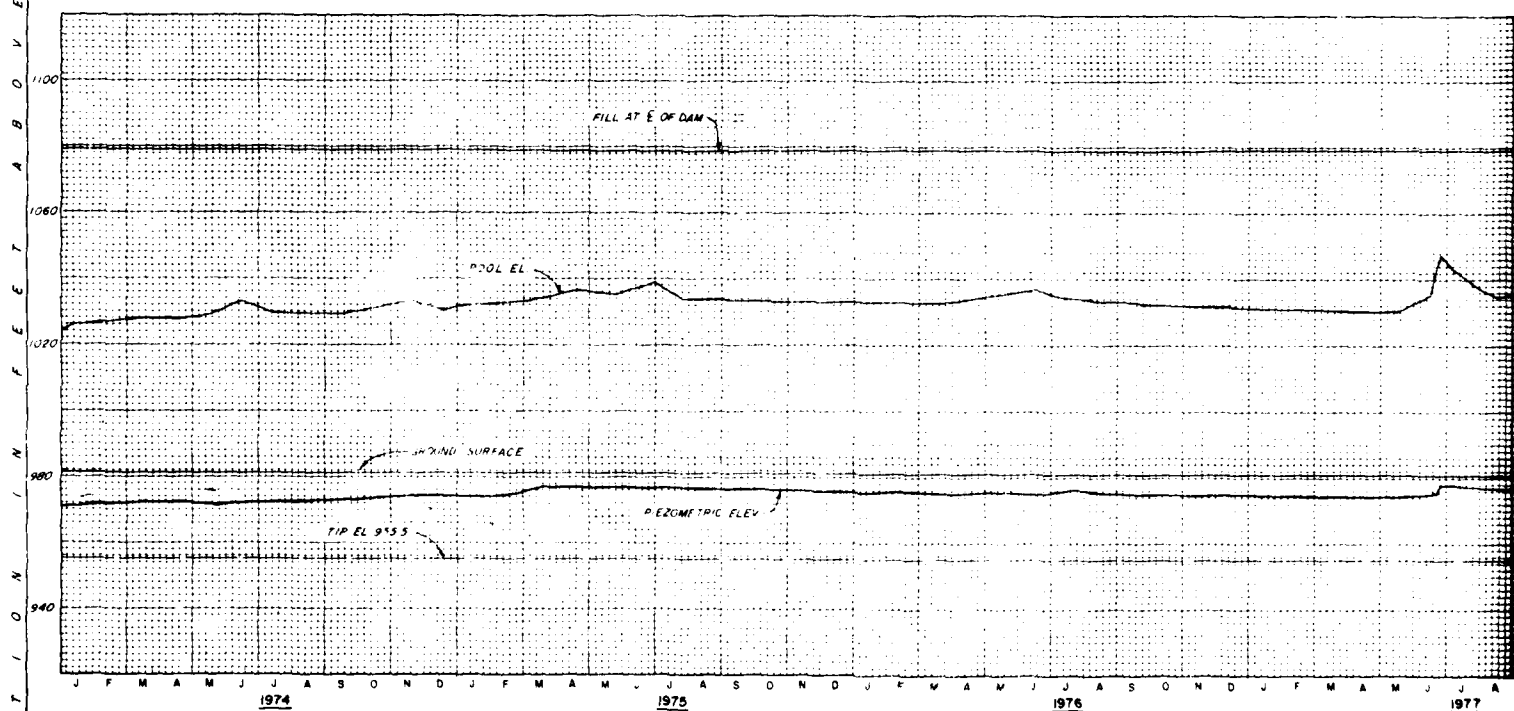
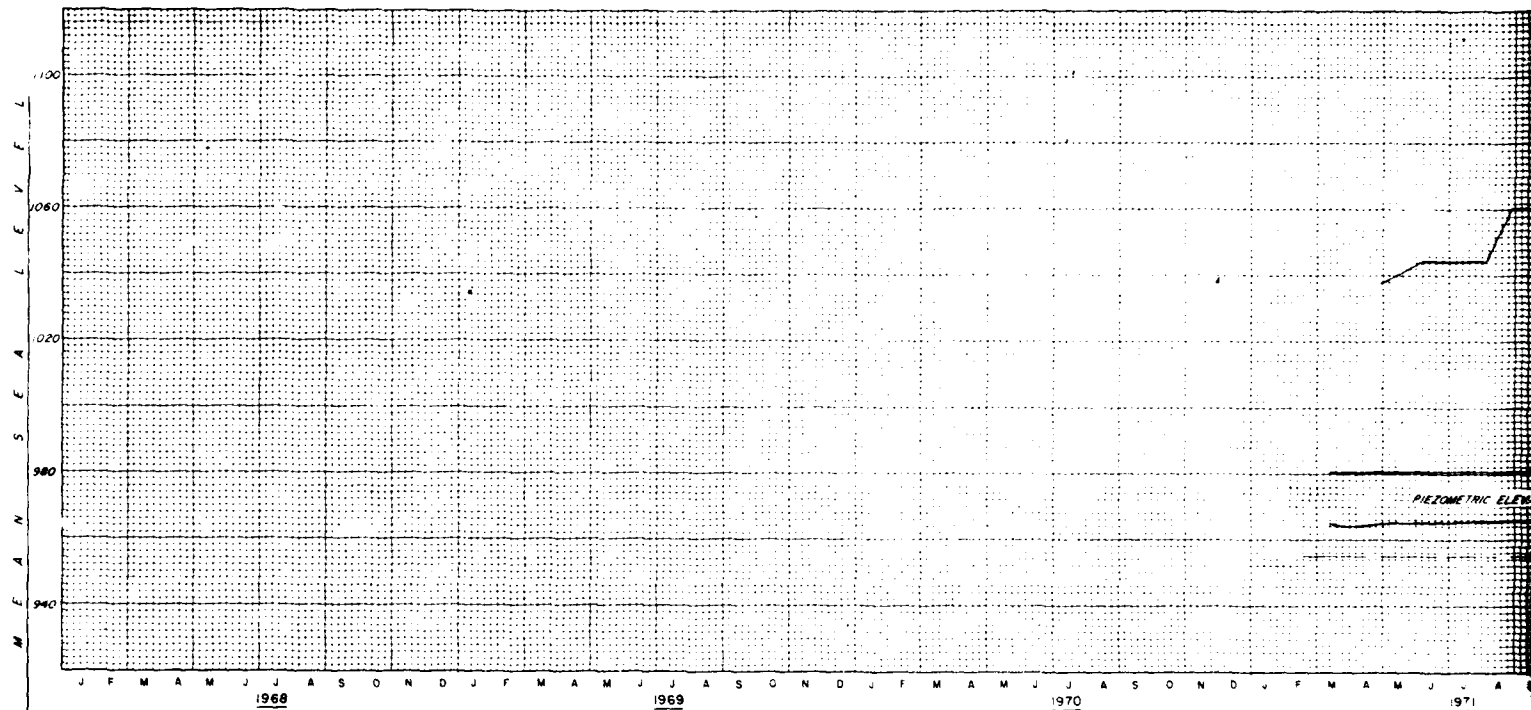
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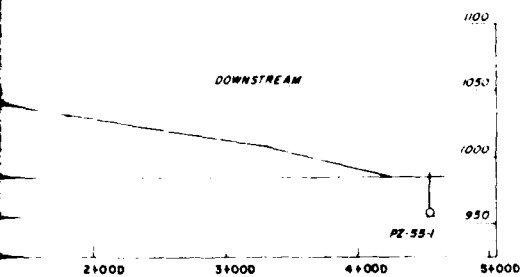
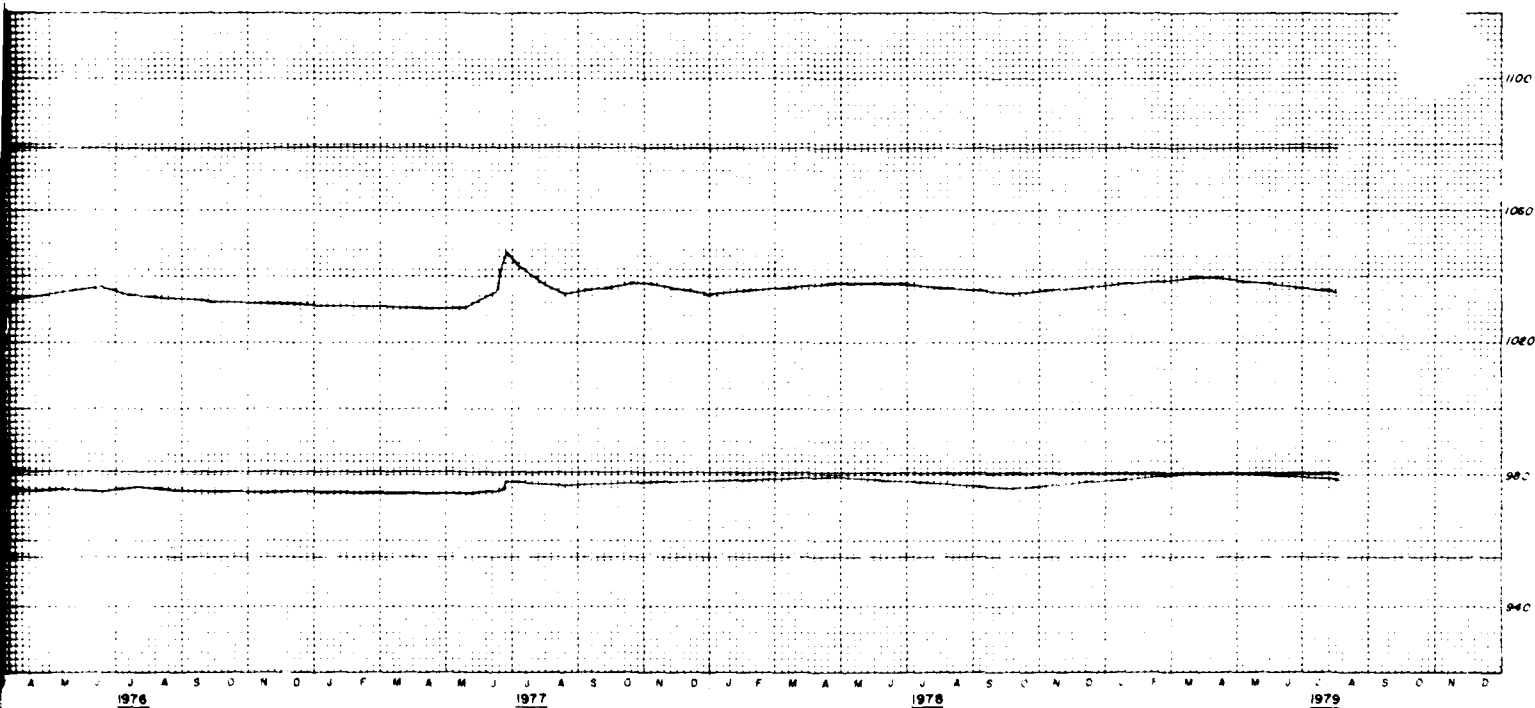
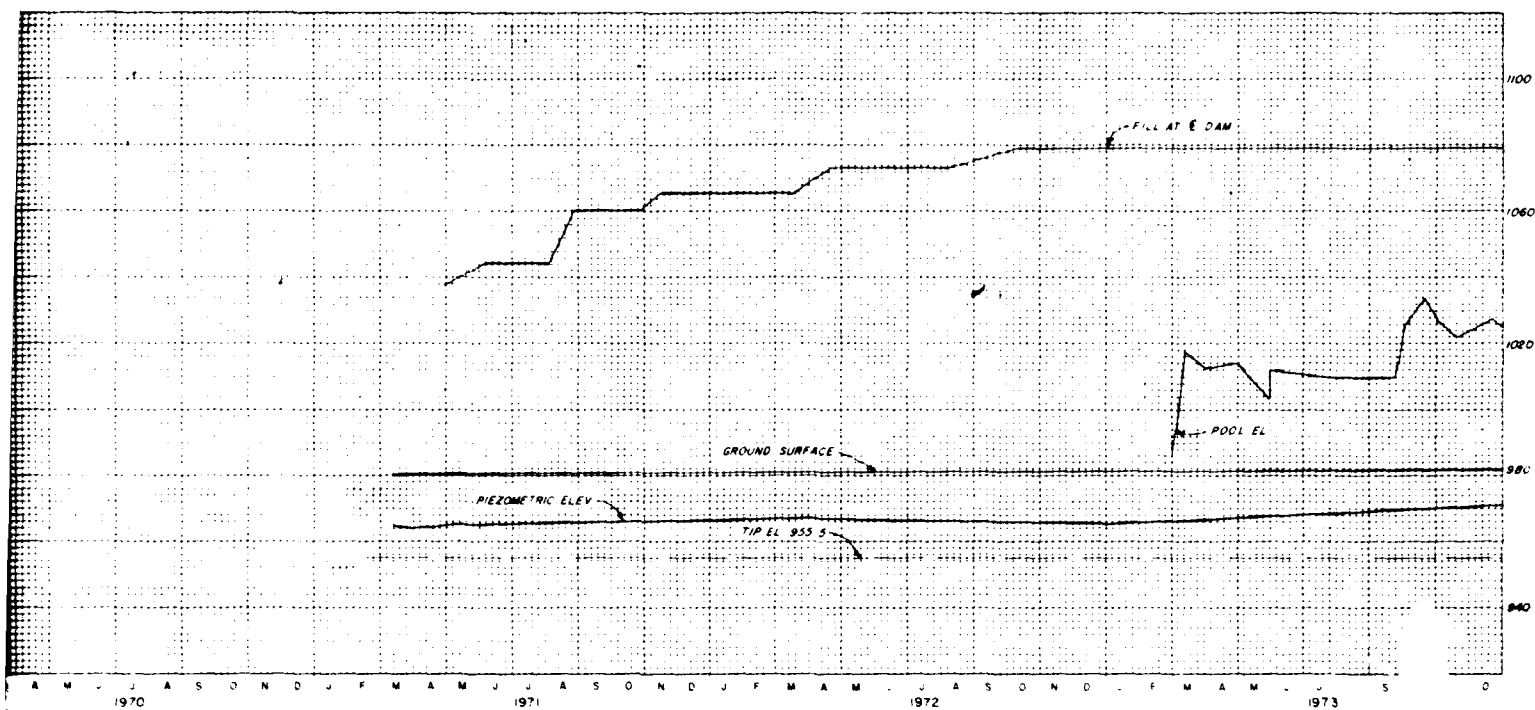
In 1 sheet

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CORPS OF ENGINEERS U. S. ARMY
KANSAS CITY DISTRICT

Scale as shown

FILE NO. 0-5-1281
AUGUST 1975





LEGEND

OPEN TUBE ———— ○
PNEUMATIC CELL ———— ●

APR 20 1975
MARAI DES CYGNES RIVER, KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
PZ-55-1 (OPEN TUBE)

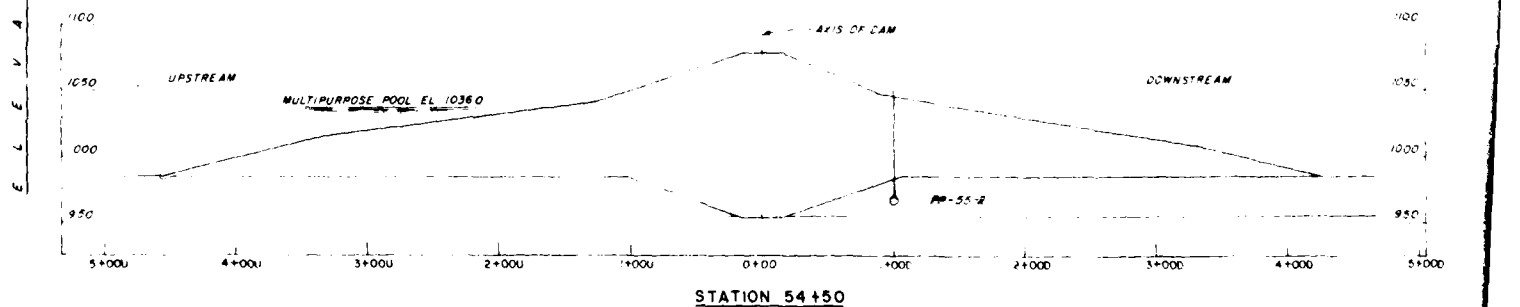
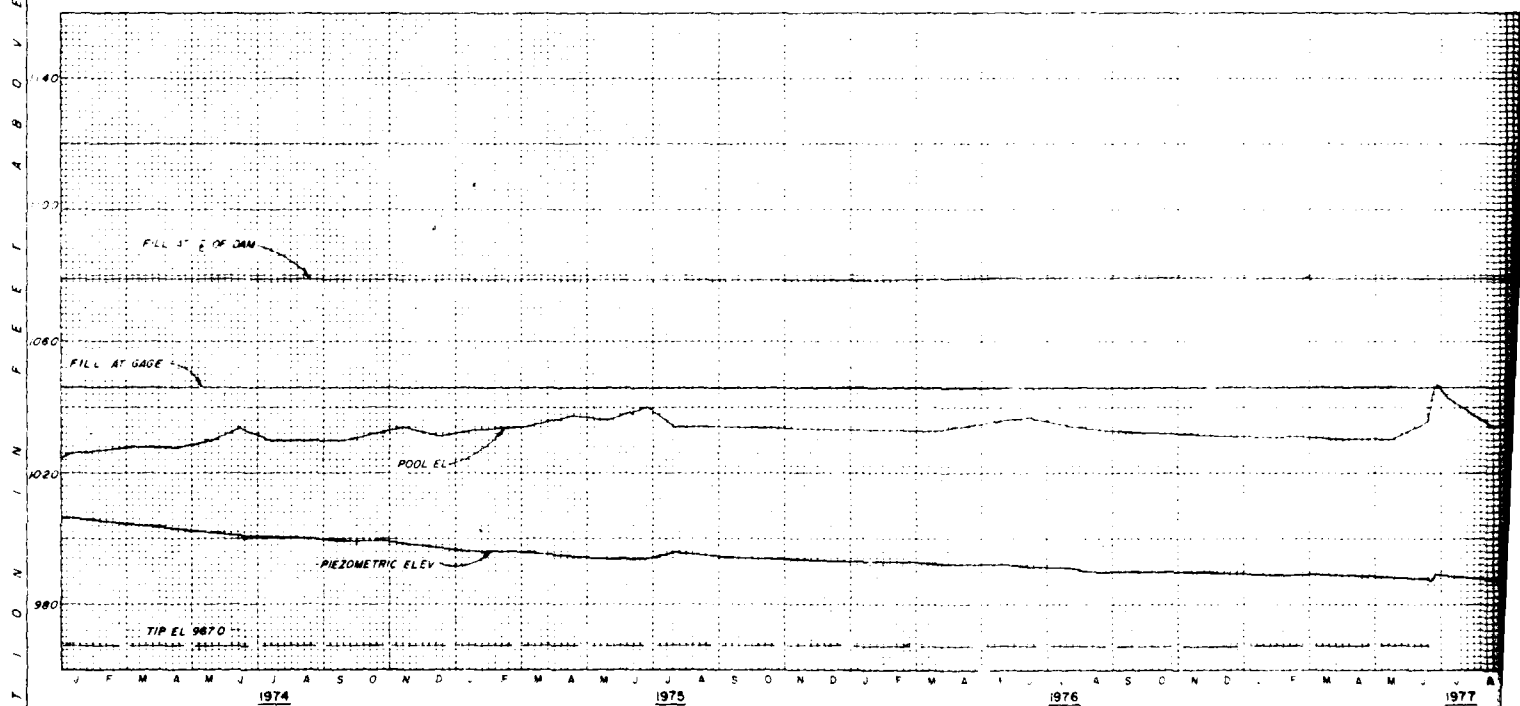
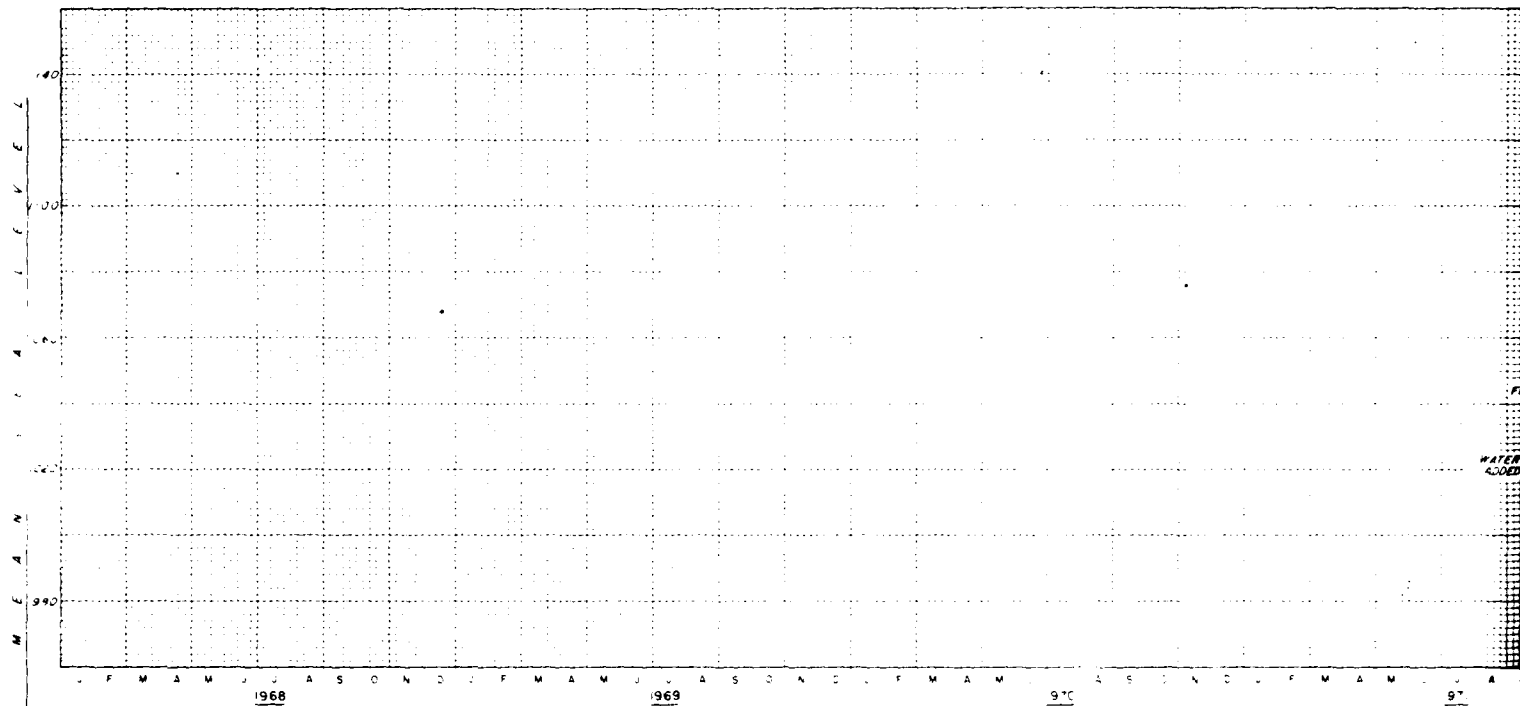
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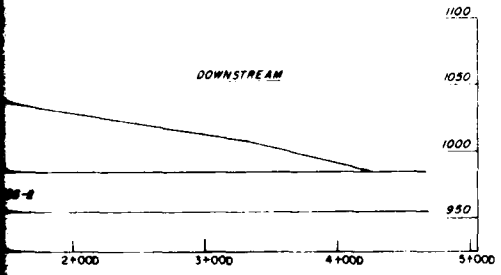
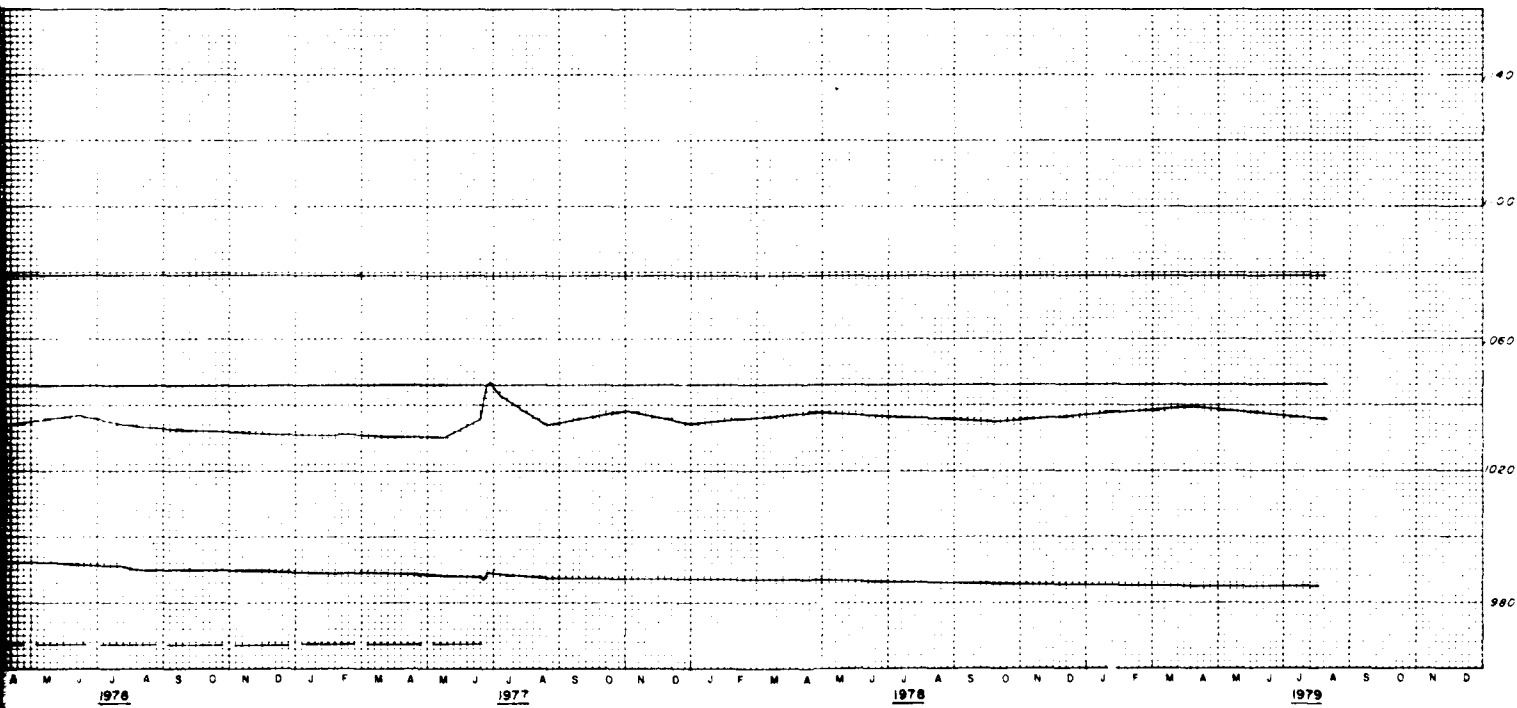
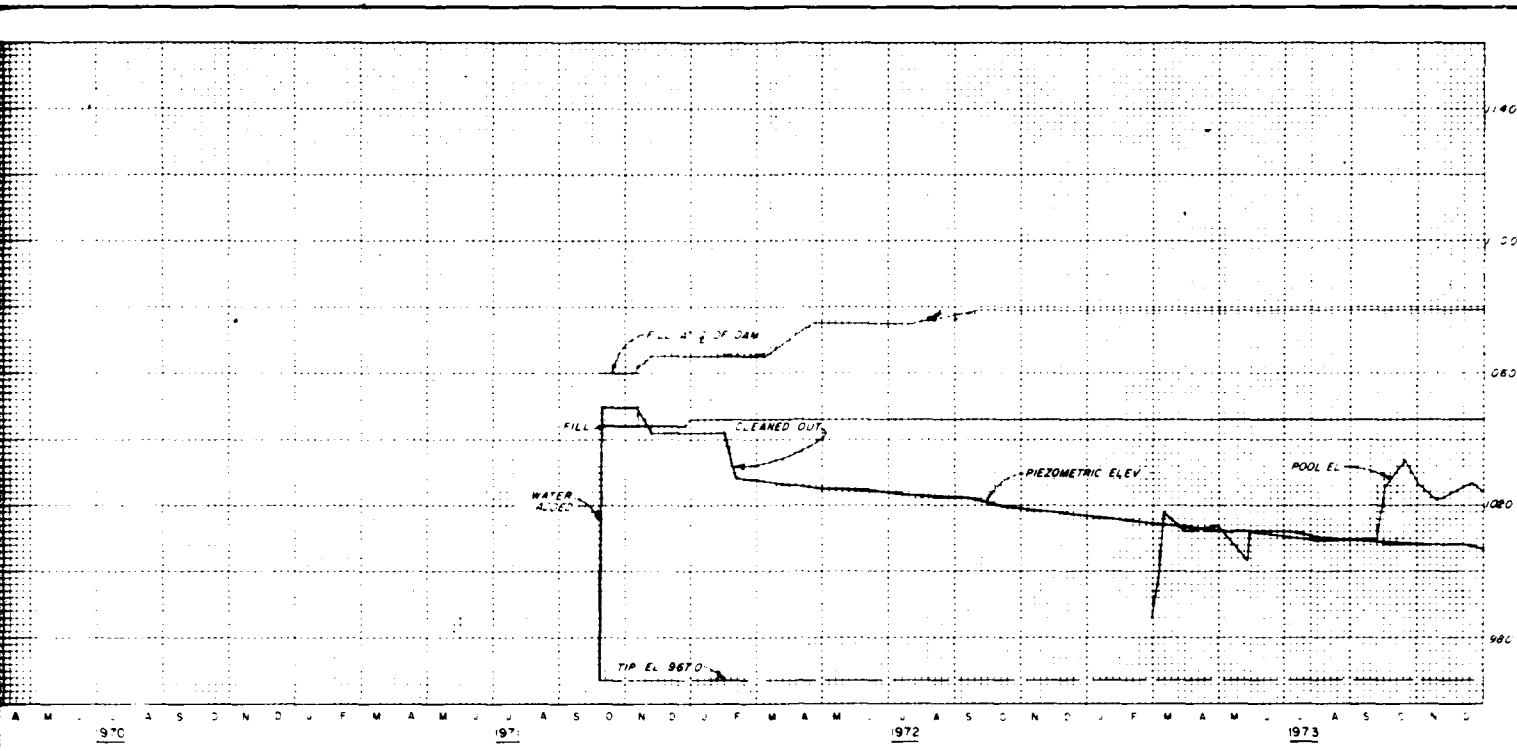
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CORPS OF ENGINEERS U. S. ARMY
KANSAS CITY DISTRICT

FILE NO 0-5-1282
AUGUST 1975



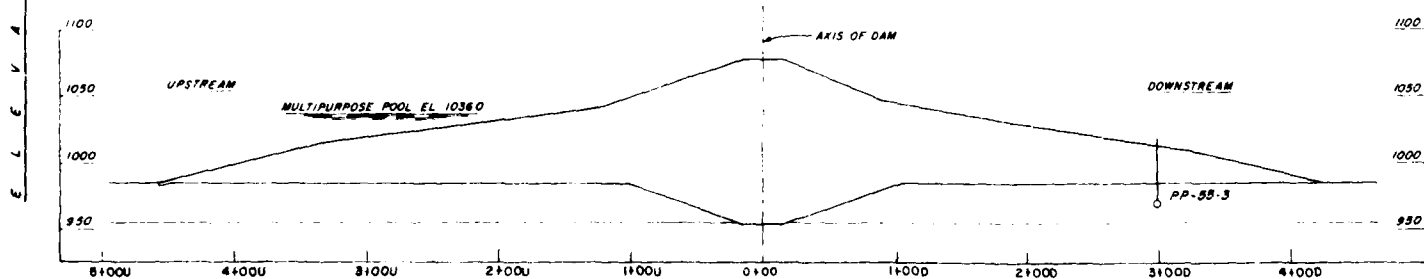
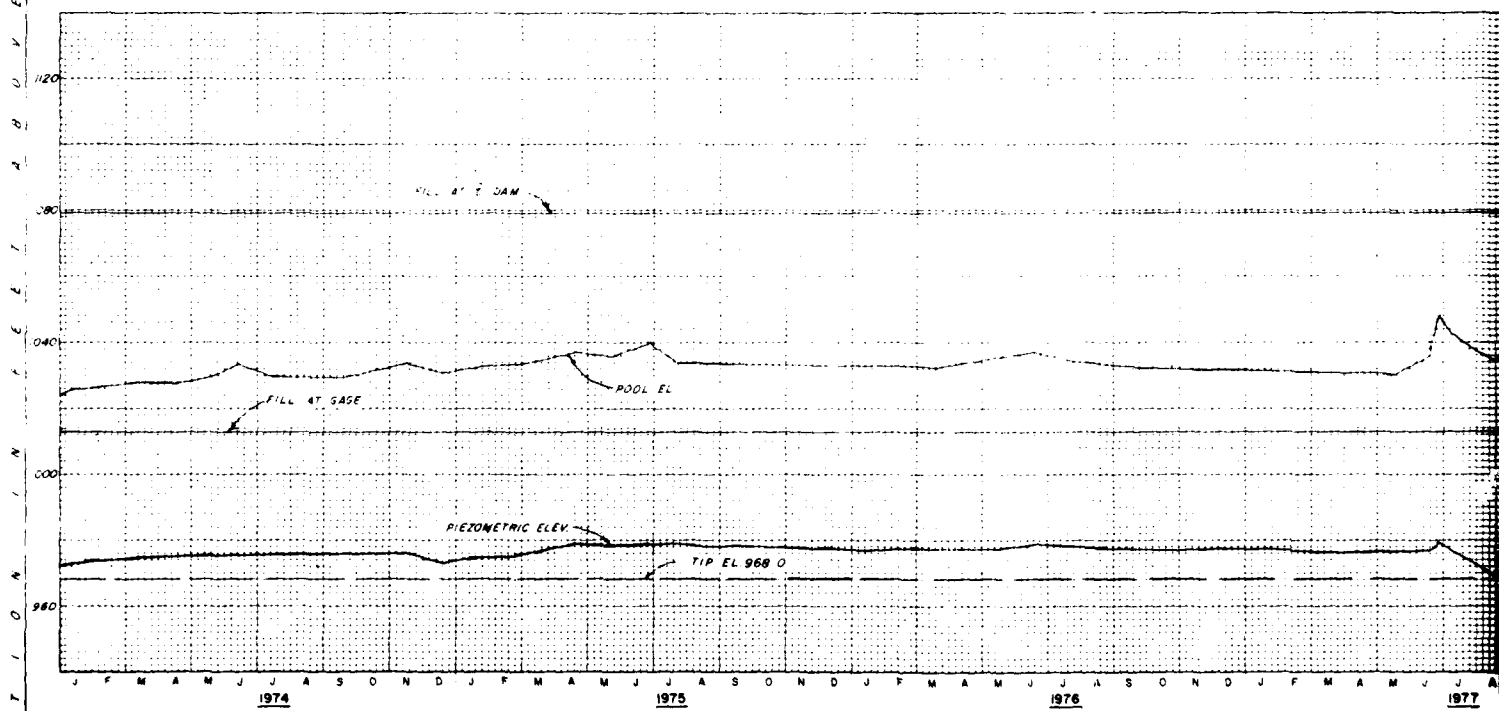
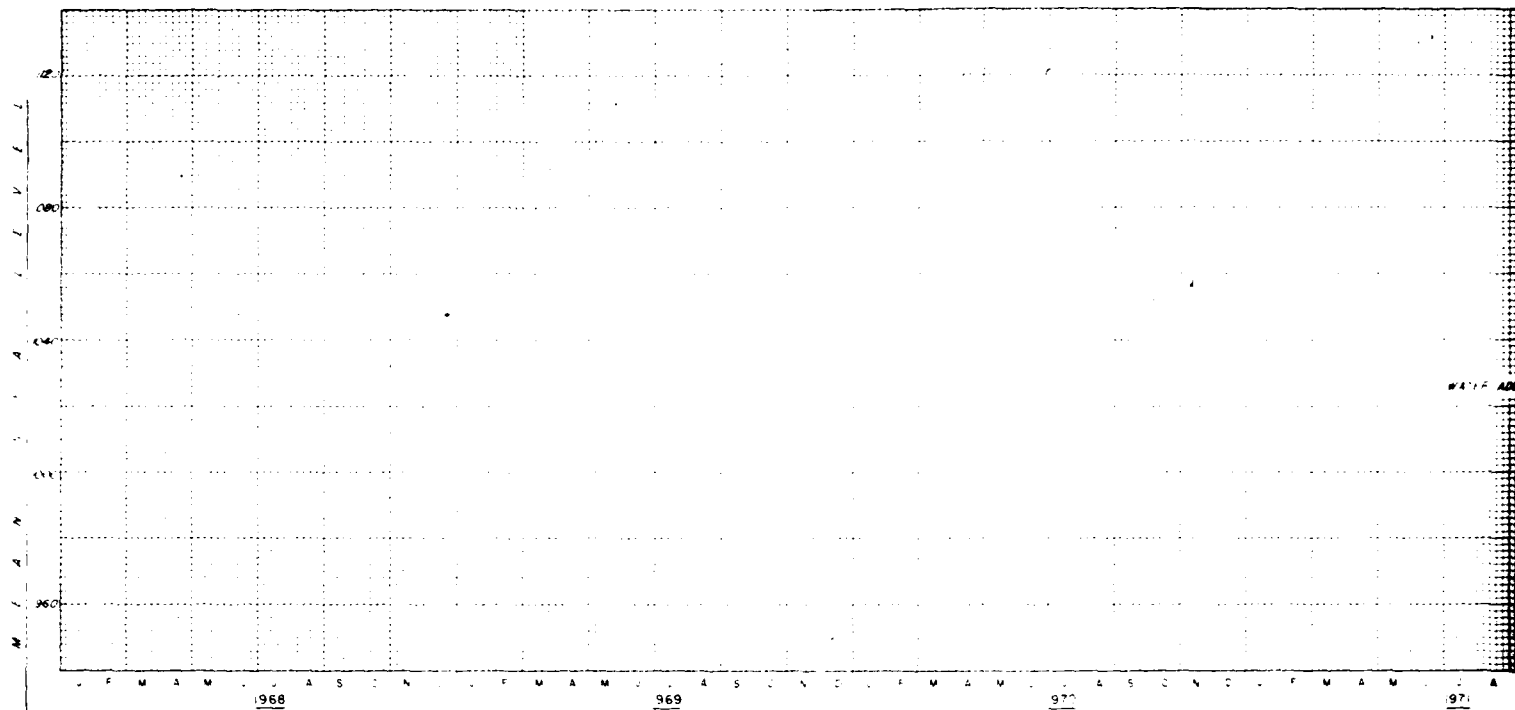


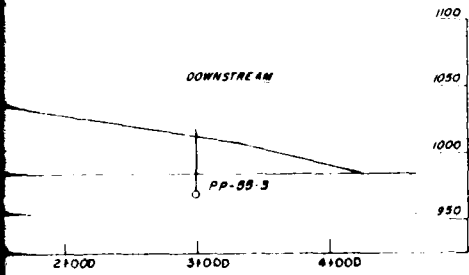
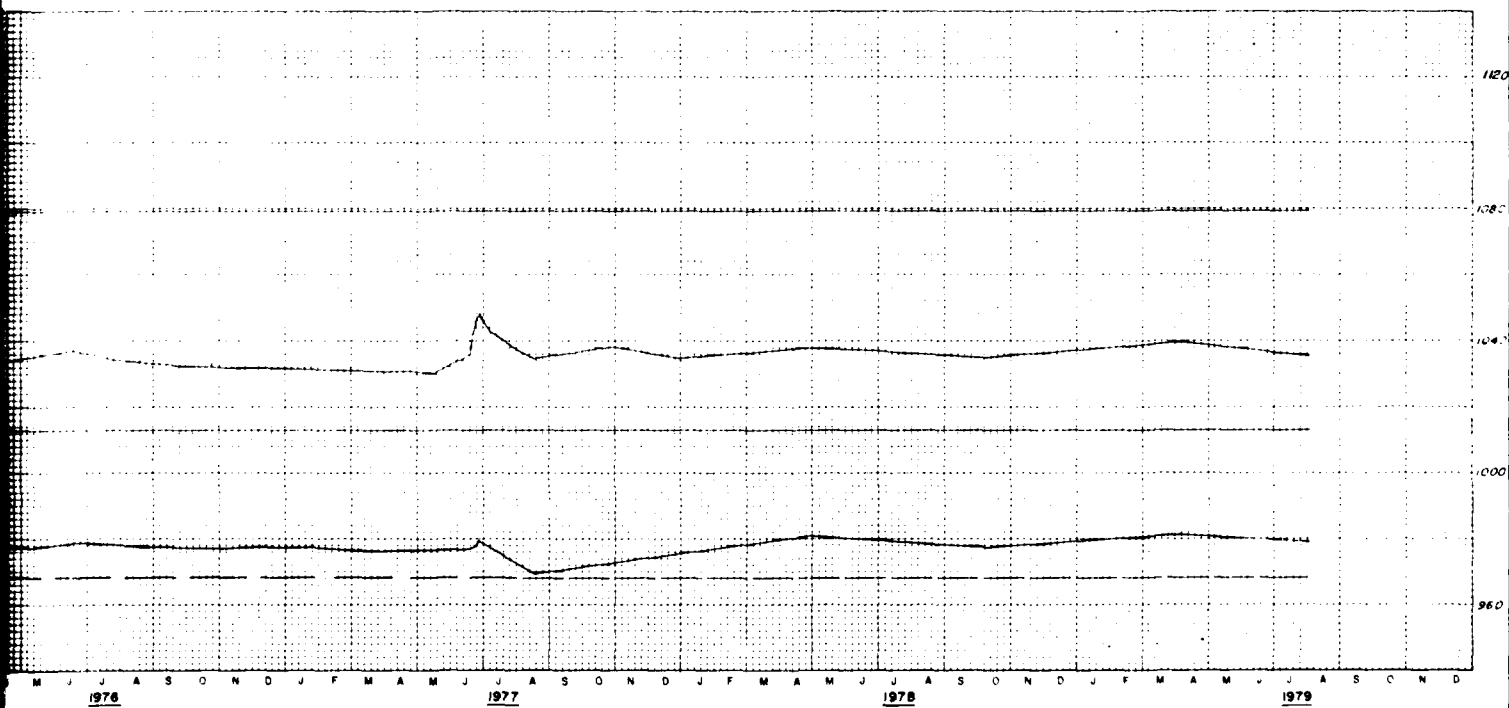
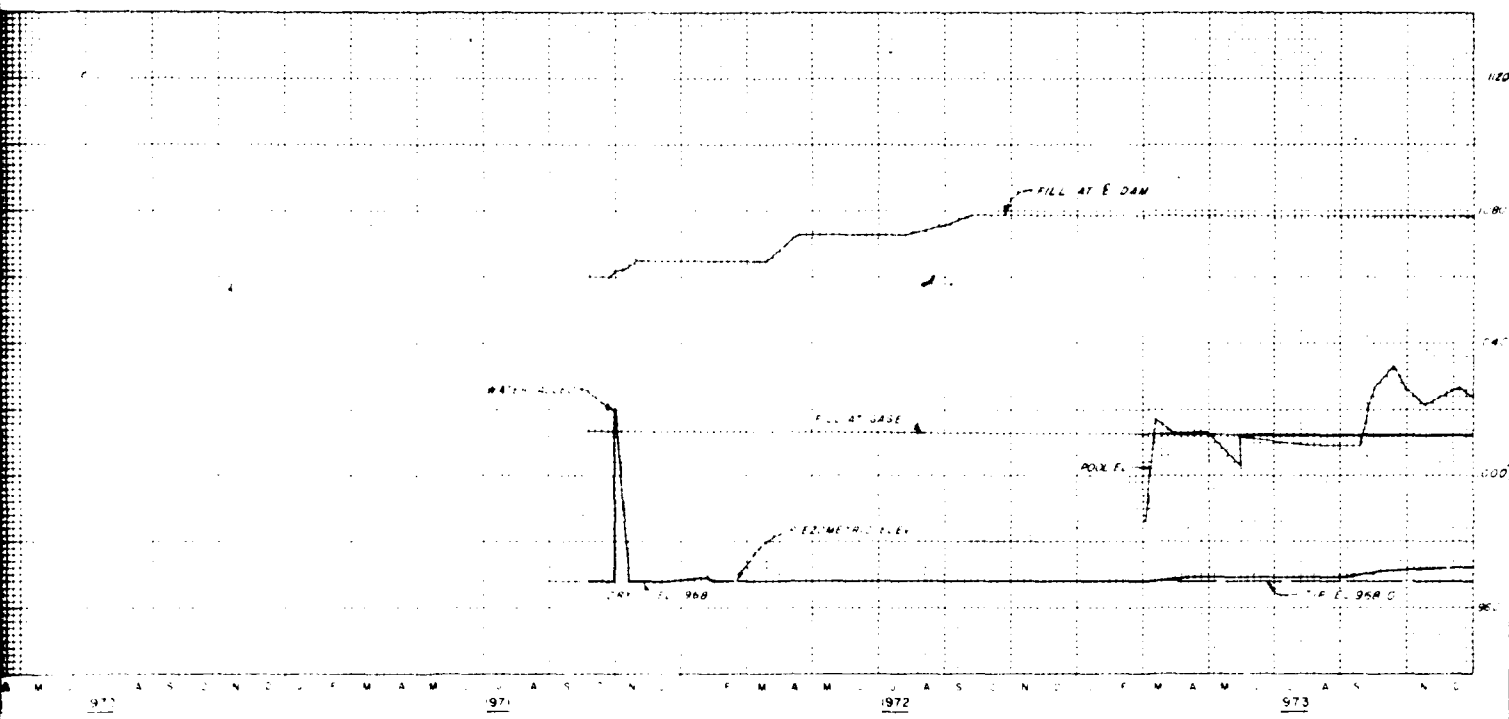
LEGEND
 OPEN TUBE ————○
 PNEUMATIC CELL ————●

Rev. Sept. August 1979
 MARAIS DES CYGNES RIVER KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
 PP-55-2 (OPEN TUBE)

In 1 sheet
 Sheet No 1
 CORPS OF ENGINEERS U.S. ARMY
 KANSAS CITY DISTRICT
 FILE NO. 0-5-1283
 AUGUST 1975
 Scale as shown





LEGEND
 OPEN TUBE ————○
 PNEUMATIC CELL ————●

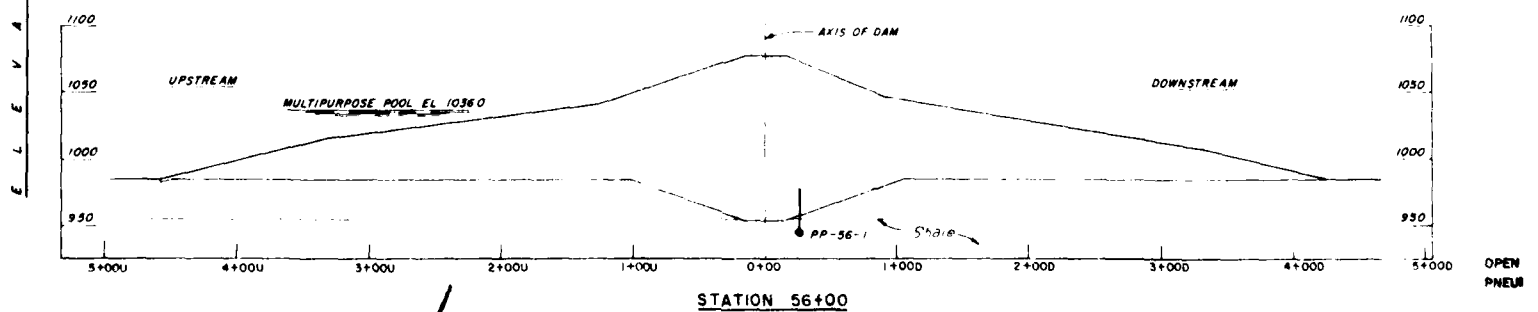
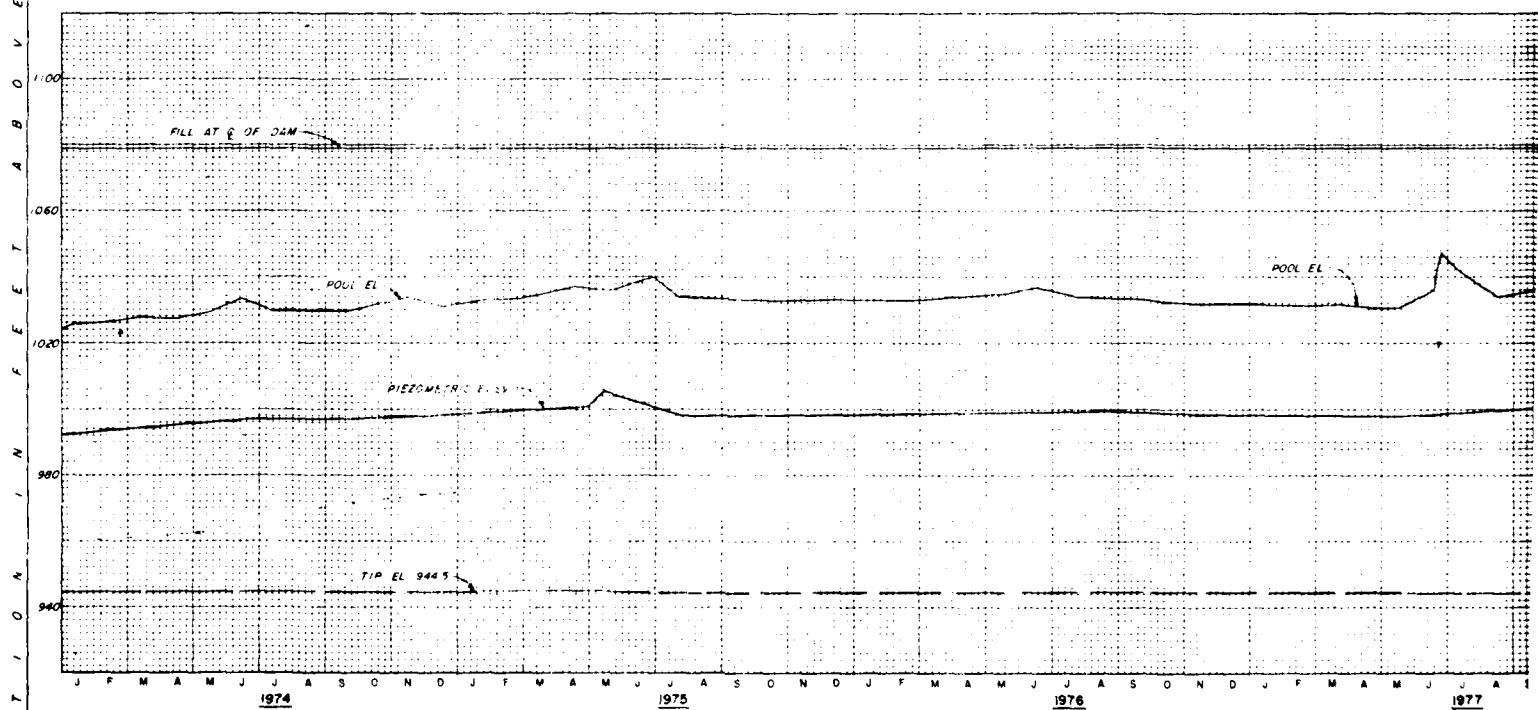
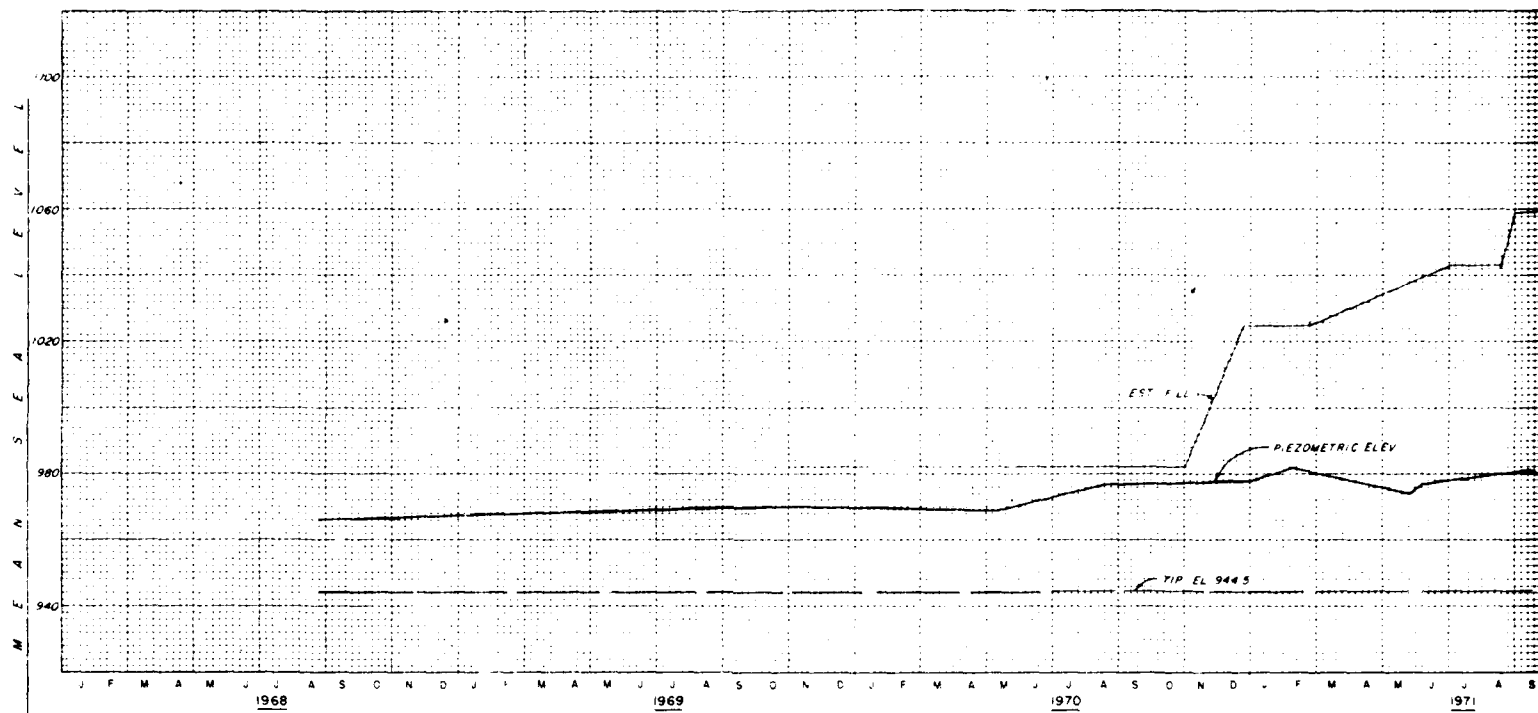
Revised August 1975
 MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

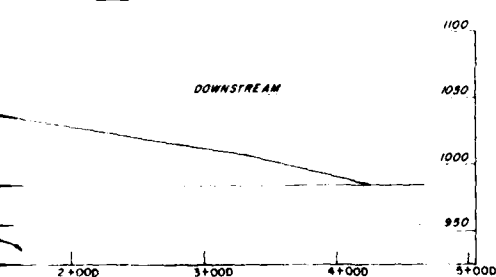
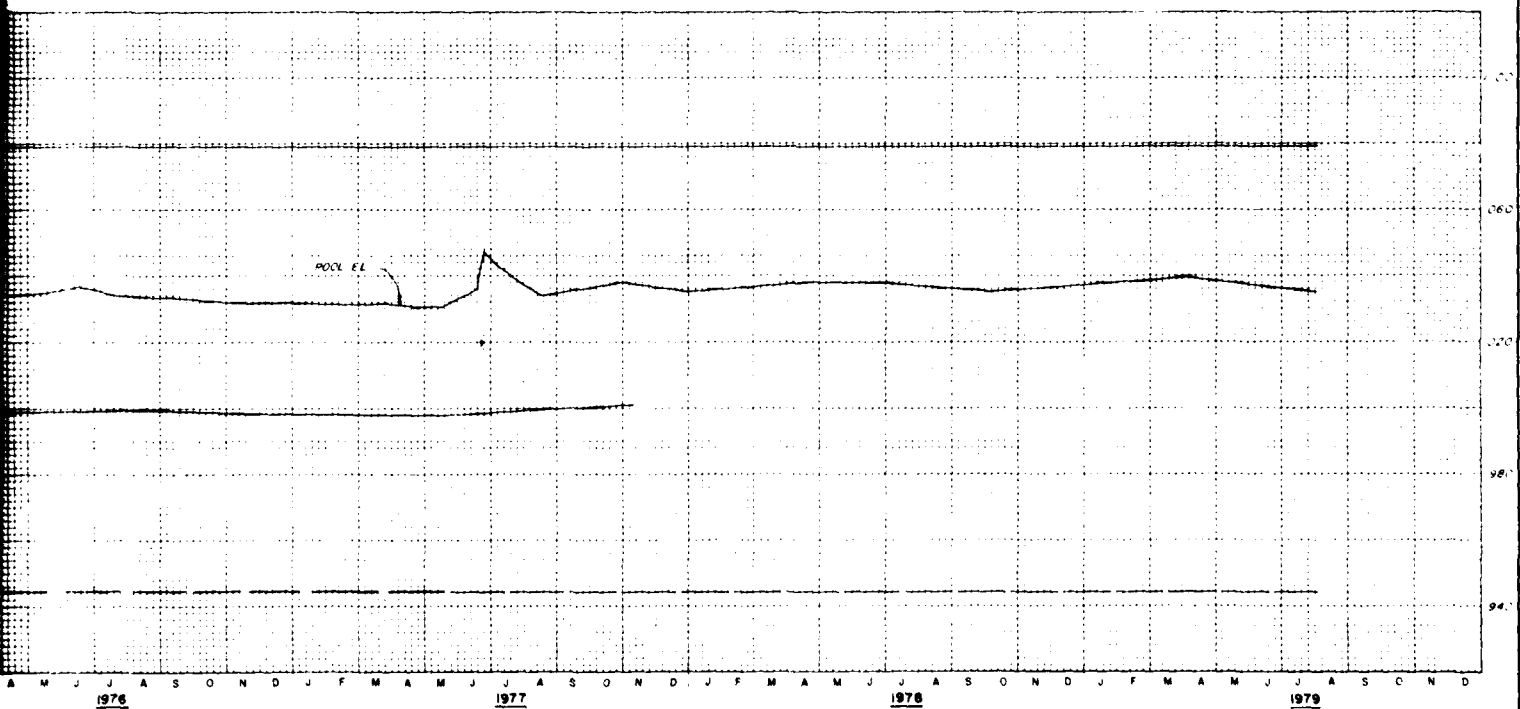
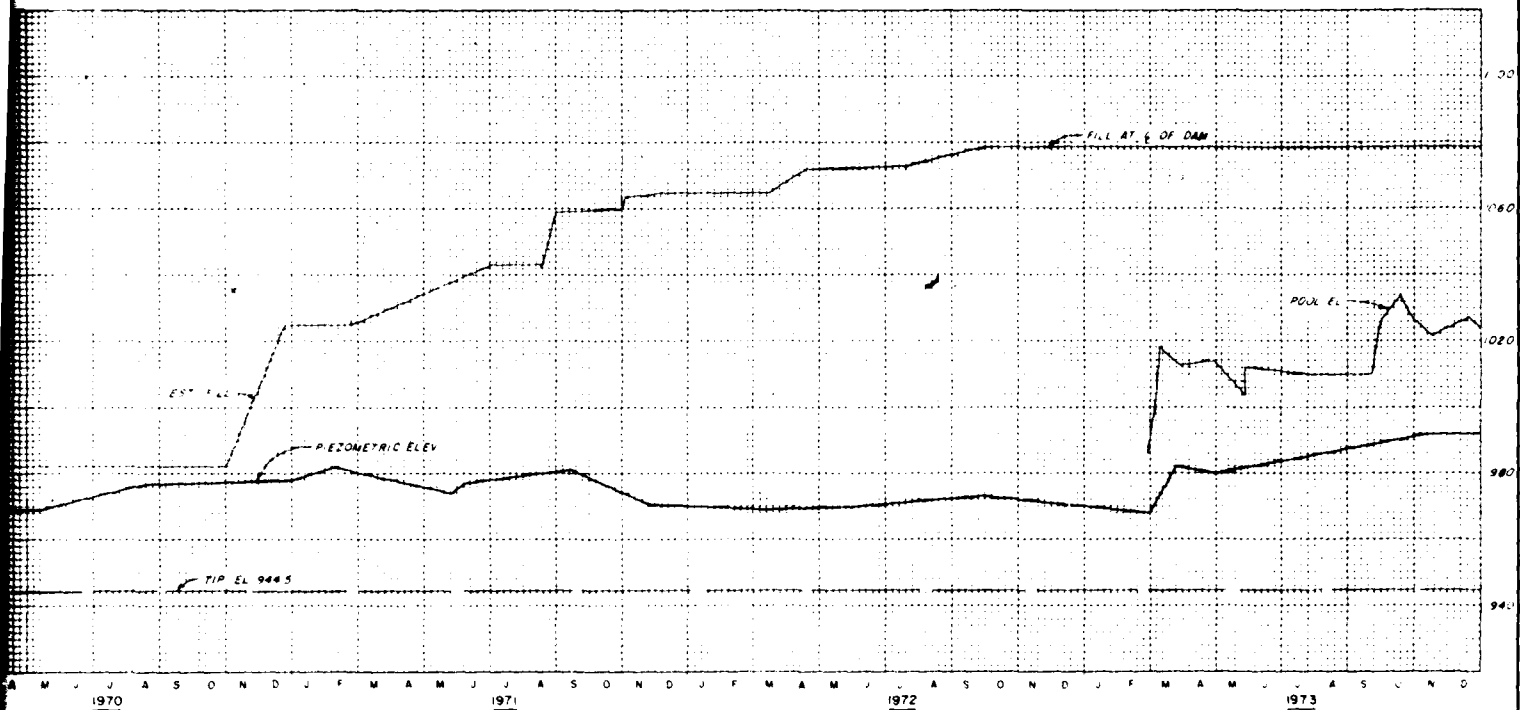
INSTRUMENTATION PLOTS
PP55-3 (OPEN TUBE)

In 1 sheet

Sheet No. 1
 CORPS OF ENGINEERS U.S. ARMY
 KANSAS CITY DISTRICT
FILE NO 0-5-1284
 AUGUST 1975

Scale as shown





LEGEND
 OPEN TUBE
 PNEUMATIC CELL

Revised August 1979
 MARAIS DES CYGNES RIVER KANSAS
MELVERN LAKE

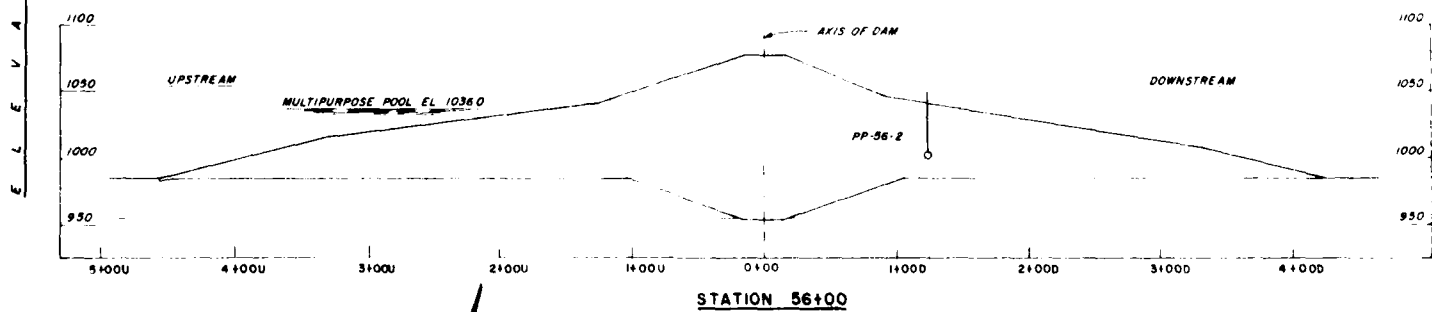
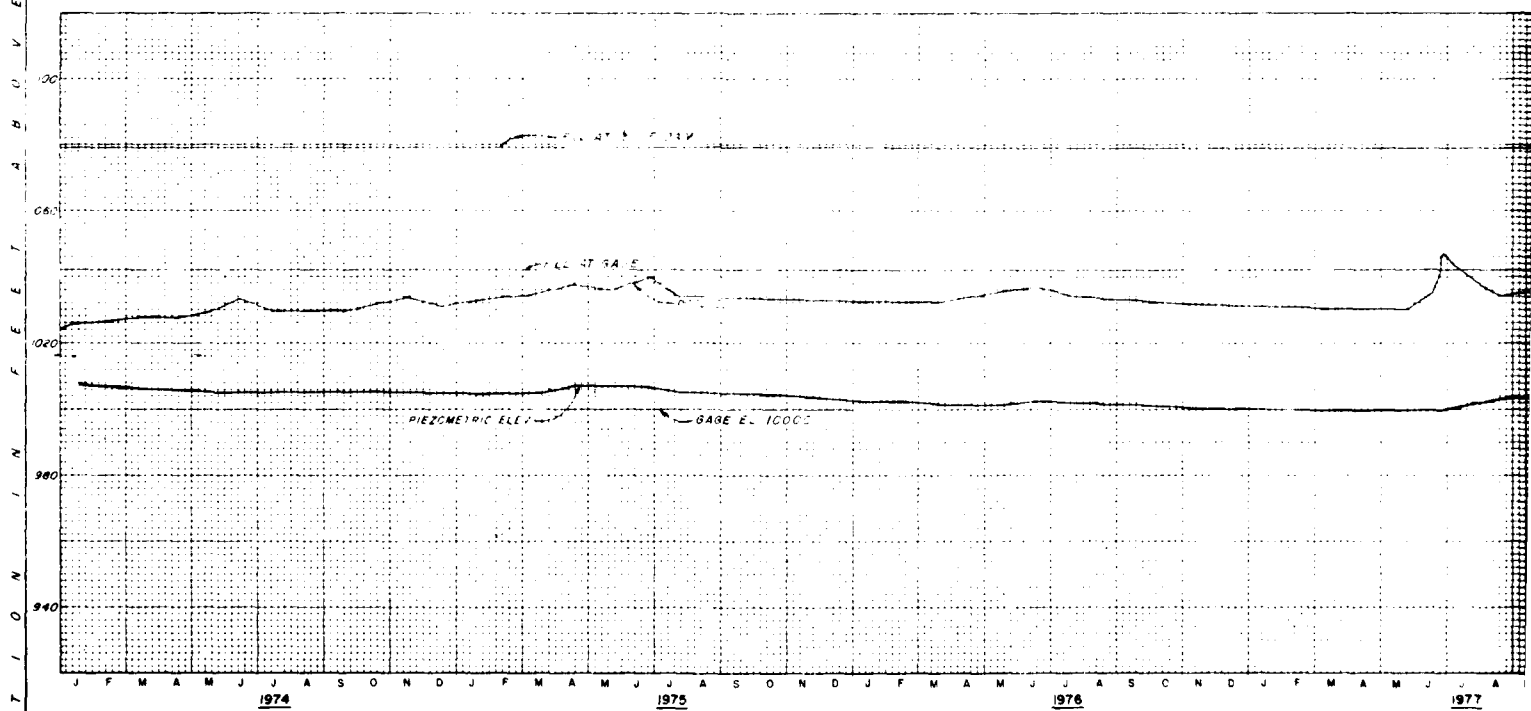
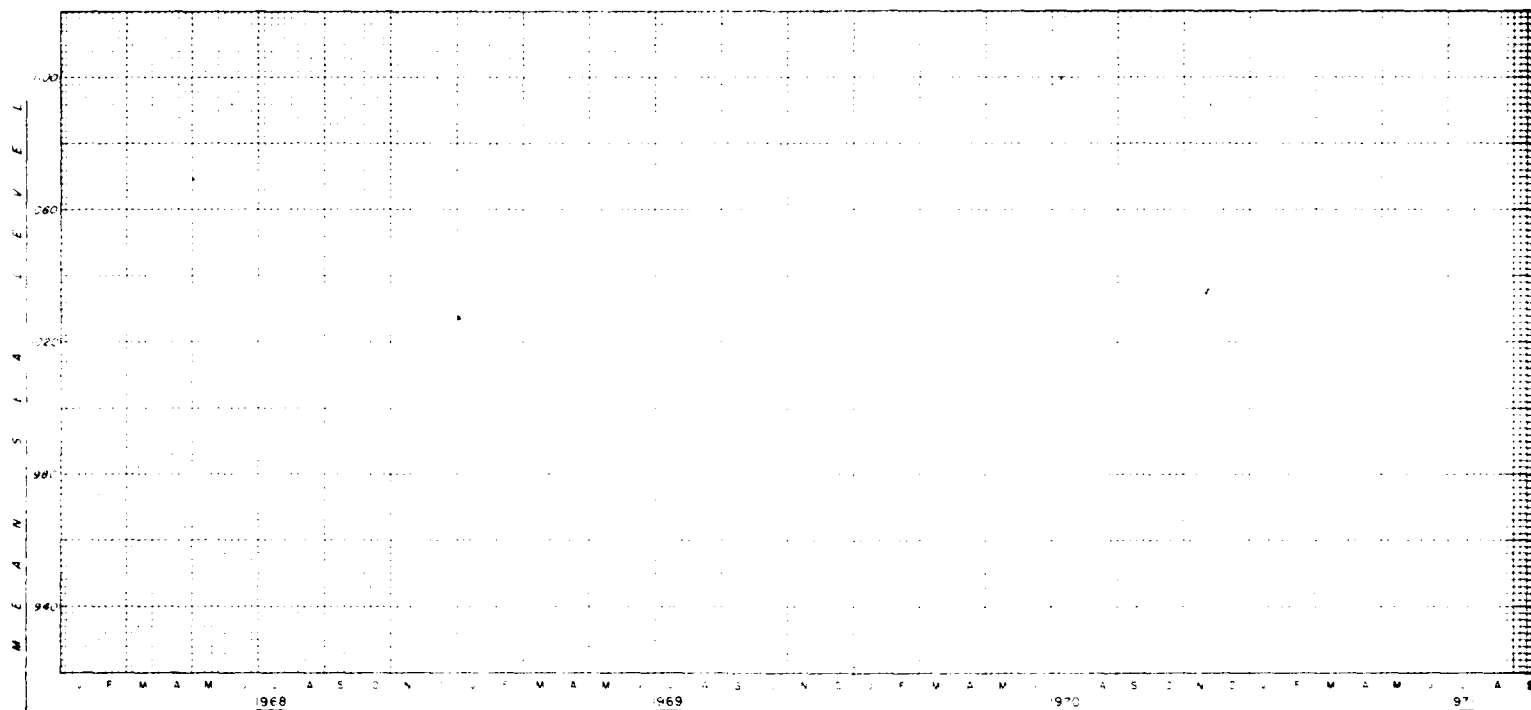
INSTRUMENTATION PLOTS
 PP-56-1 (SHANNON-WILSON CELL)

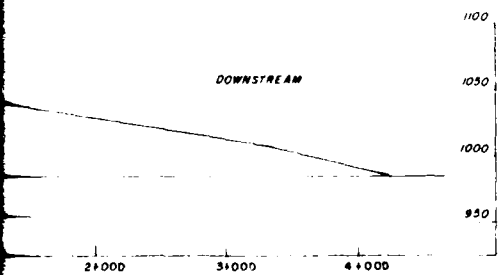
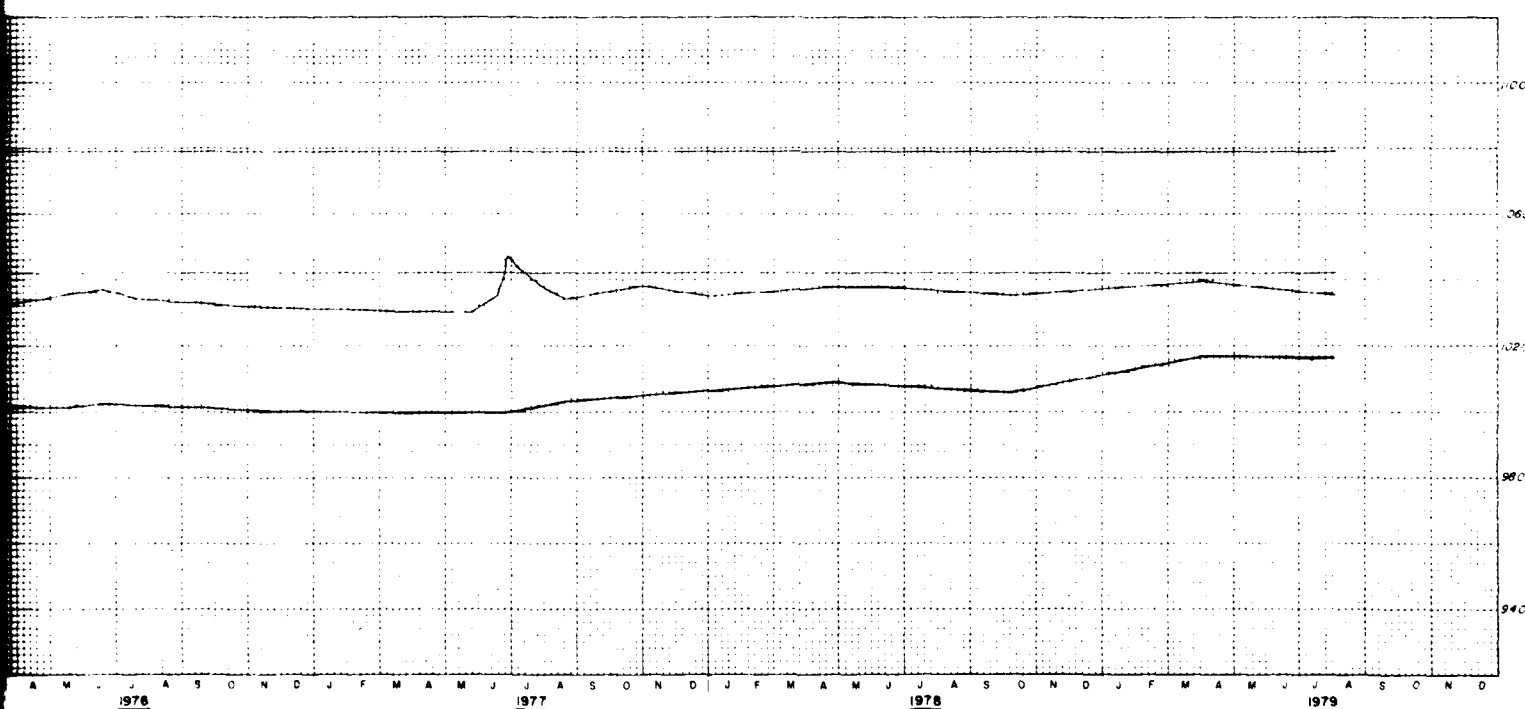
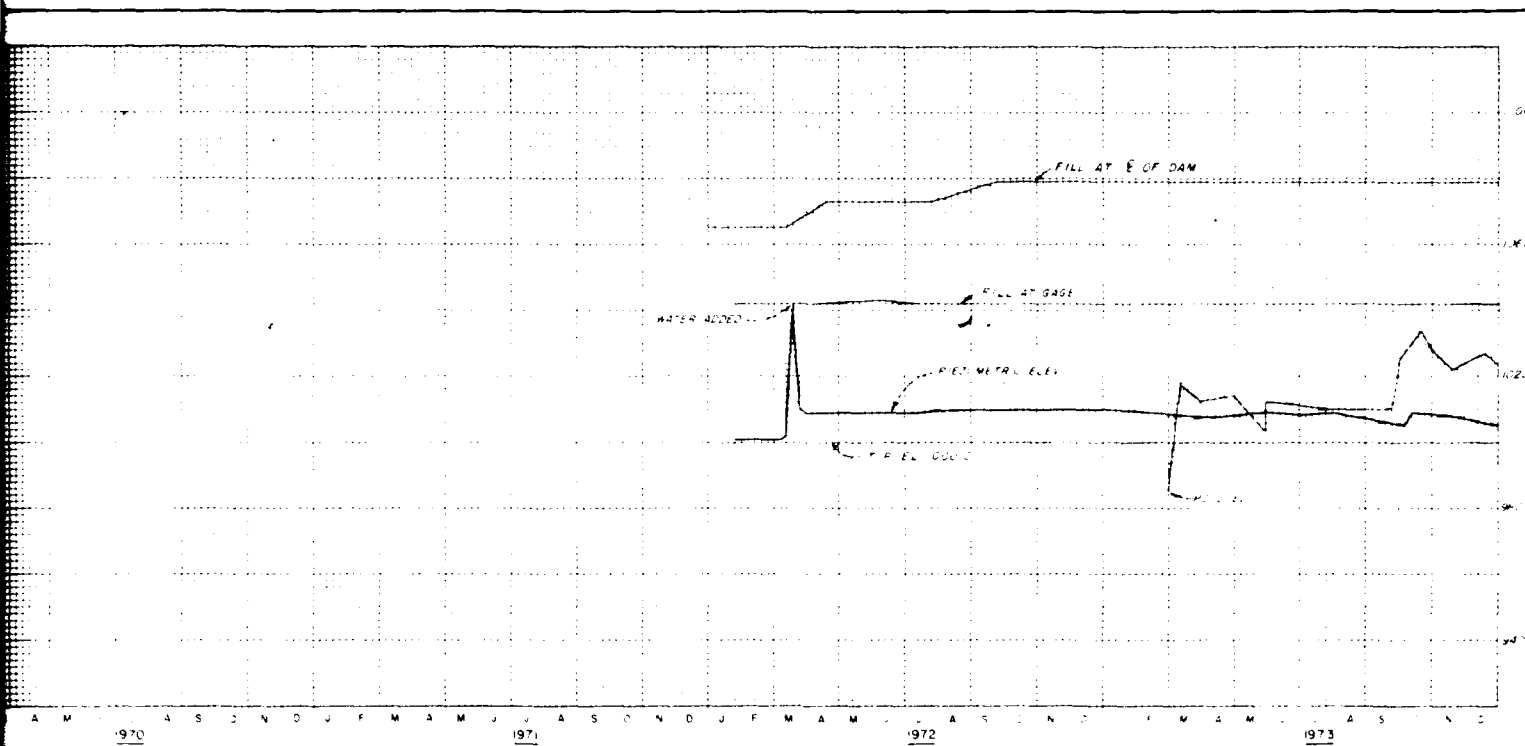
In 1 sheet

Sheet No. 1
 CORPS OF ENGINEERS U. S. ARMY
 KANSAS CITY DISTRICT

Scale as shown

FILE NO. 0-5-1285
 AUGUST 1979



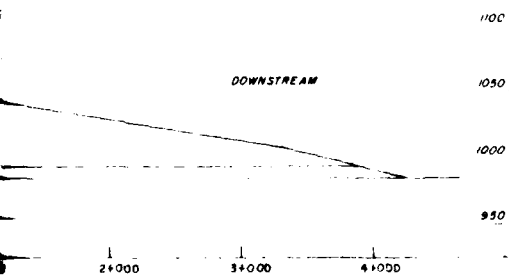
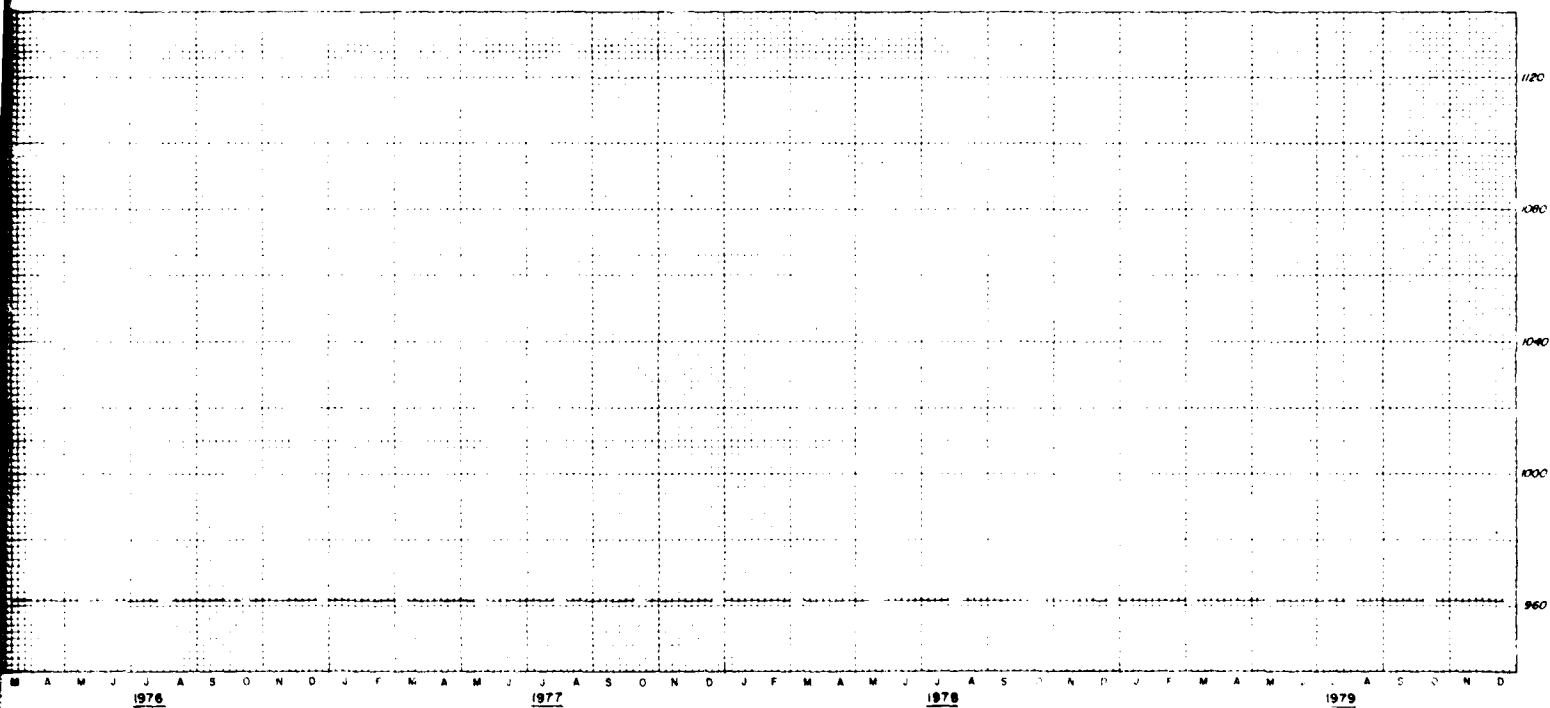
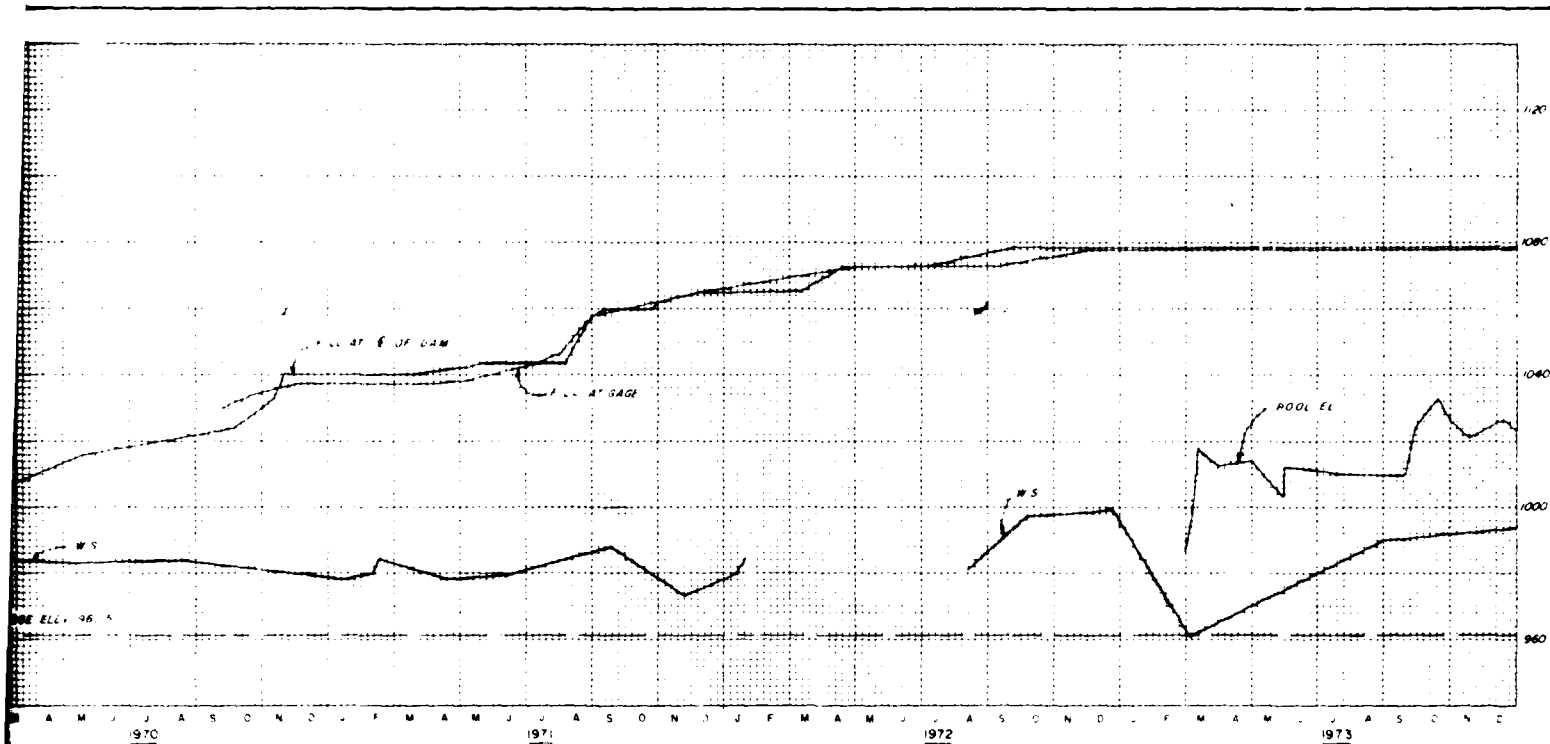


LEGEND
 OPEN TUBE ○
 PNEUMATIC CELL ●

Revised August 1979
 MARAIS DES CYGNES RIVER KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
 PP-56-2 (OPEN TUBE)

In 1 sheet
 Sheet No. 1
 Scale as shown
 CORPS OF ENGINEERS U.S. ARMY
 KANSAS CITY DISTRICT
 FILE NO 0-5-1286
 AUGUST 1975



MELVERN LAKE

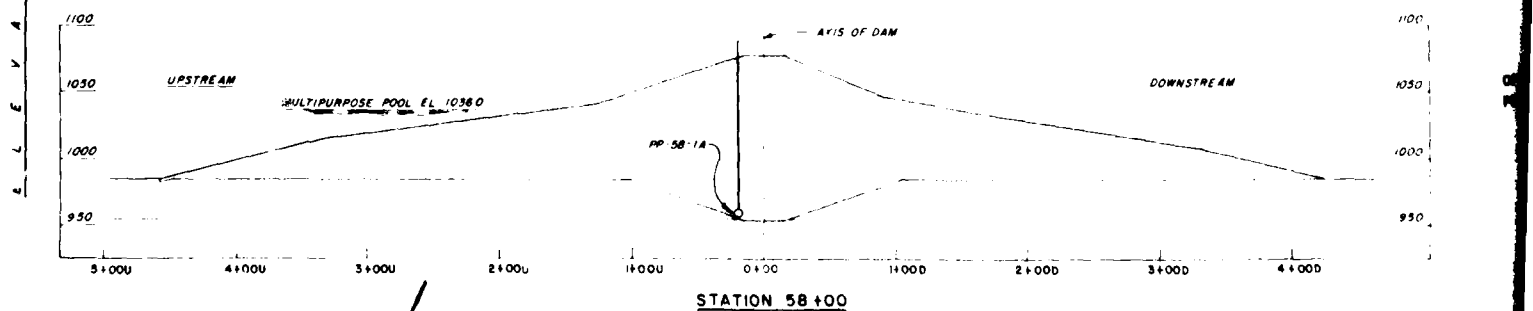
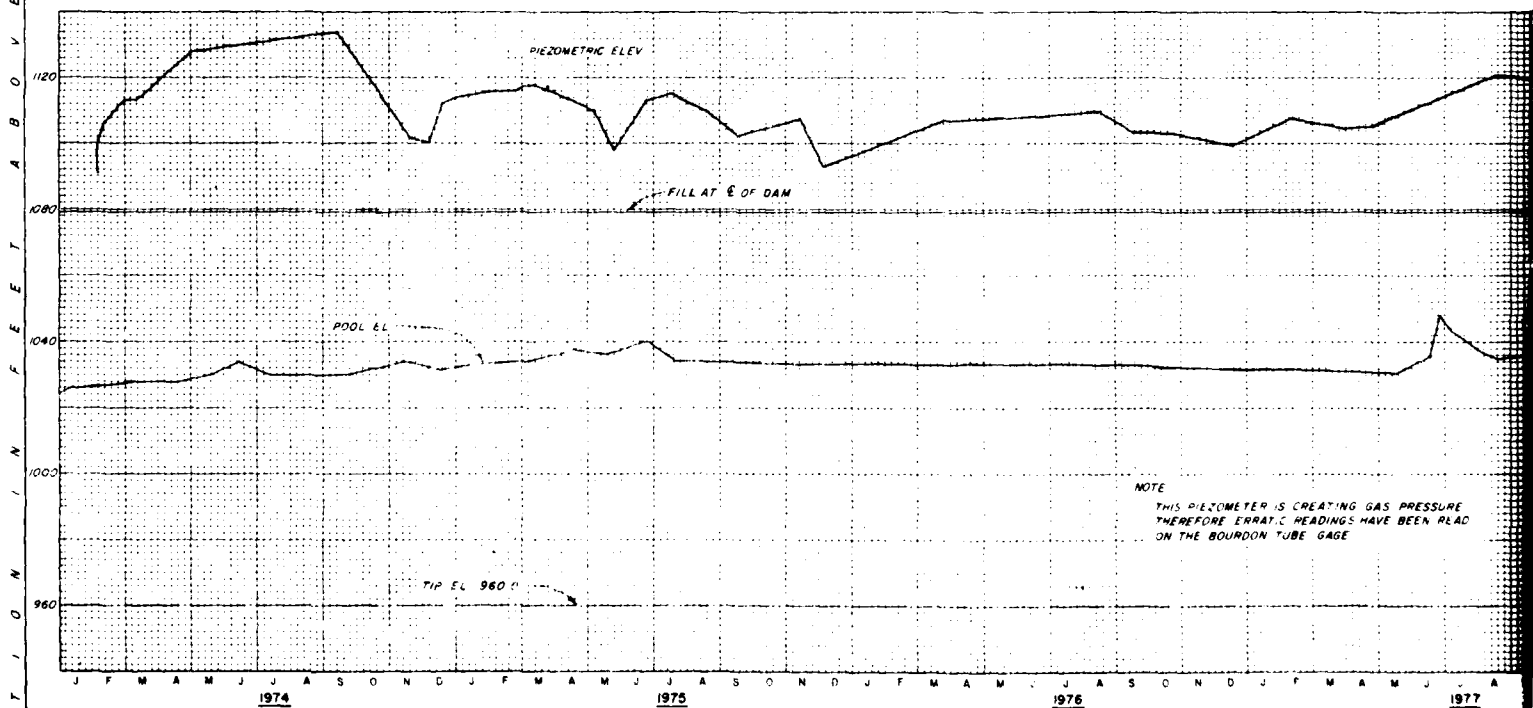
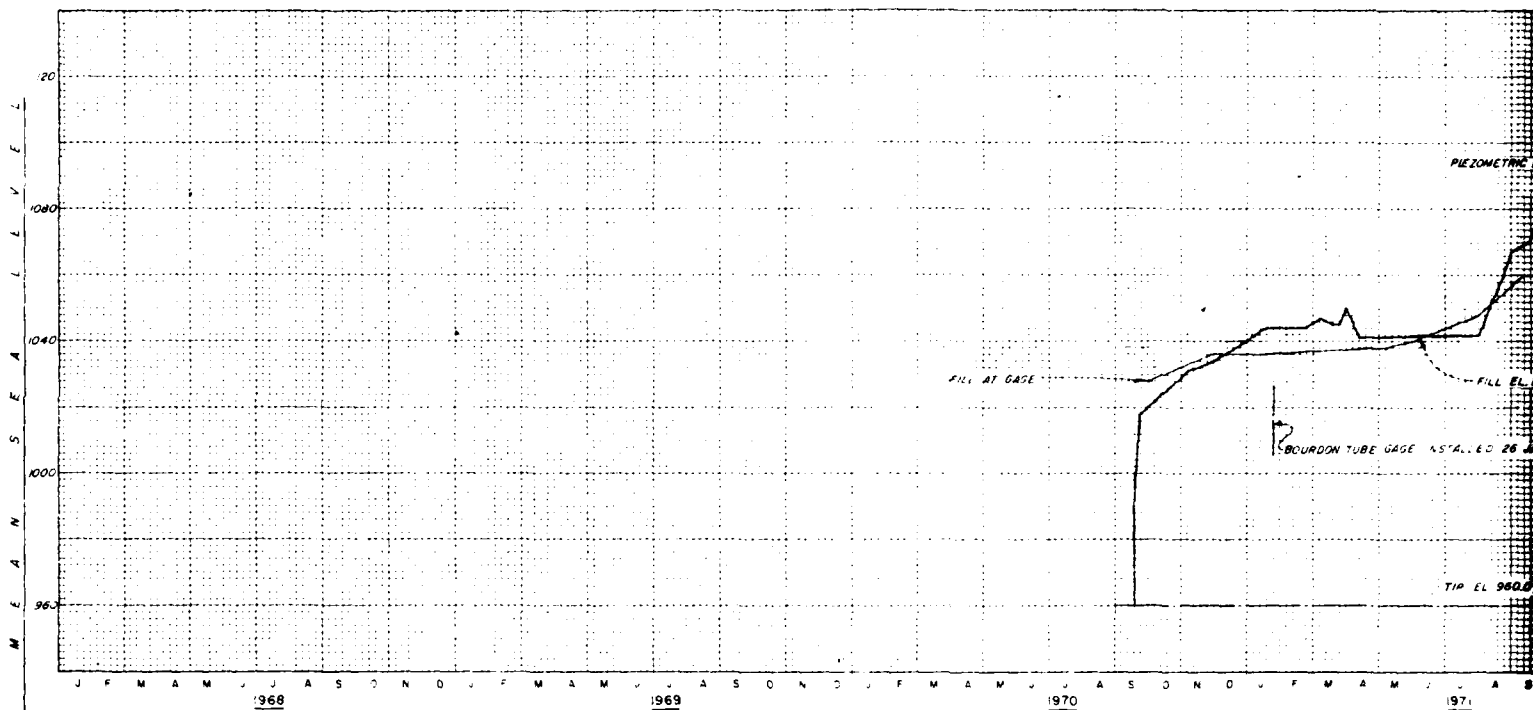
INSTRUMENTATION PLOTS
PP-58-1 (SHANNON-WILSON CELL)

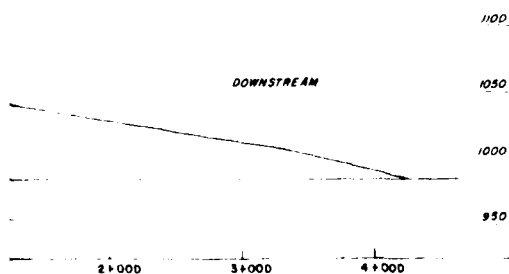
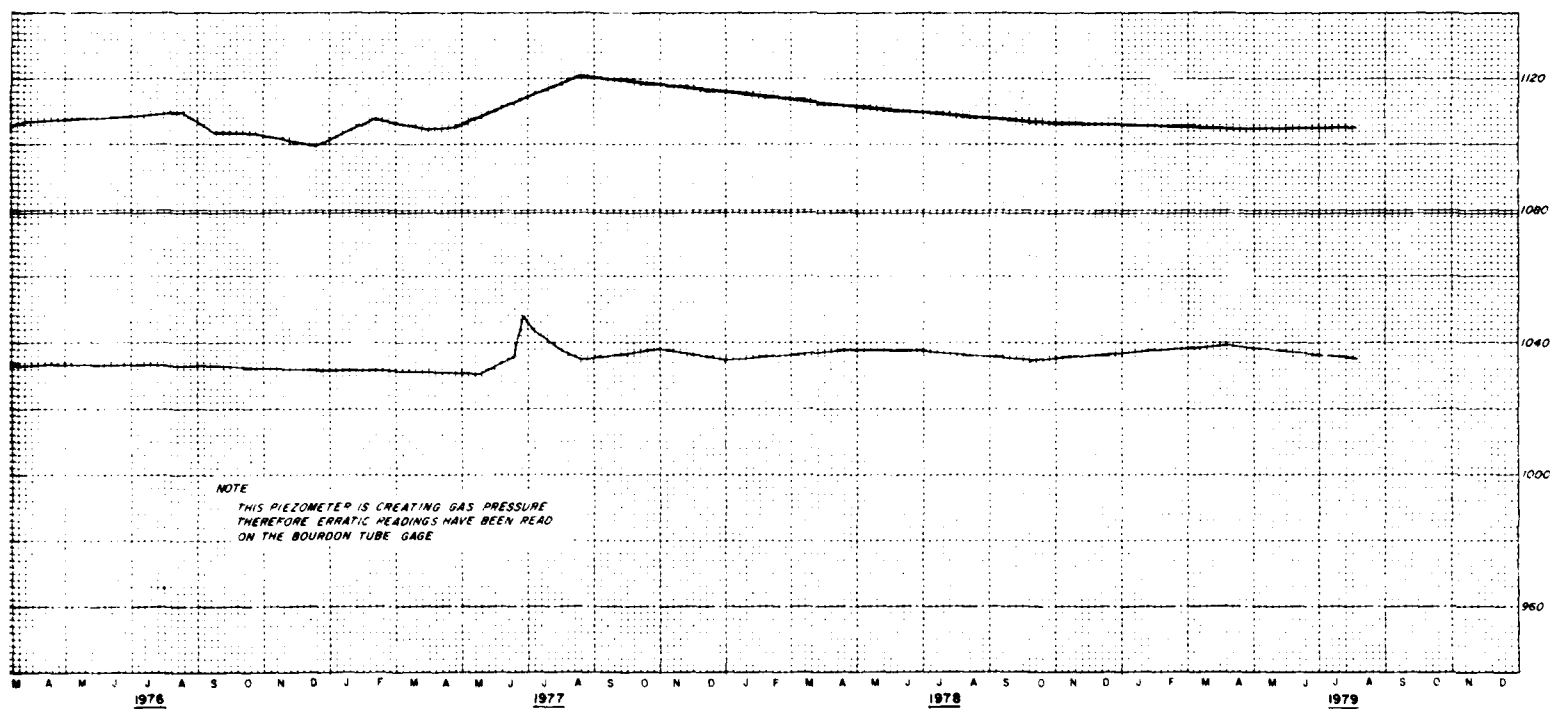
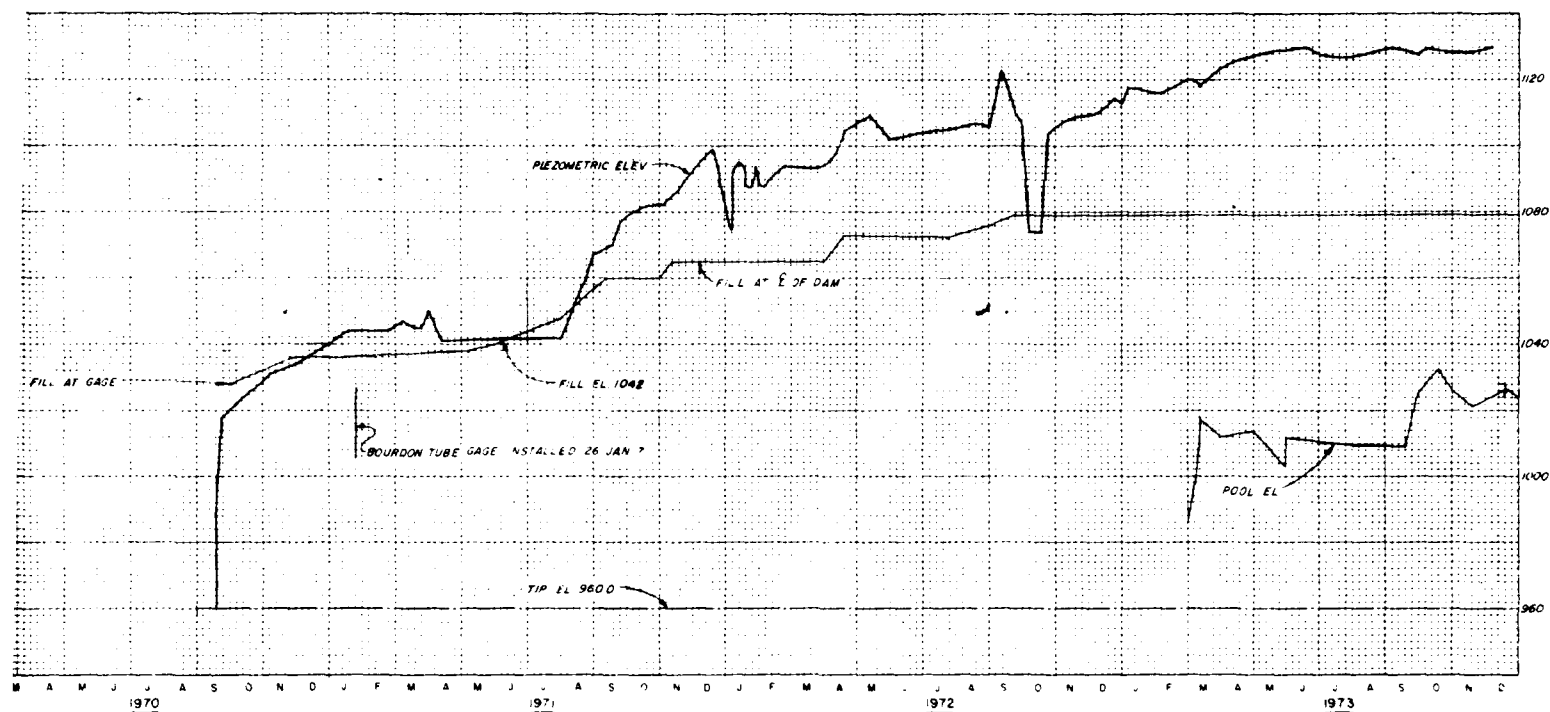
In 1 sheet

Sheet No. 1

Scale: as shown

FILE NO. O-5-1287
AUGUST 1975





LEGEND
 OPEN TUBE ○
 PNEUMATIC CELL ●

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 MARAIS DES CYGNES RIVER KANSAS
MELVERN LAKE

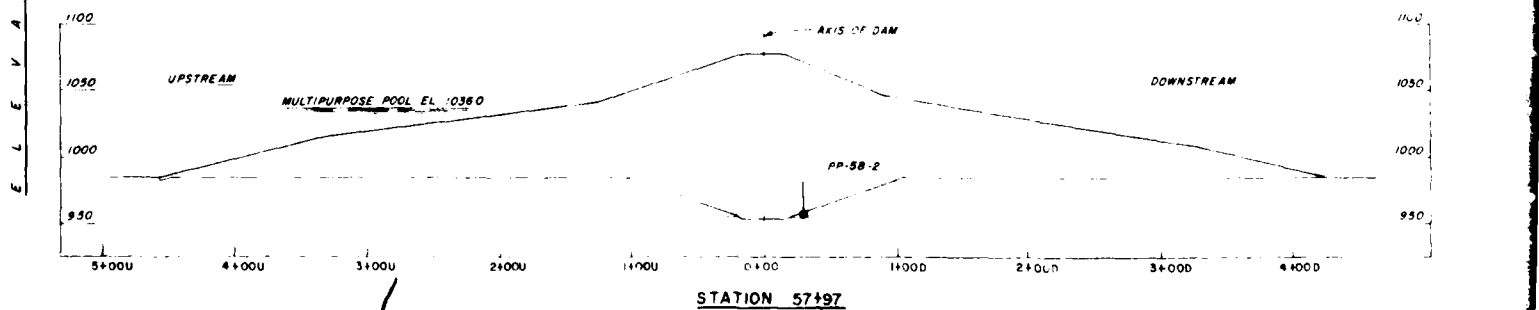
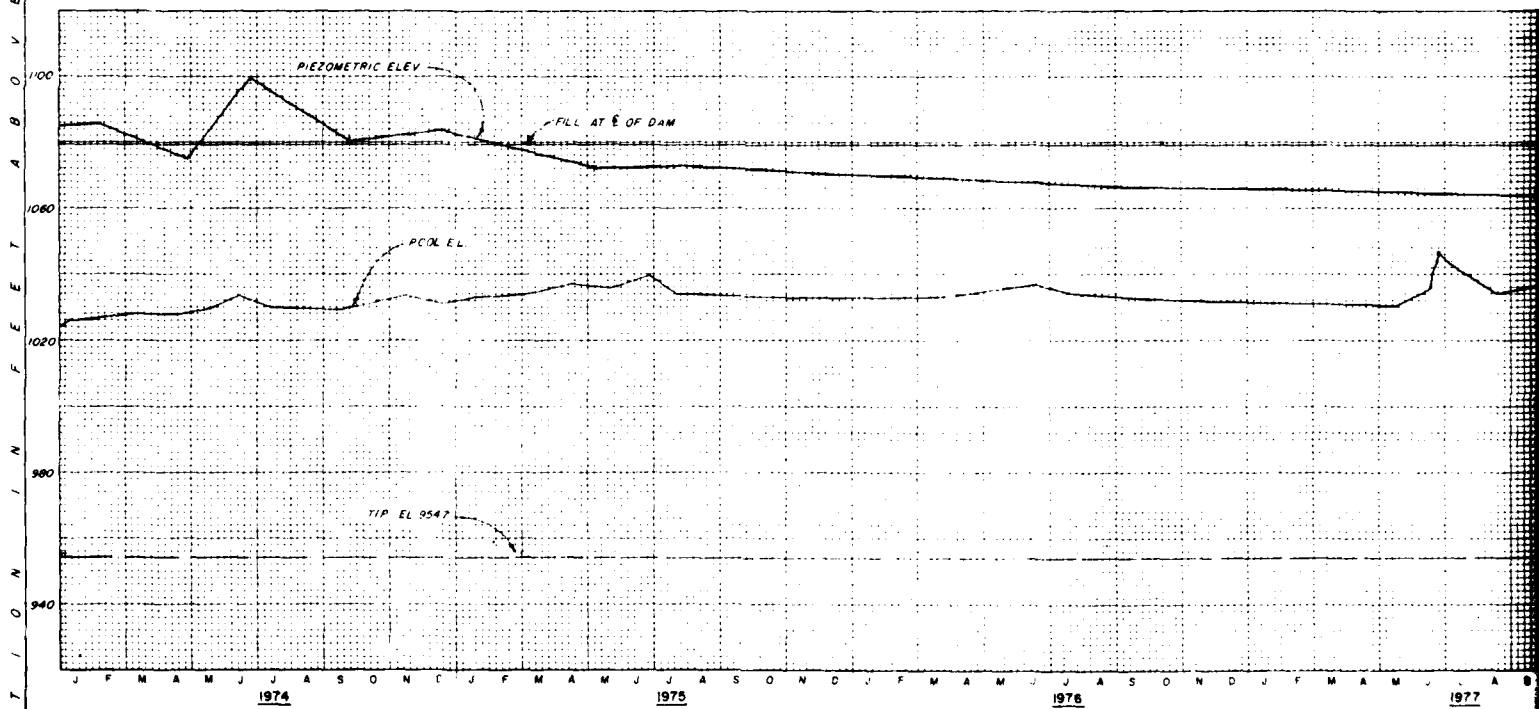
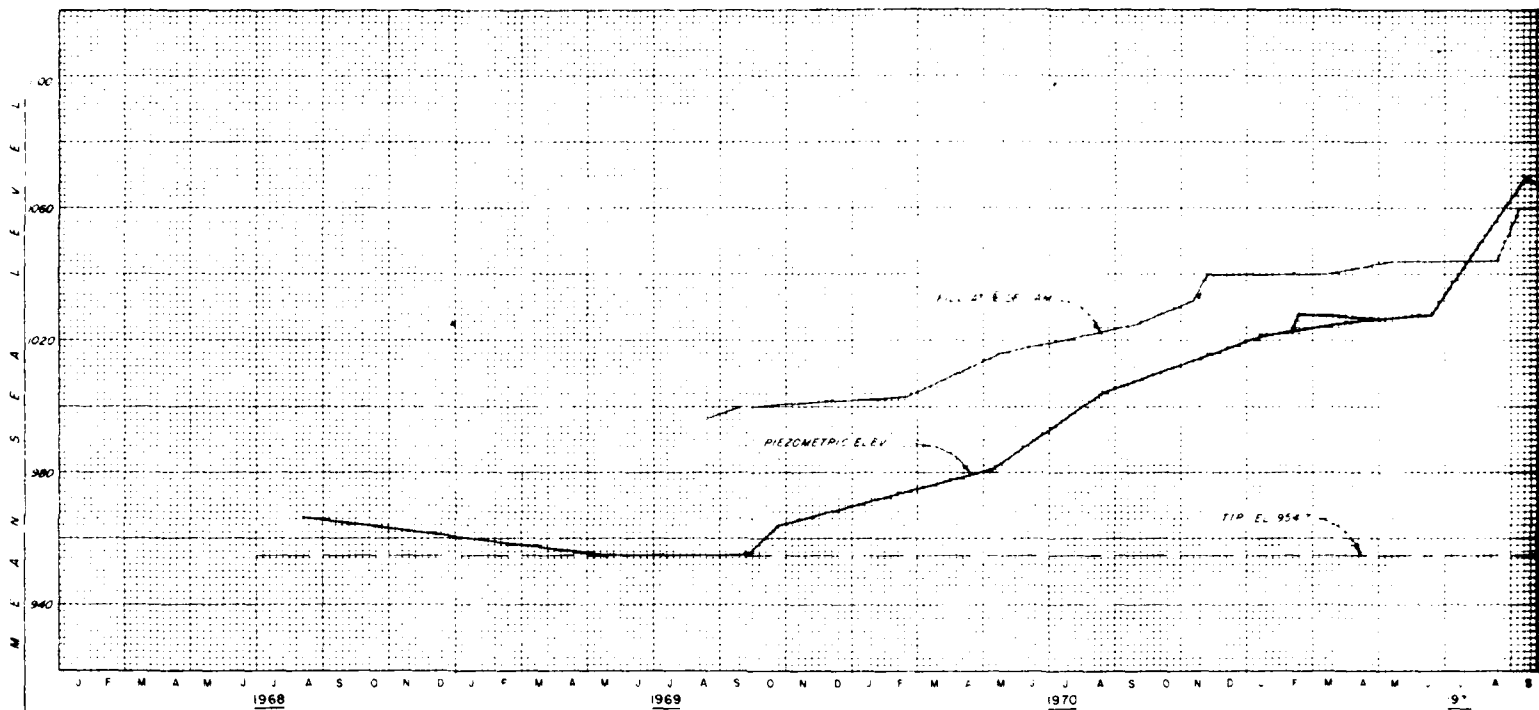
INSTRUMENTATION PLOTS
 PP-58-1A (OPEN TUBE)

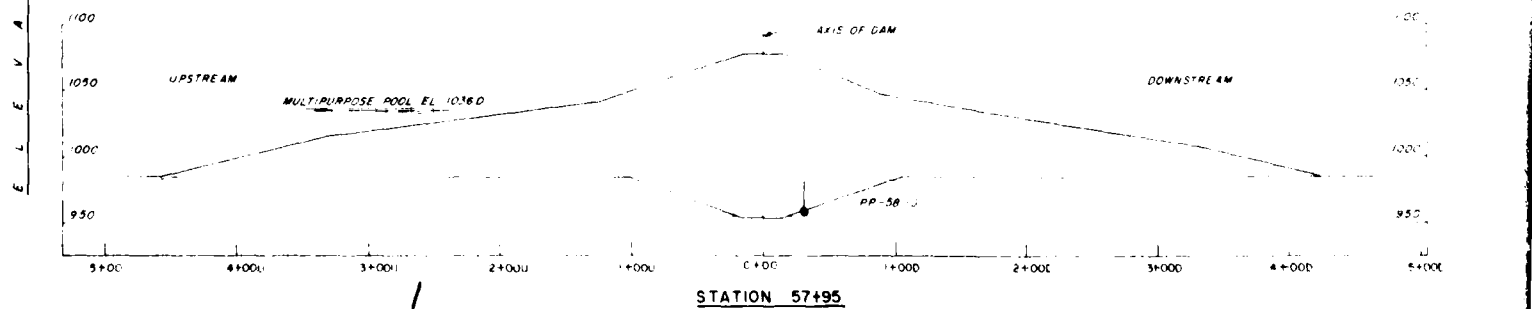
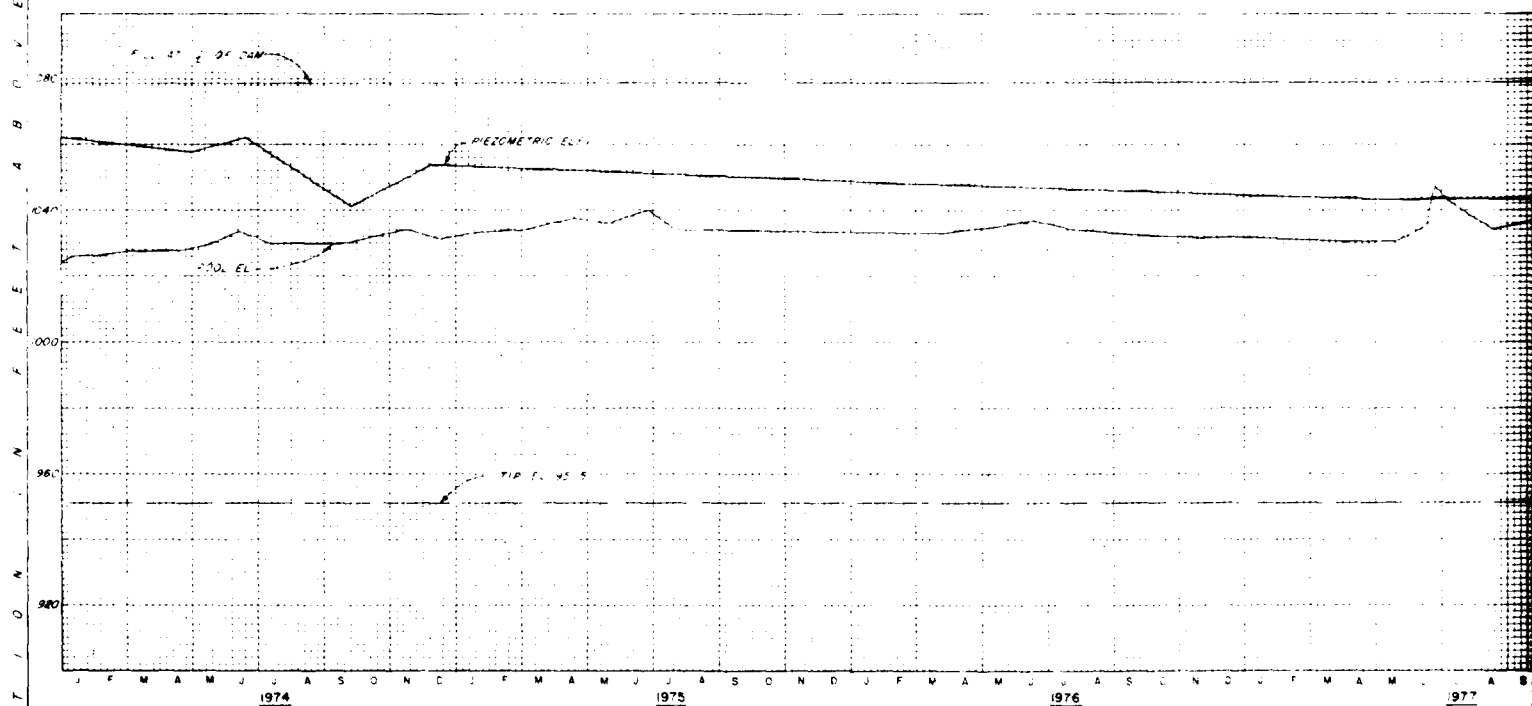
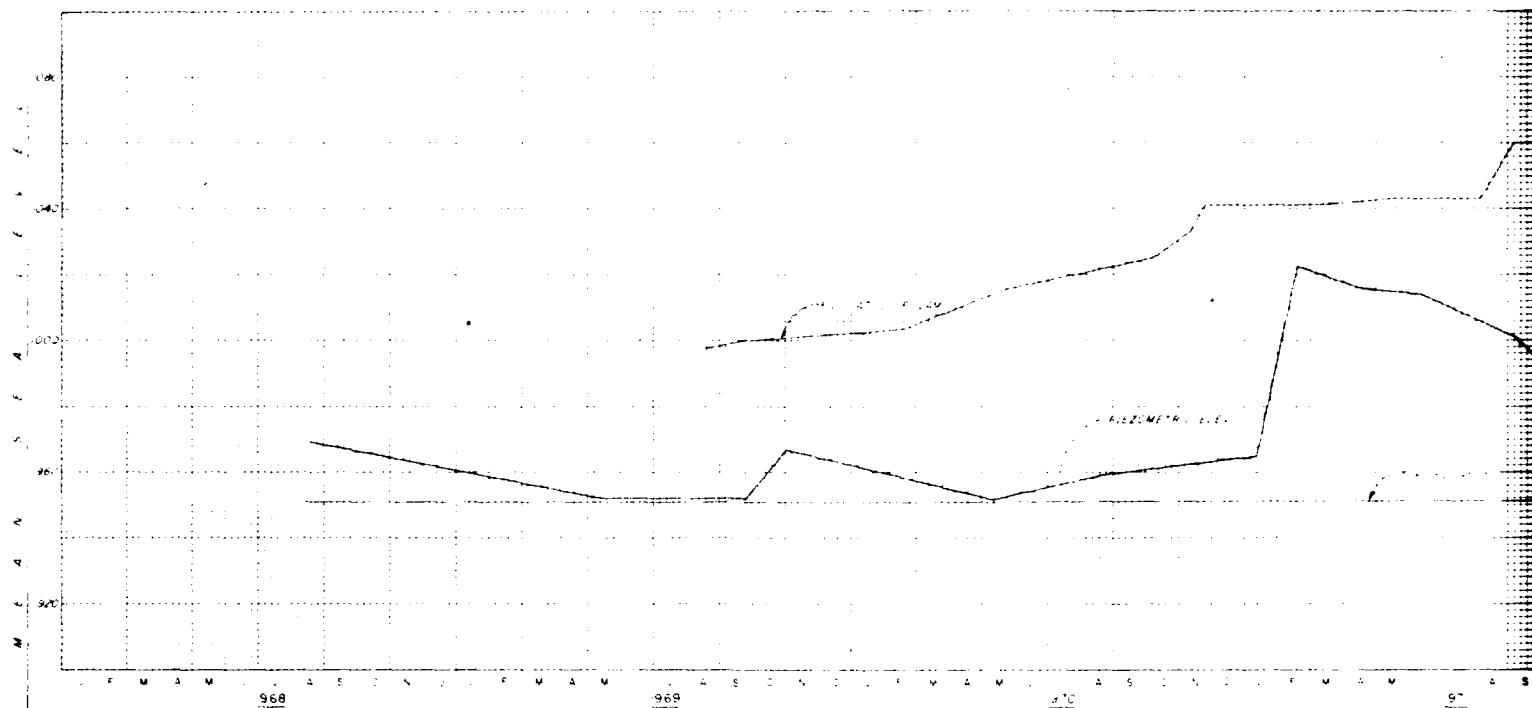
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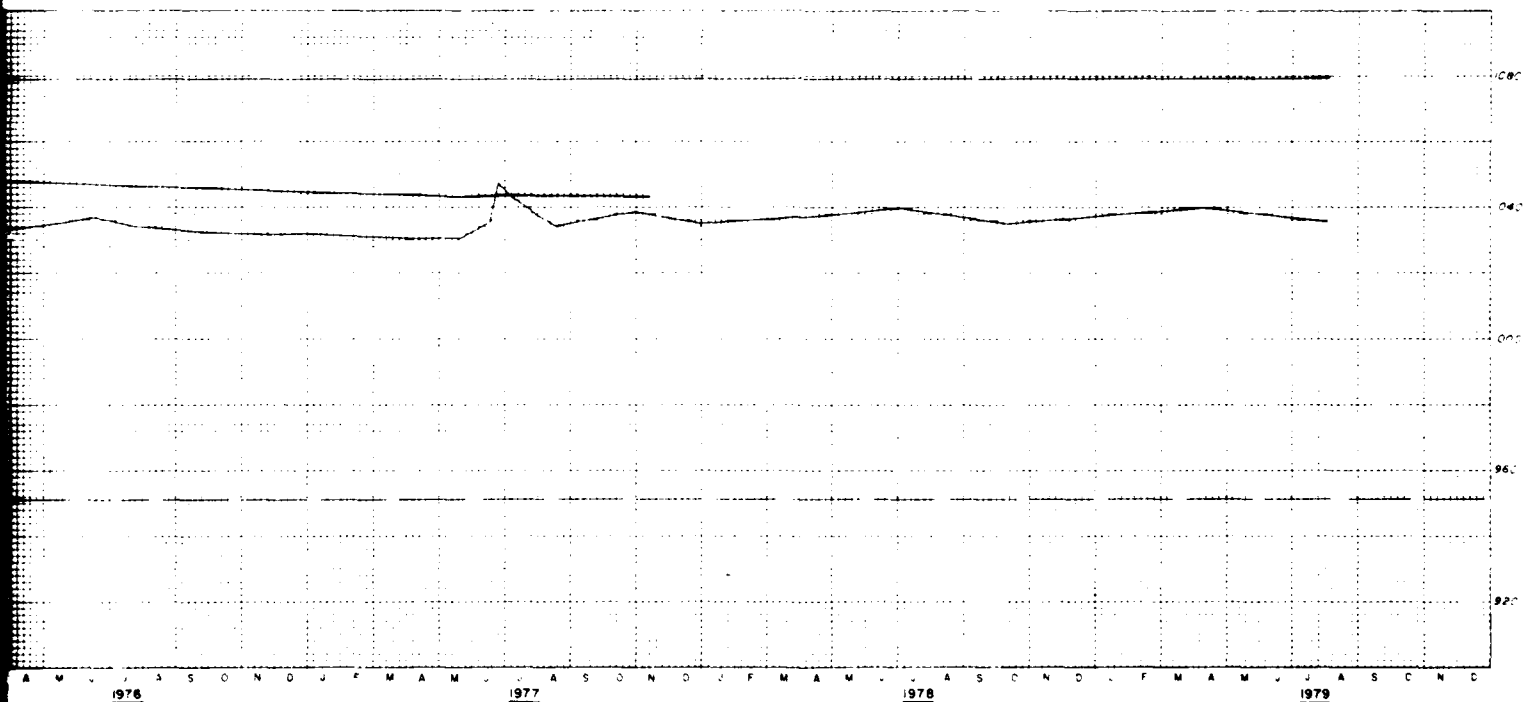
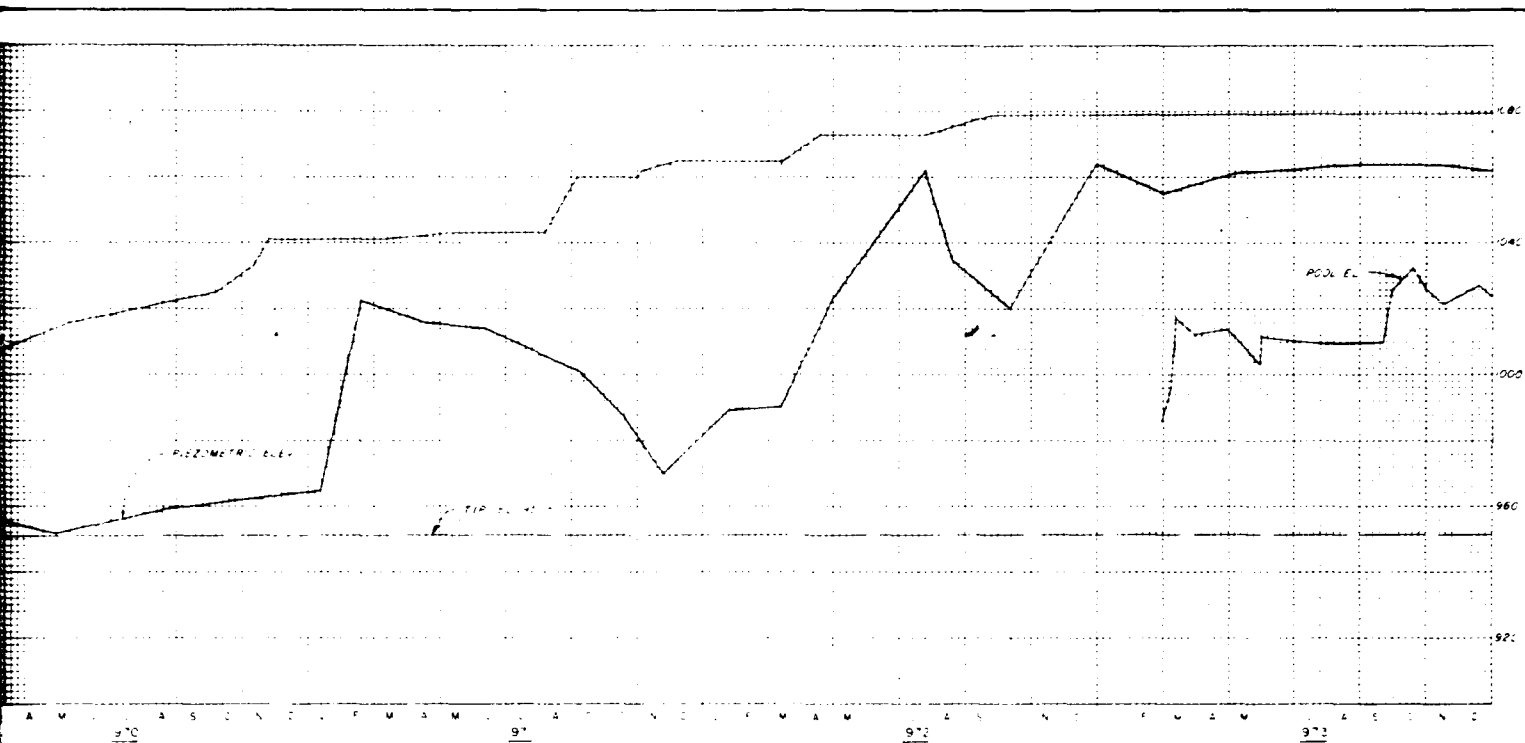
Sheet No. 1

Scale as shown

CORPS OF ENGINEERS U. S. ARMY
 KANSAS CITY DISTRICT
 FILE NO. 0-5-1288
 AUGUST 1975







DOWNSTREAM

1100
1050
1000
950
5+000

LEGEND

OPEN TUBE
 PNEUMATIC CELL

Revised August 1979
MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
PP-58-3 (SHANNON-WILSON CELL)

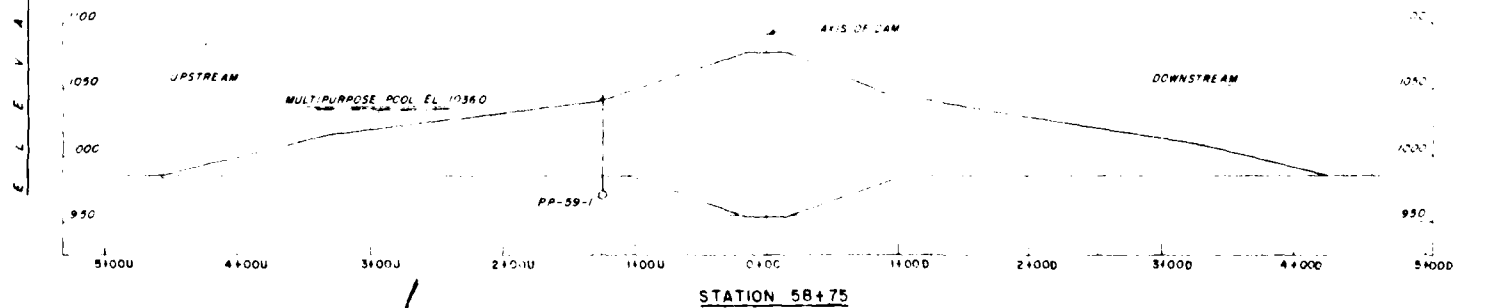
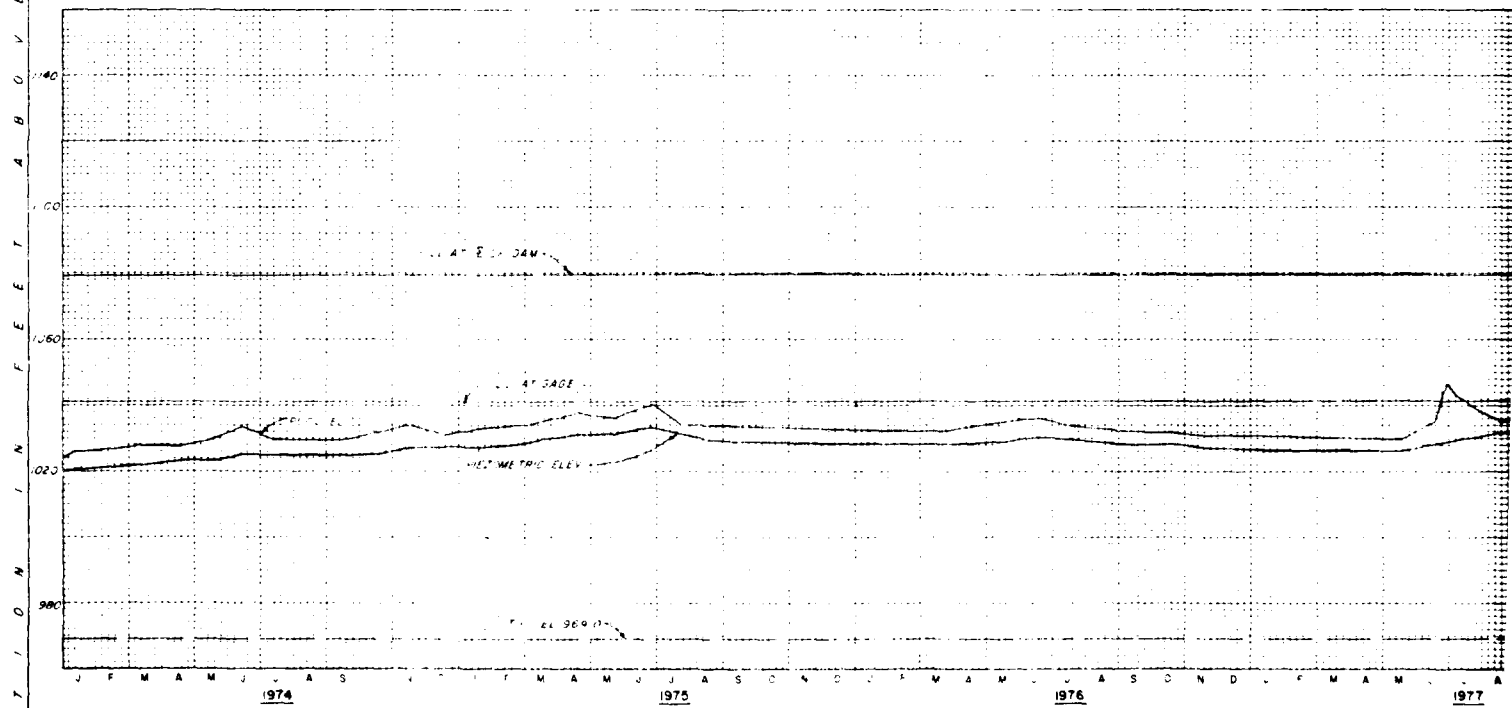
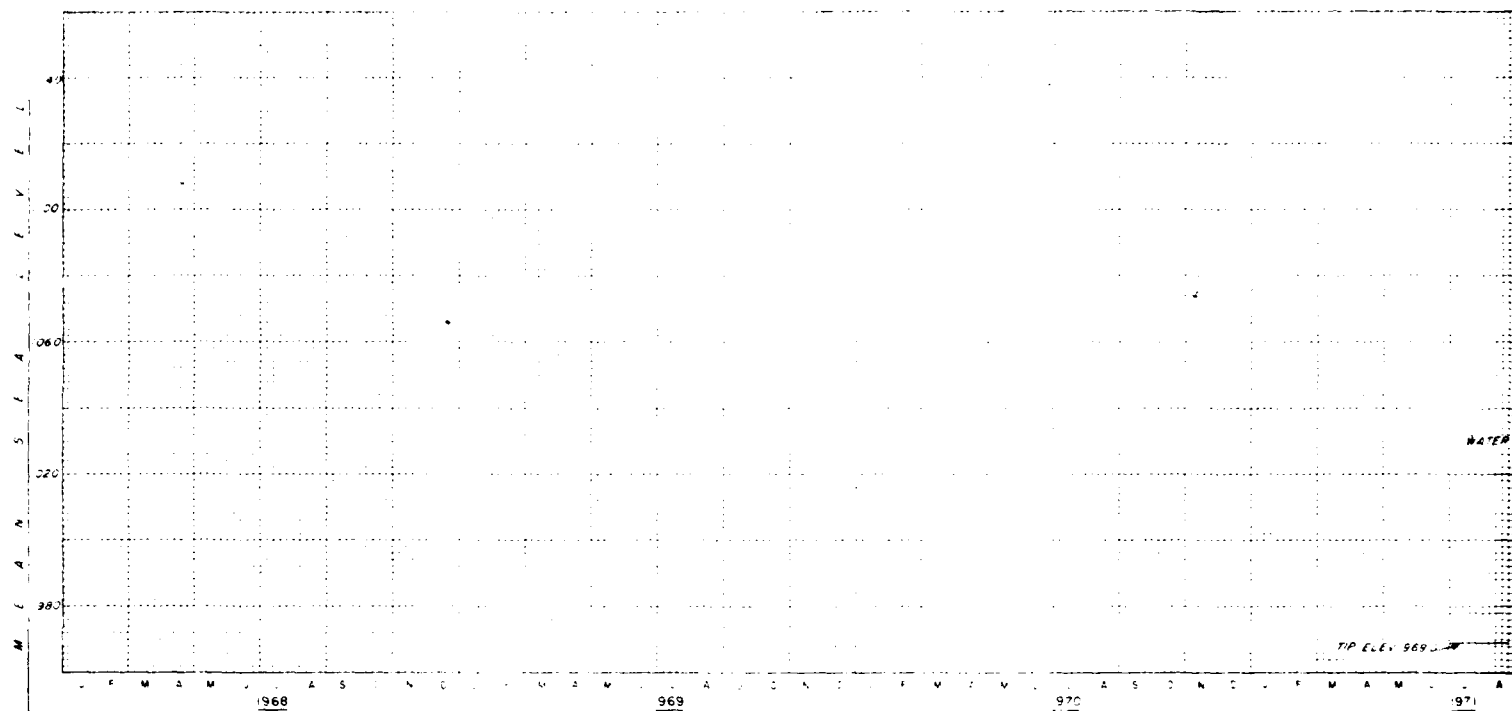
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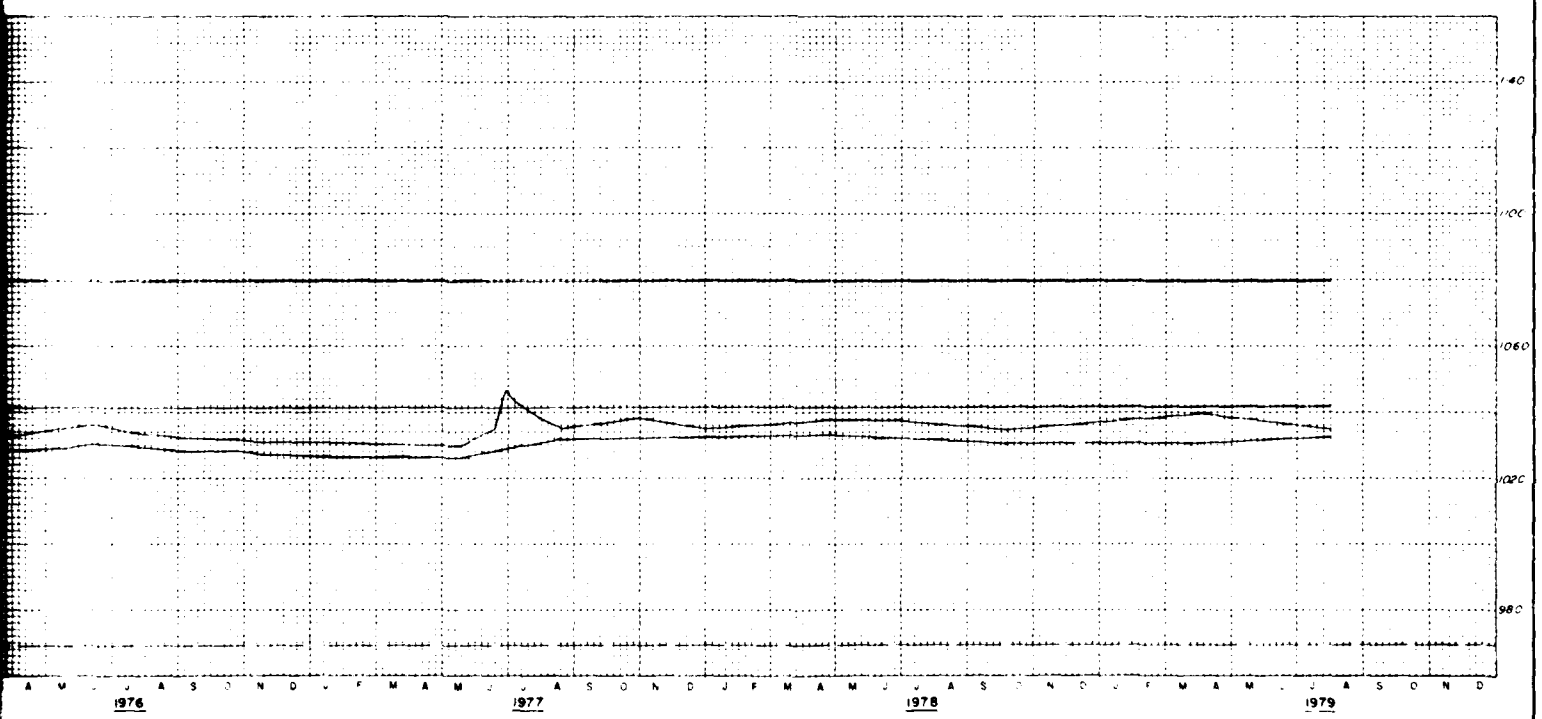
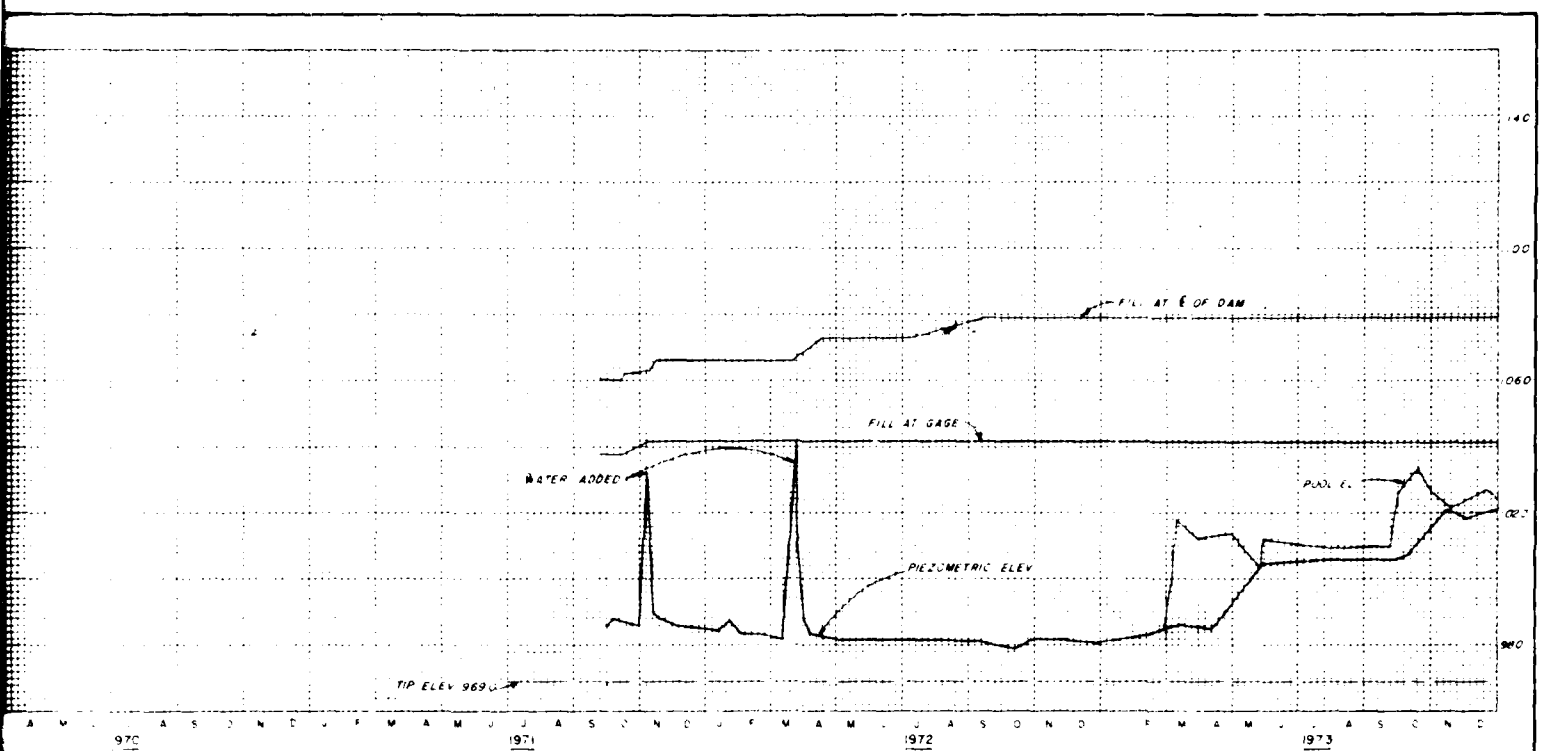
Sheet No. 1

Scale as shown

CORPUS ENGINEERS & ARCHT.
KANSAS CITY DISTRICT

FILE NO C-5-1290
AUGUST 1975





DOWNSTREAM

LEGEND
 OPEN TUBE)
 PNEUMATIC CELL ●

MELVERN LAKE

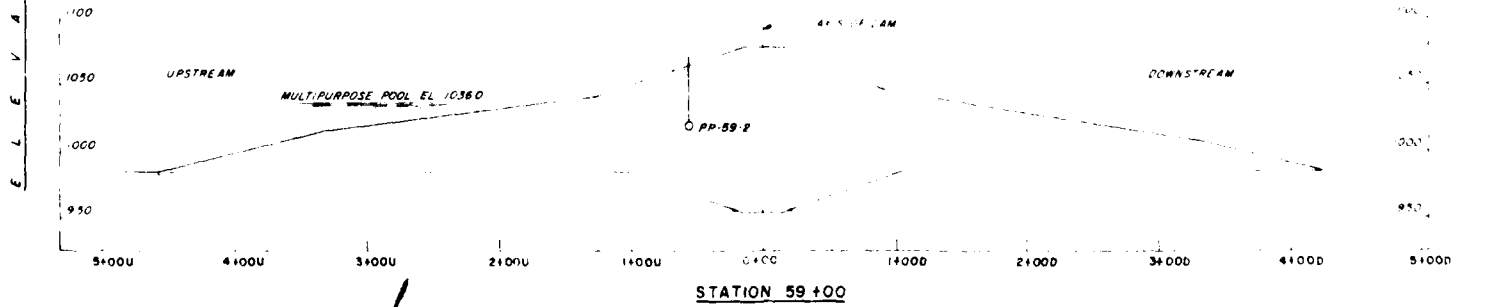
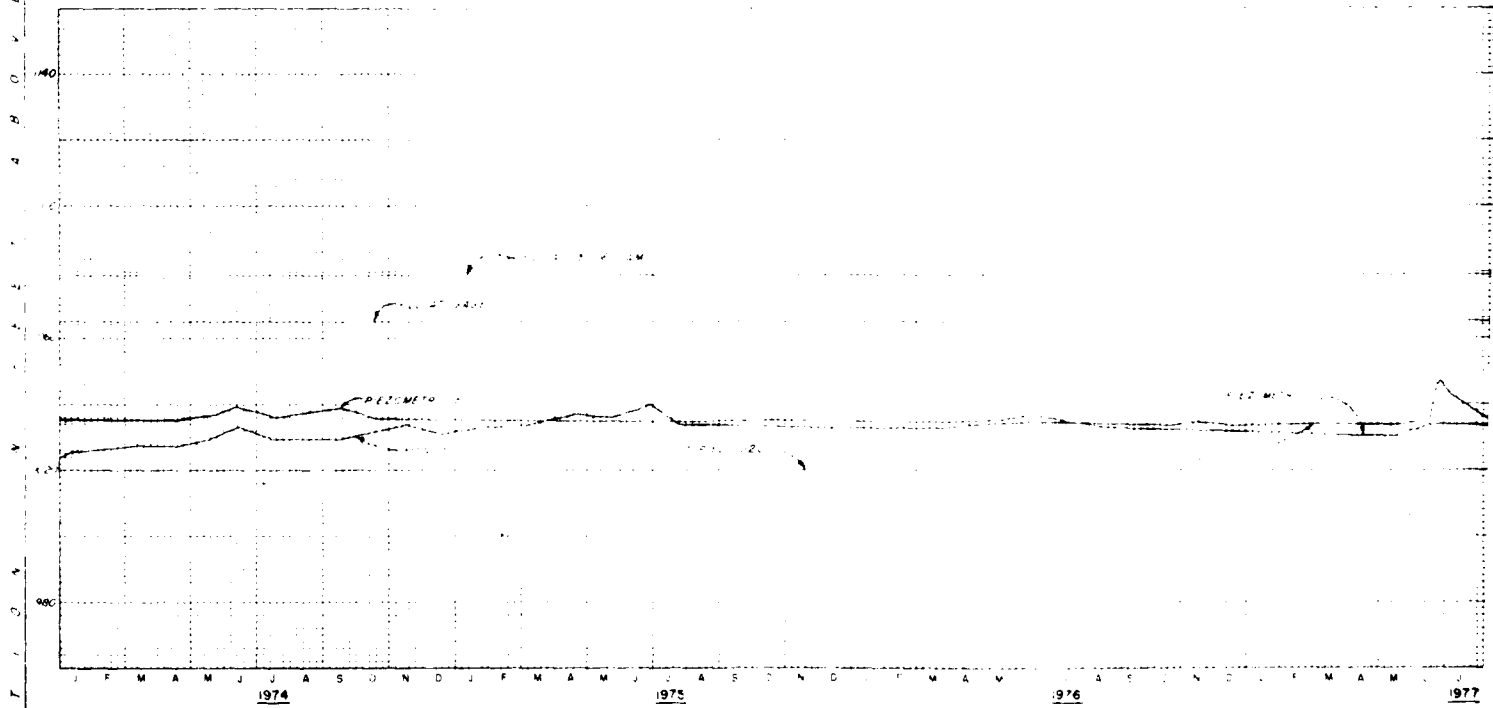
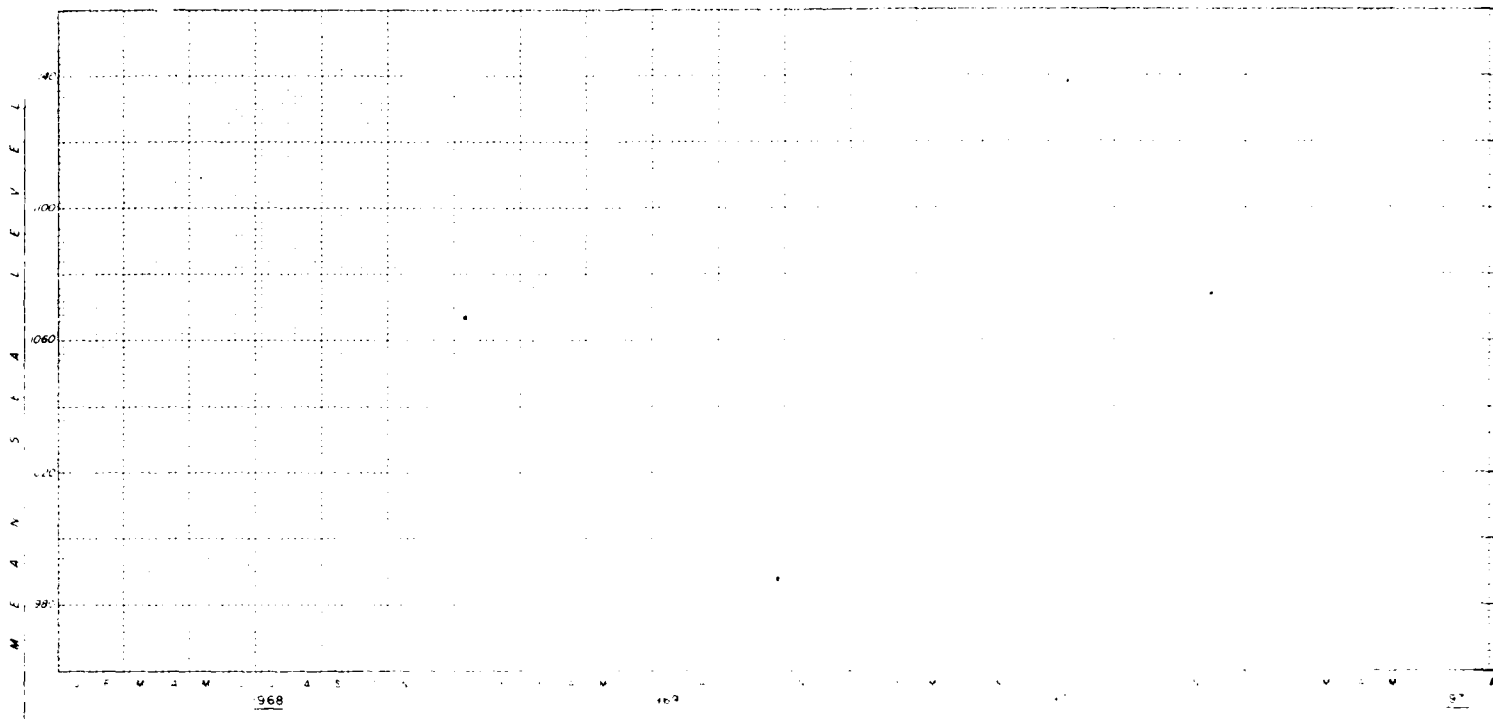
INSTRUMENTATION PLOTS
 PP-59-1 (OPEN TUBE)

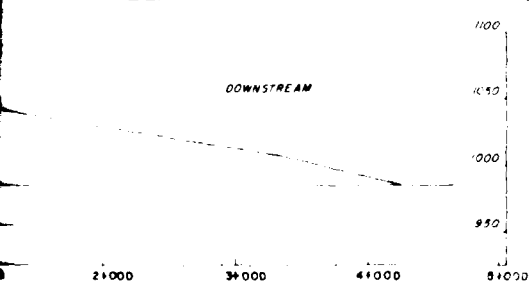
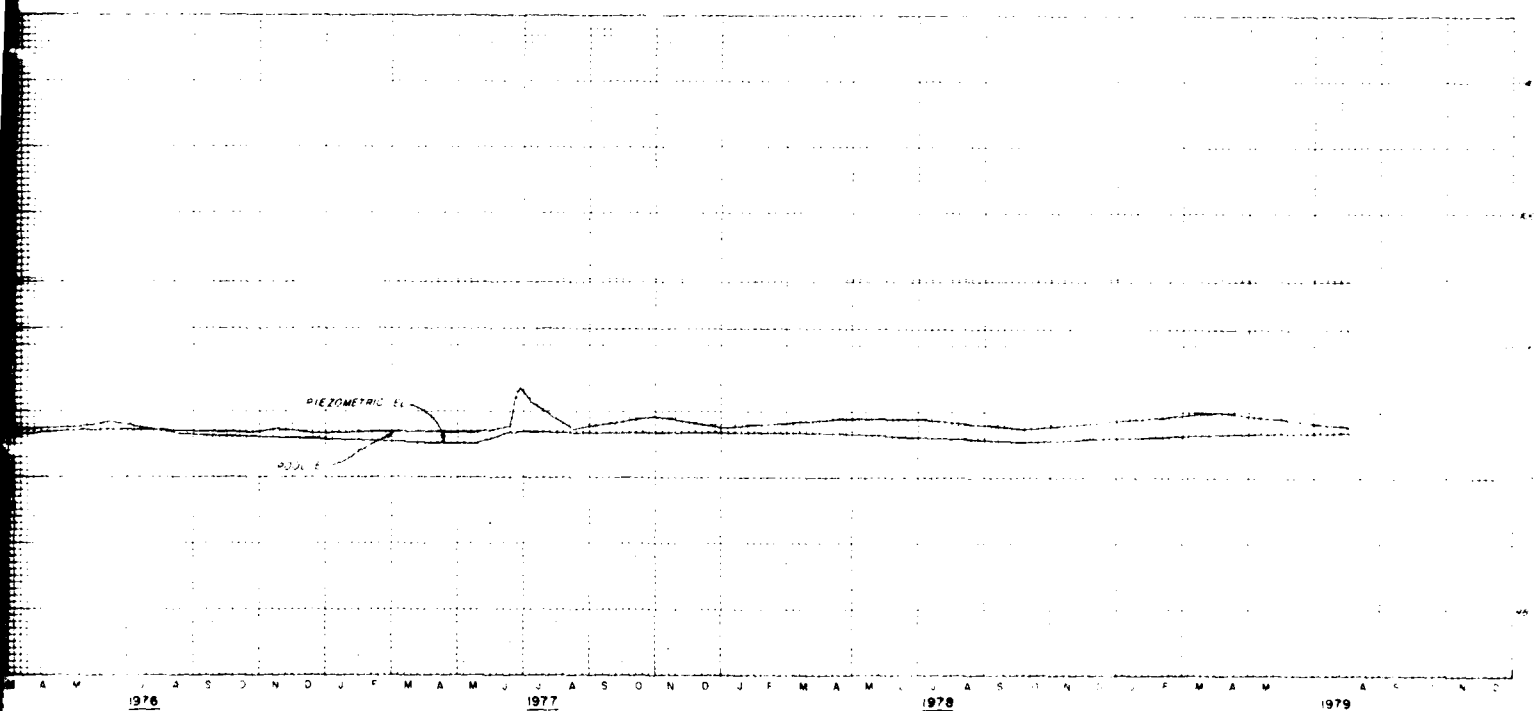
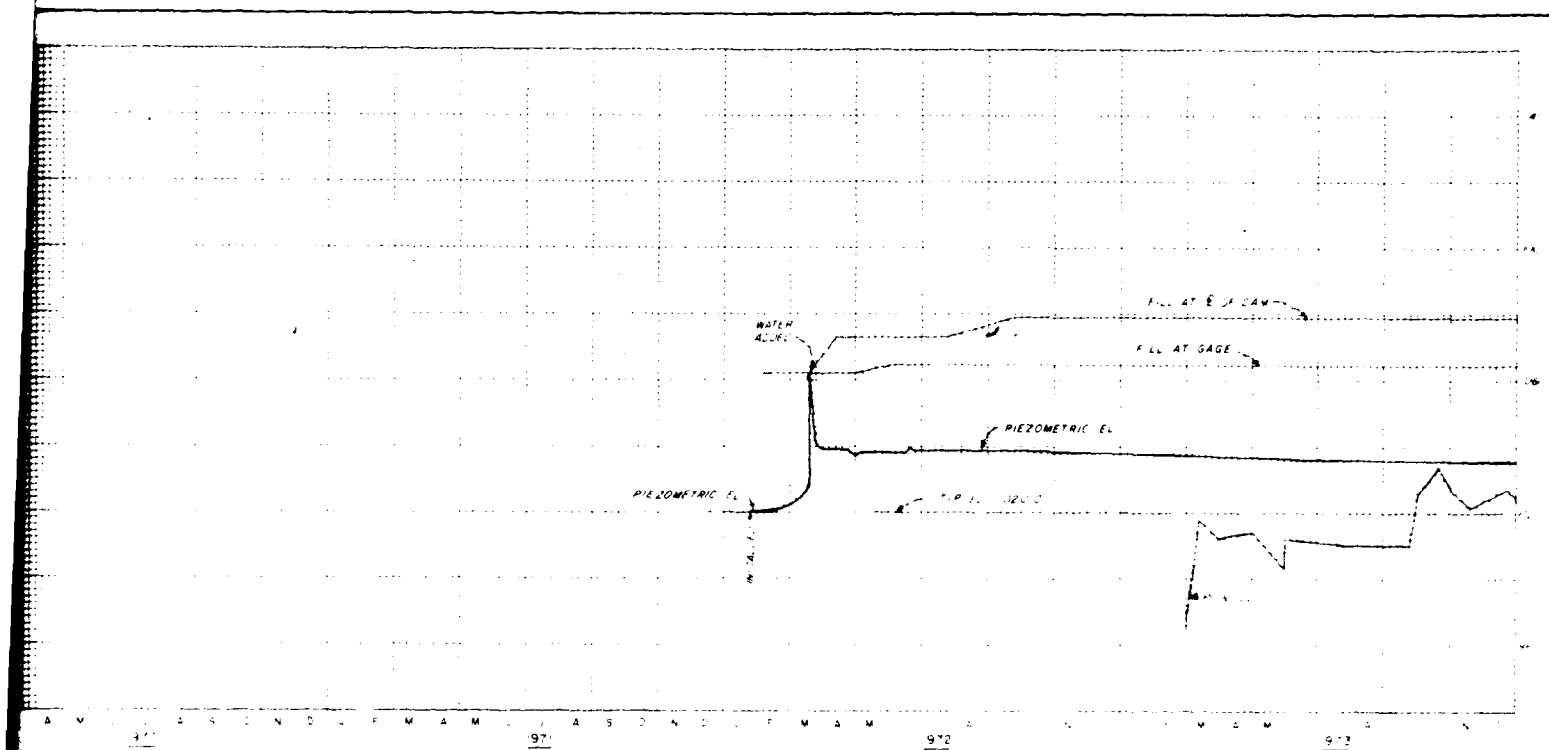
In 1 sheet

Sheet No. 1

Scale as shown

KANSAS ENGINEERS & ARCHITECTS
 KANSAS CITY, MISSOURI
 FILE NO. 0-5-1291
 AUGUST 1975





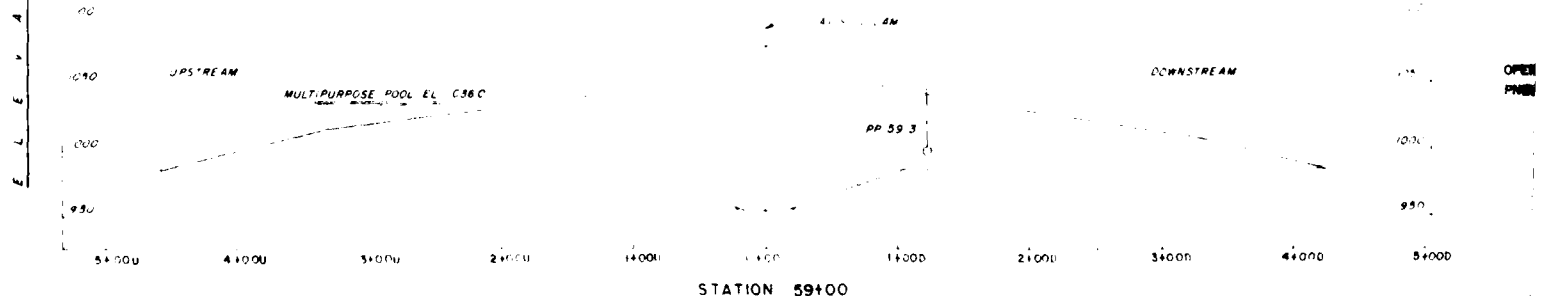
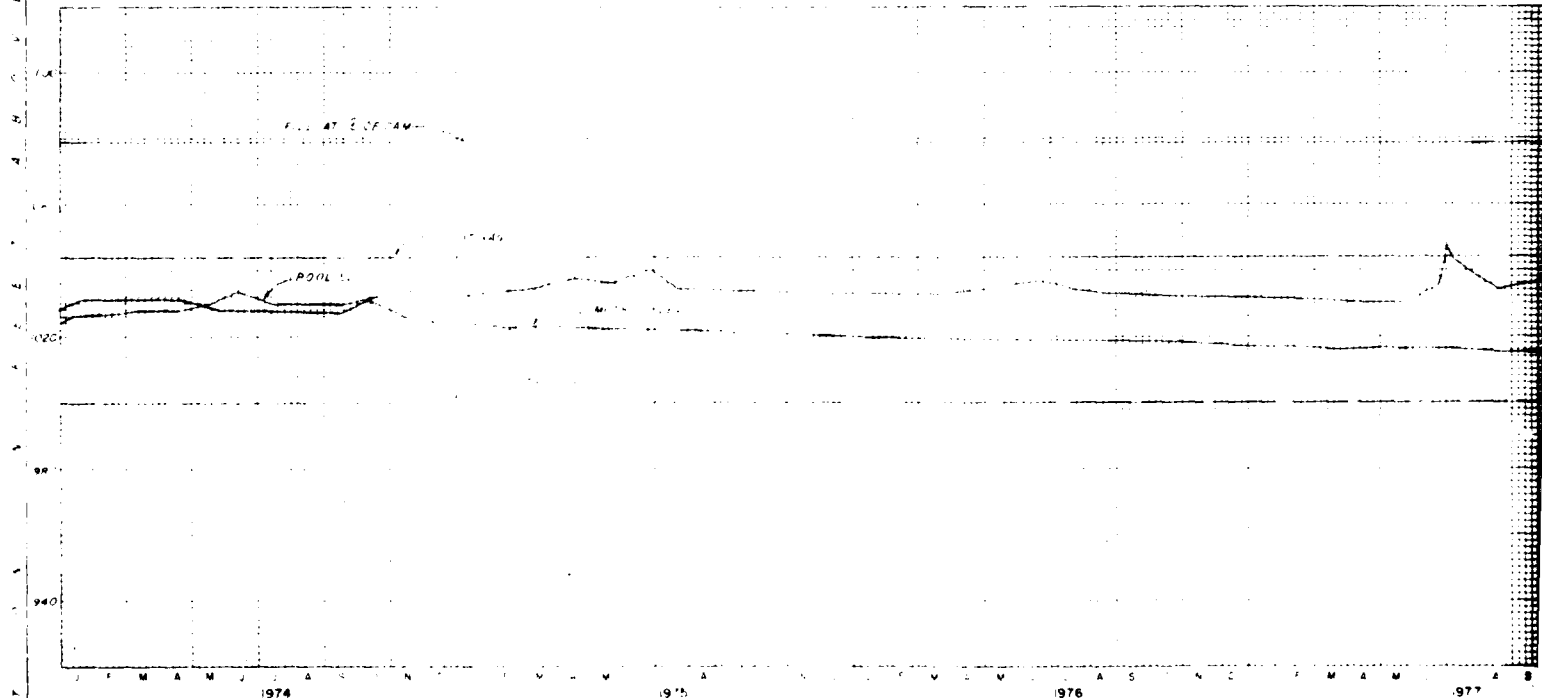
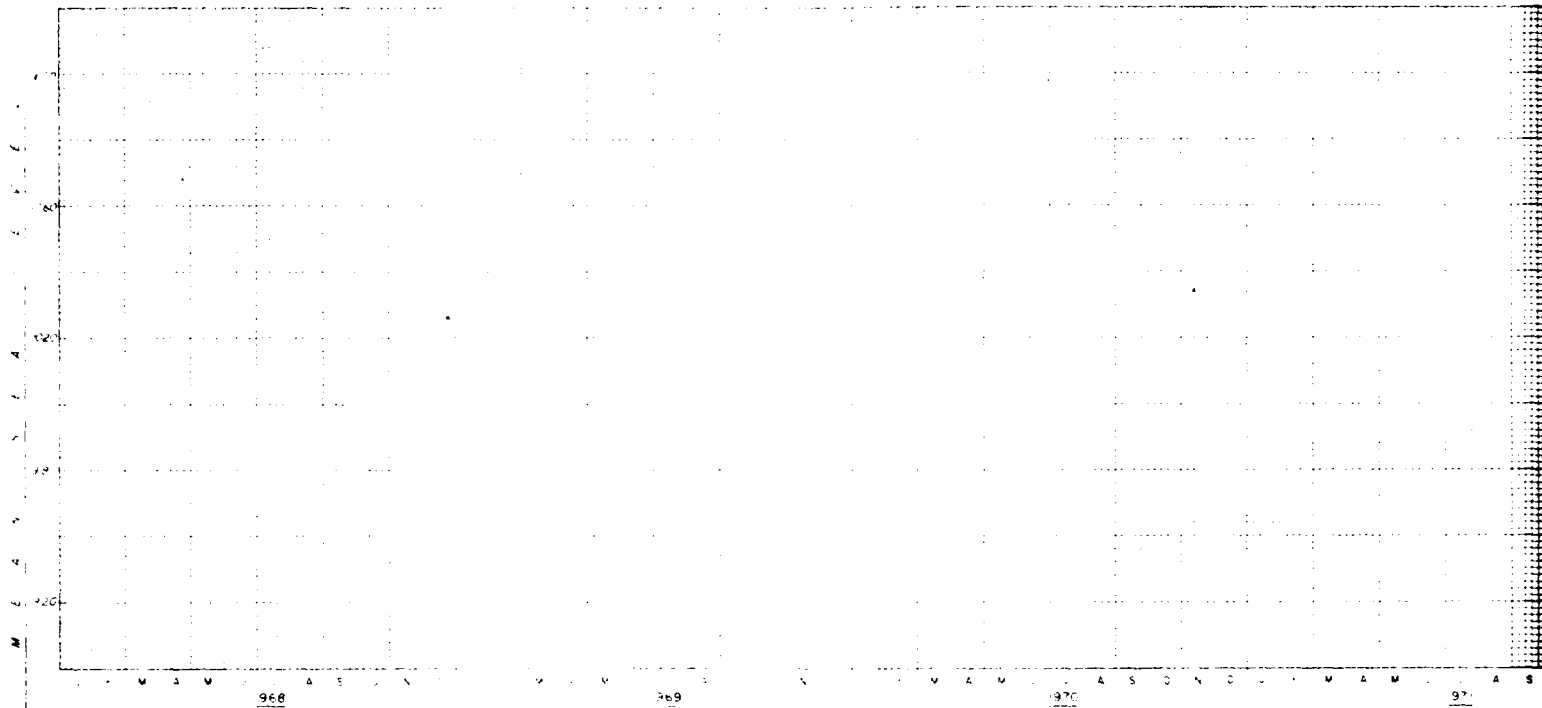
LEGEND
 OPEN TUBE O
 PNEUMATIC CELL •

MAHARISHI ENGINEERING CO.
 MAHARISHI ENGINEERING CO.
MELVERN LAKE

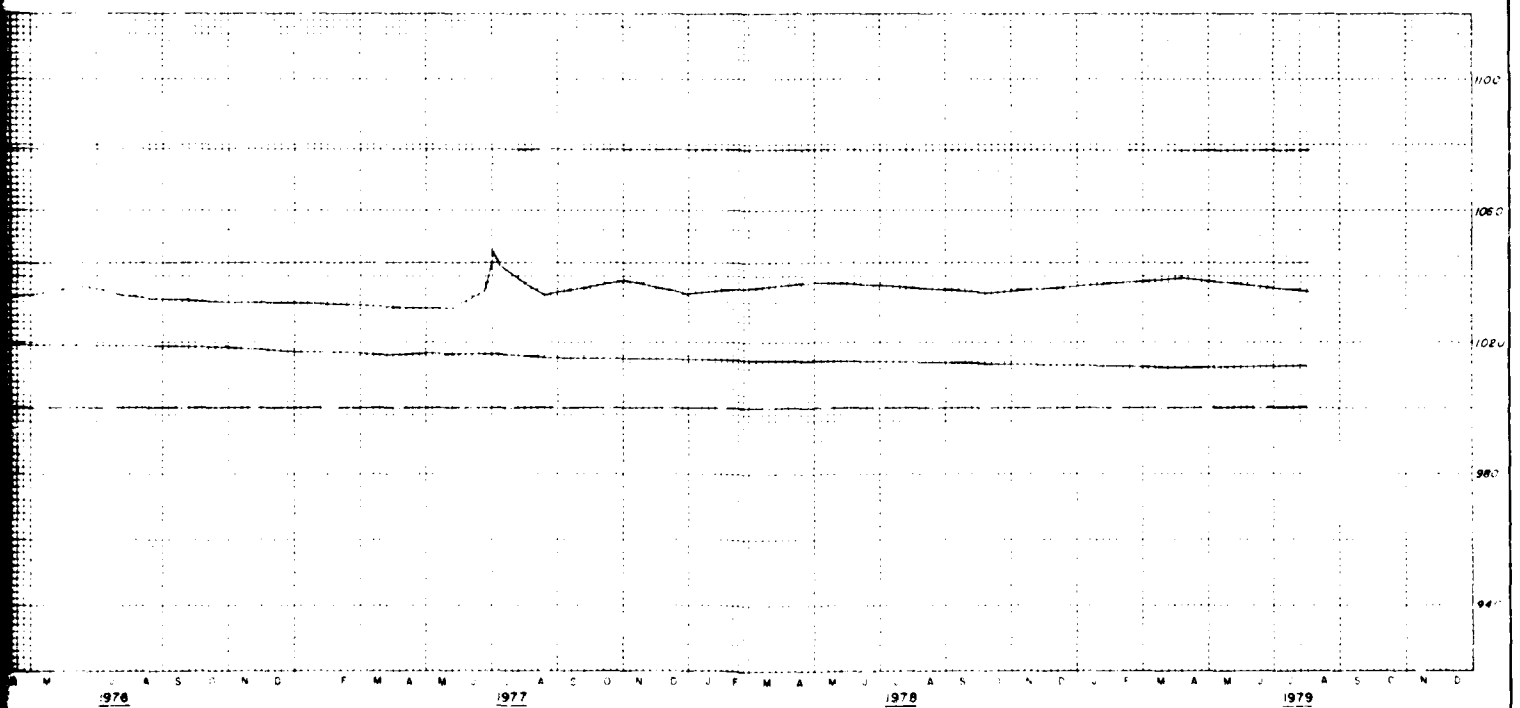
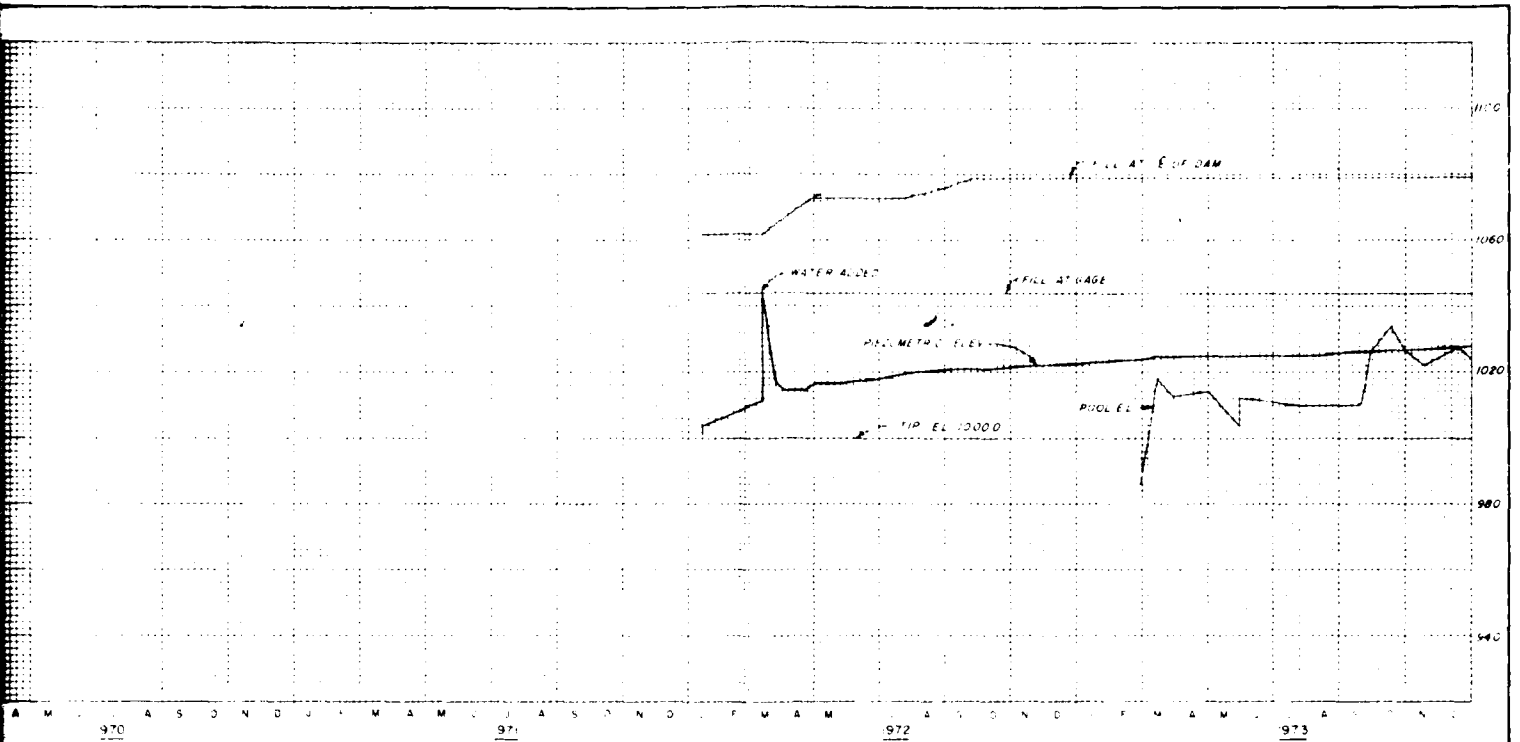
INSTRUMENTATION PLOTS
 PP-59-2 (OPEN TUBE)

Sheet No. 1
 MAHARISHI ENGINEERING CO.
 KAN. AR. 100-100000

FILE NO. 0-5-1292
 AUGUST 1975



STATION 59+00



DOWNSTREAM

LEGEND

OPEN TUBE ———○———
PNEUMATIC CELL ———●———

MAHAIS DES YGNES RIVER KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
PP.59-3 (OPEN TUBE)

Sheet No. 1

Scale: As Shown

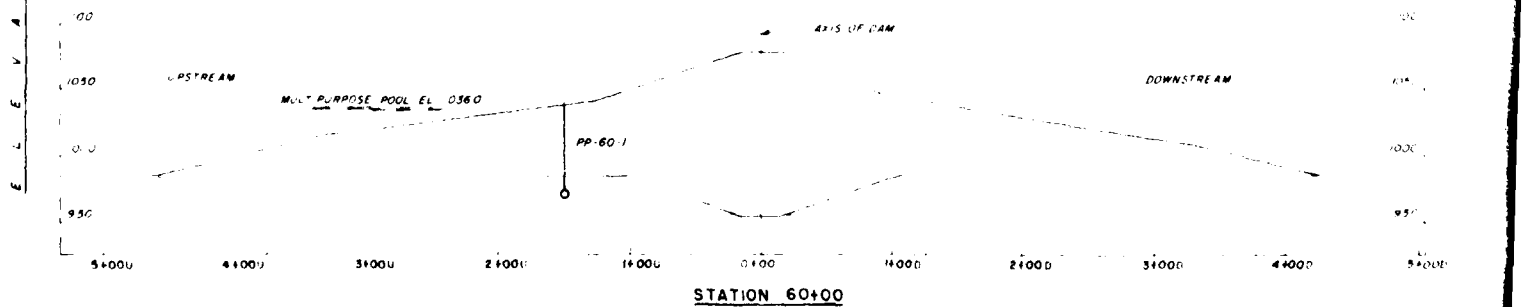
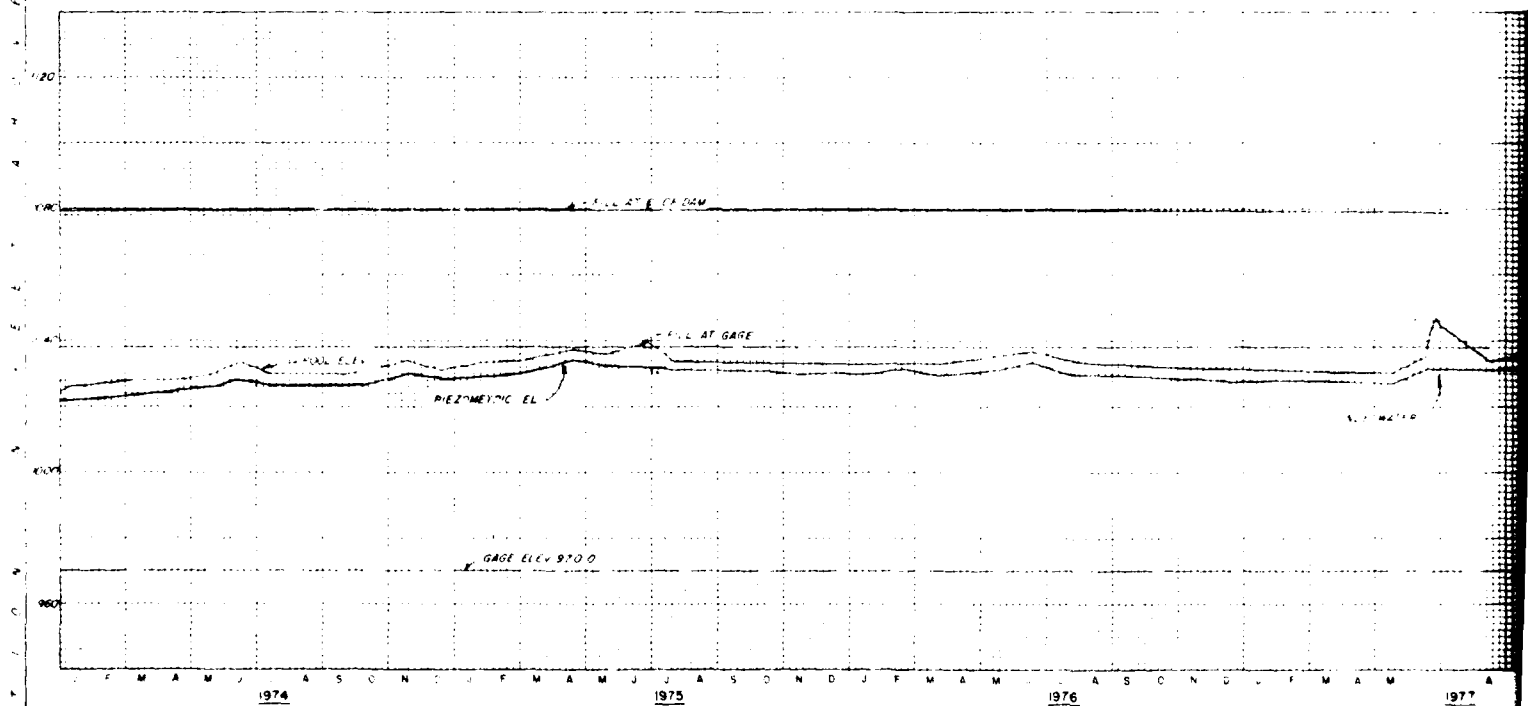
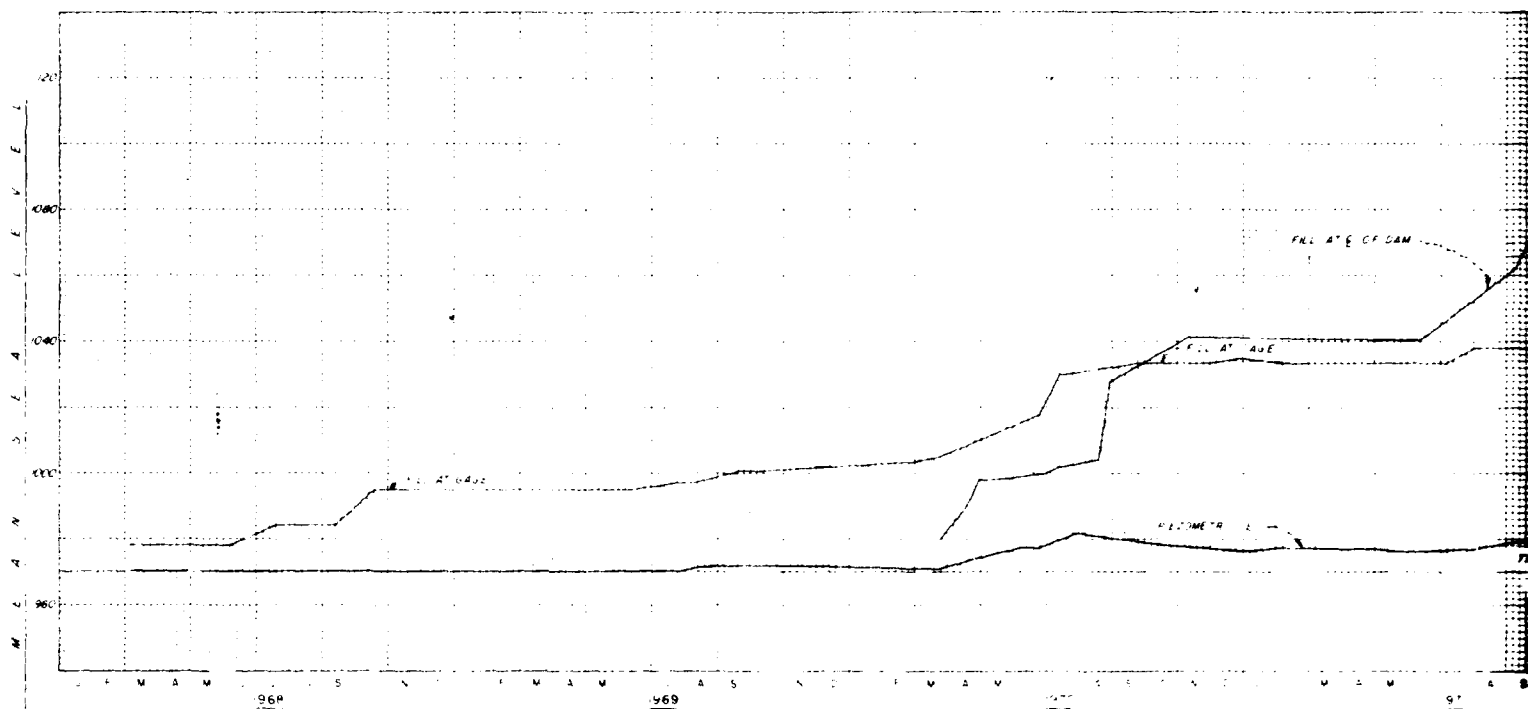
Scale: As Shown

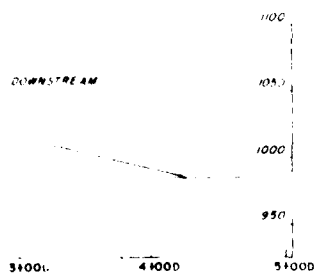
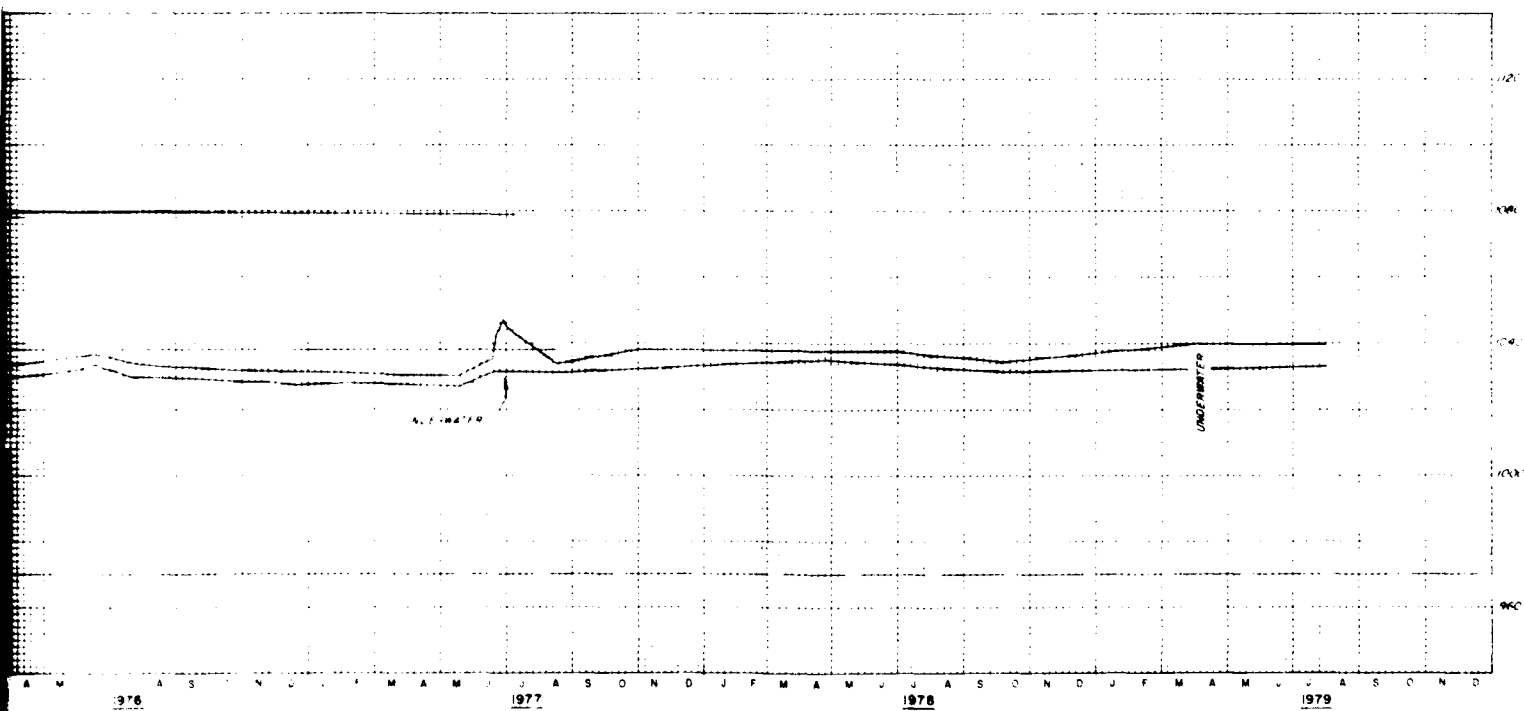
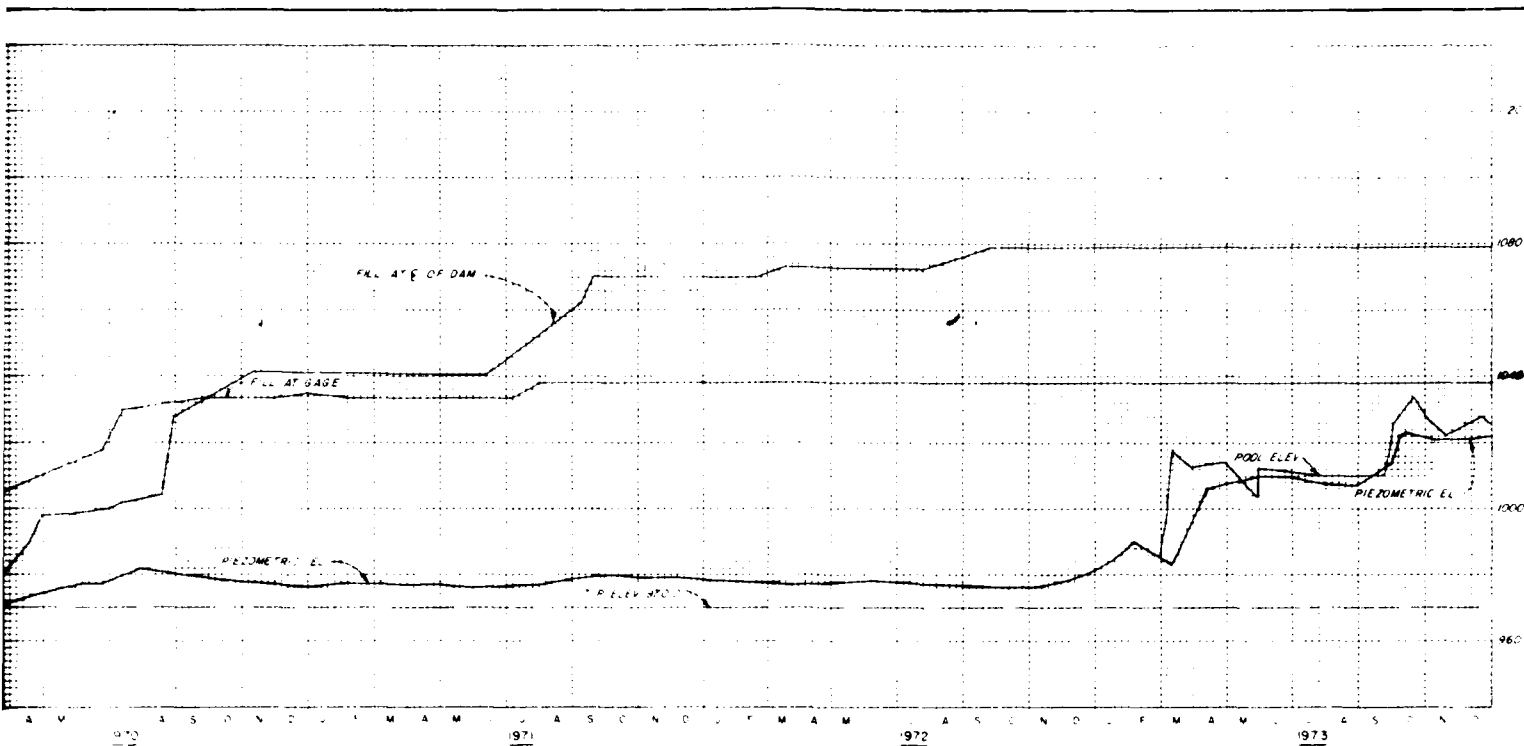
ENGINEERS S. ARMY

KANSAS DISTRICT

FILE NO 0-5-1293

AUGUST 1979





LEGEND
 OPEN TUBE — O
 PNEUMATIC CELL — ●

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 MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

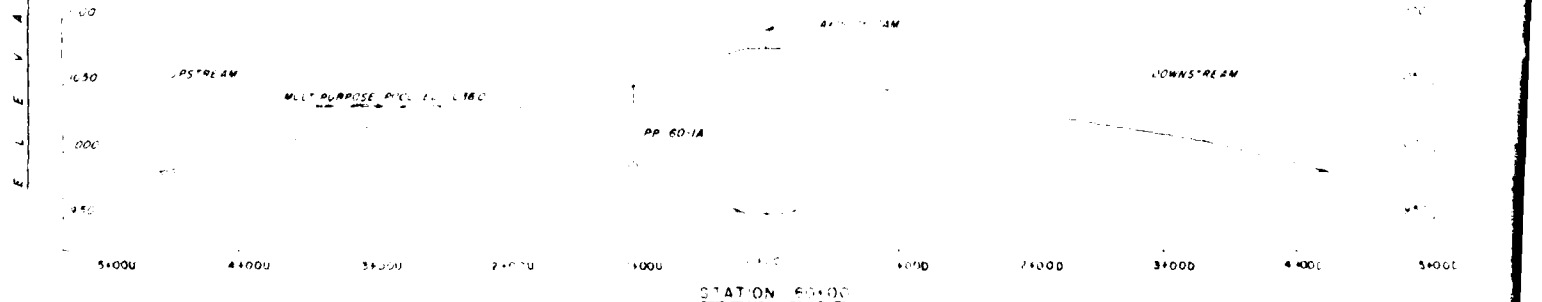
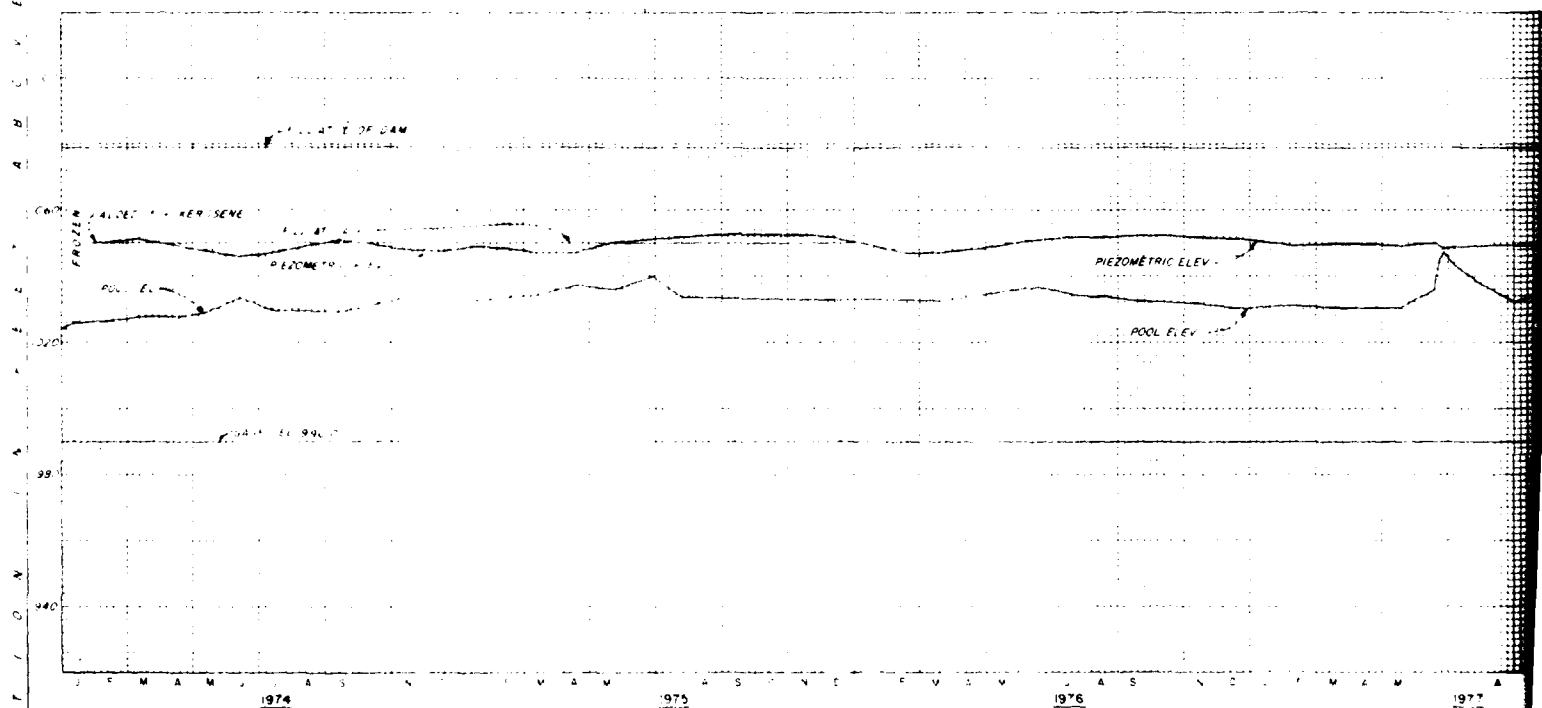
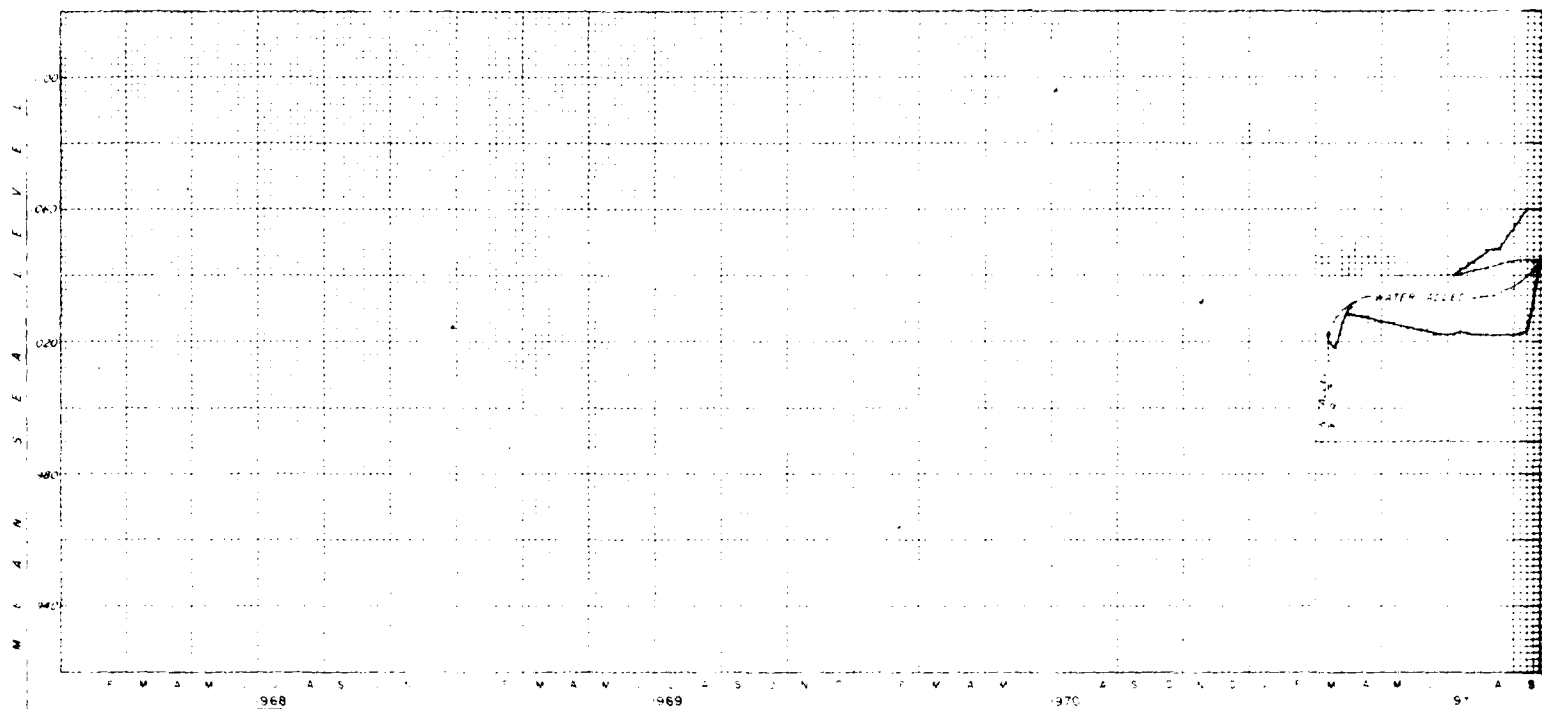
INSTRUMENTATION PLOTS
 PP-60-1 (OPEN TUBE)

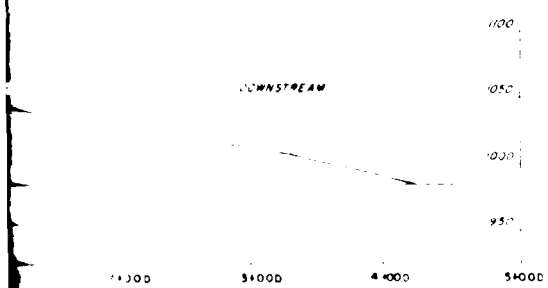
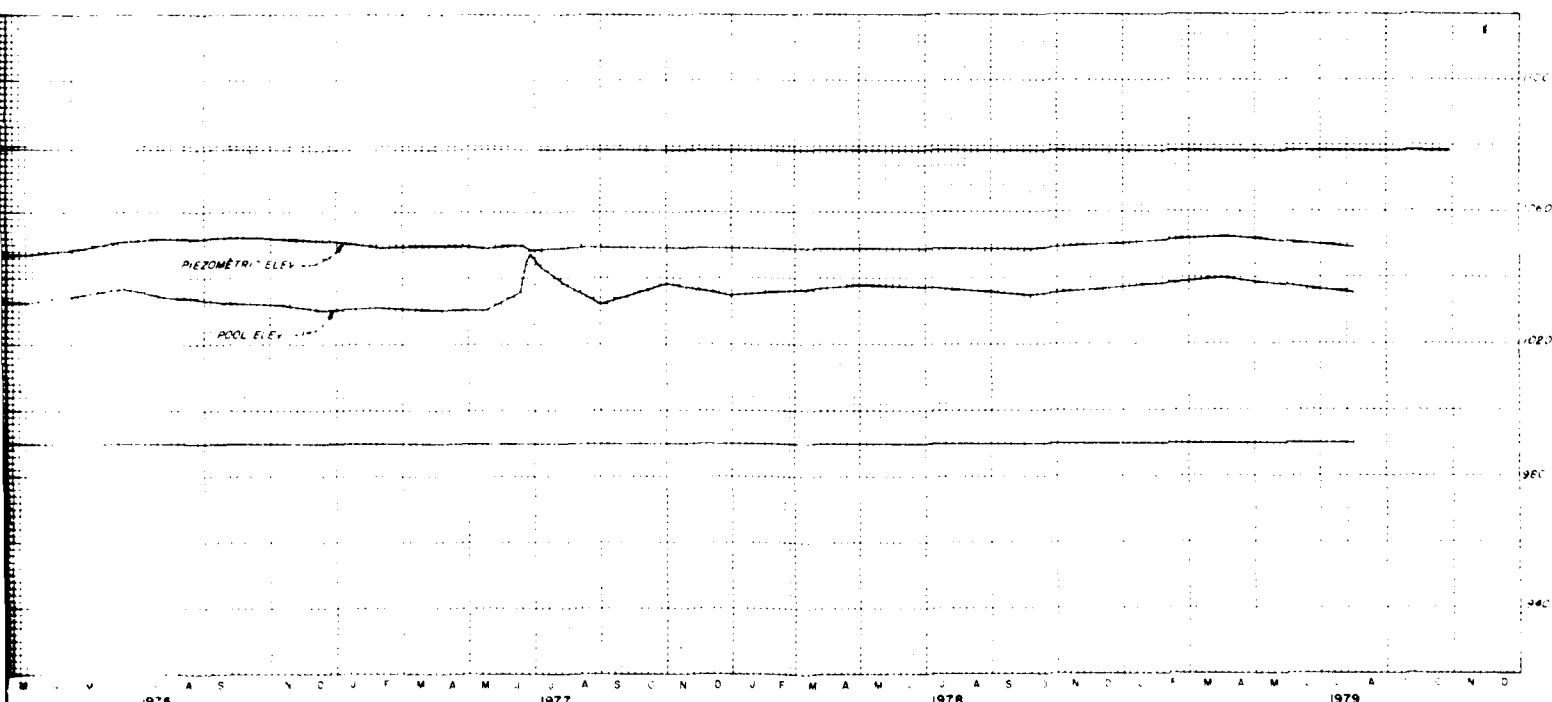
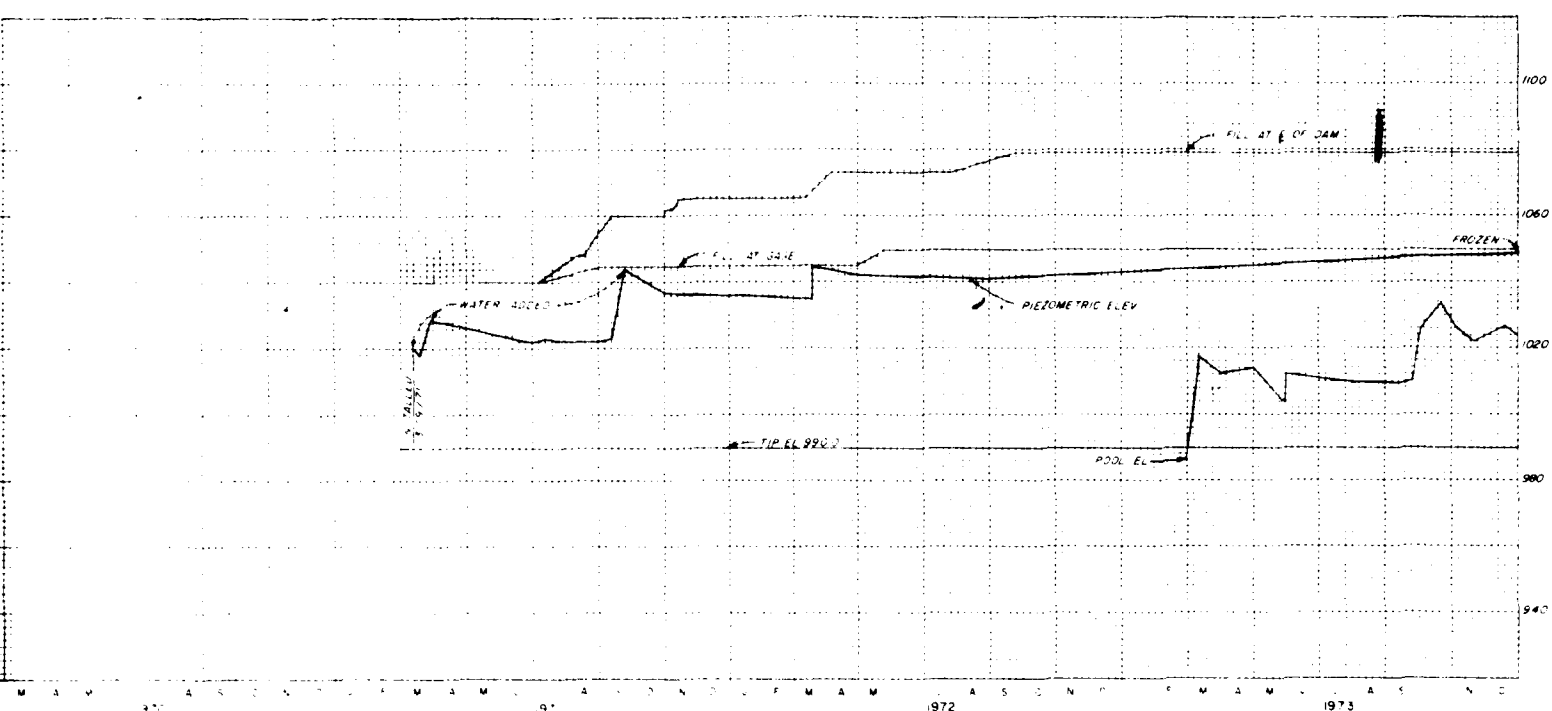
In 1 Sheet

Sheet No. 1

Scale as shown

CORPS OF ENGINEERS U.S. ARMY
 KANSAS DISTRICT
 FILE NO 0-5-1294
 AUGUST 1975





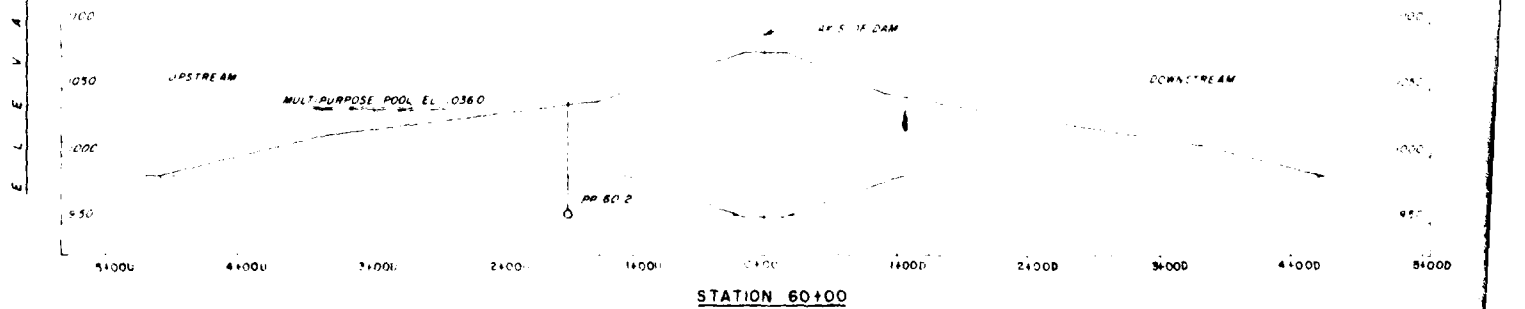
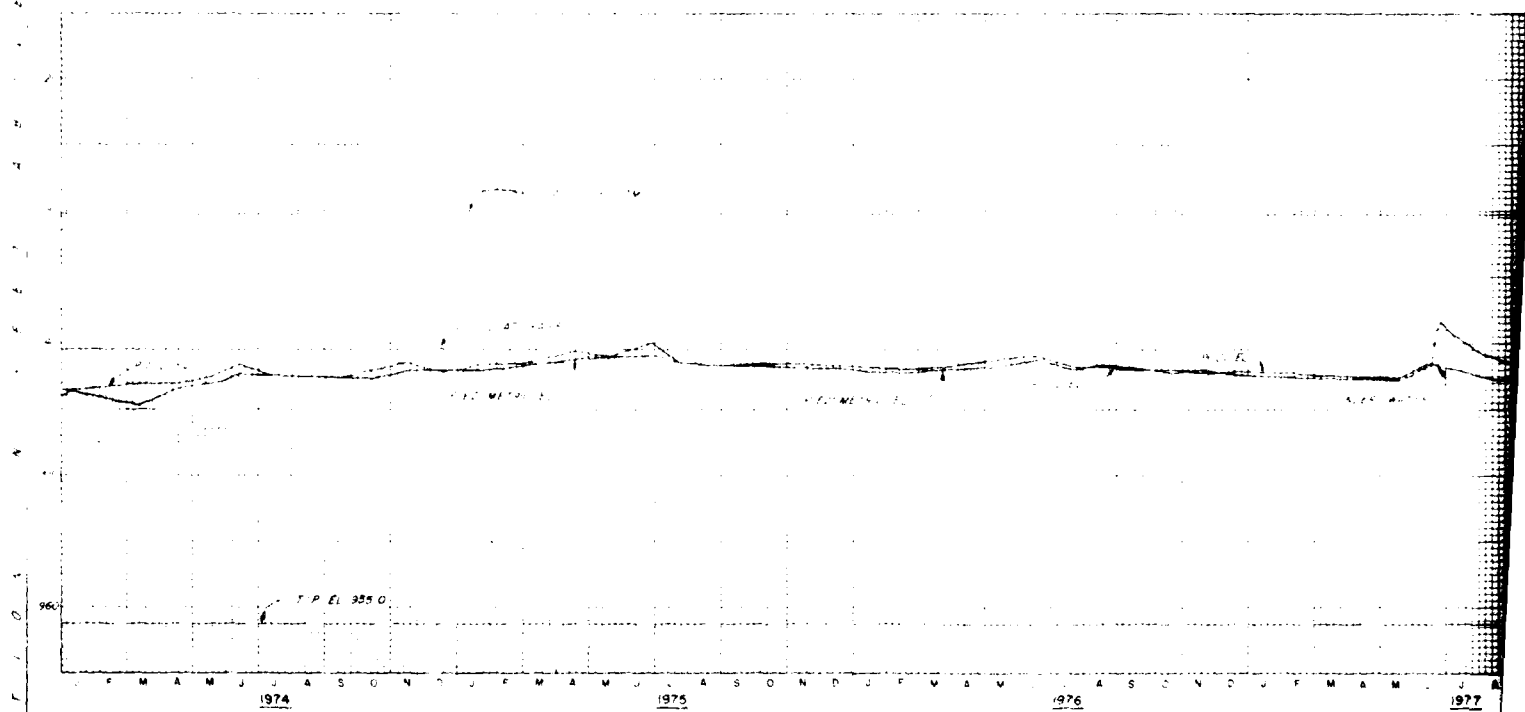
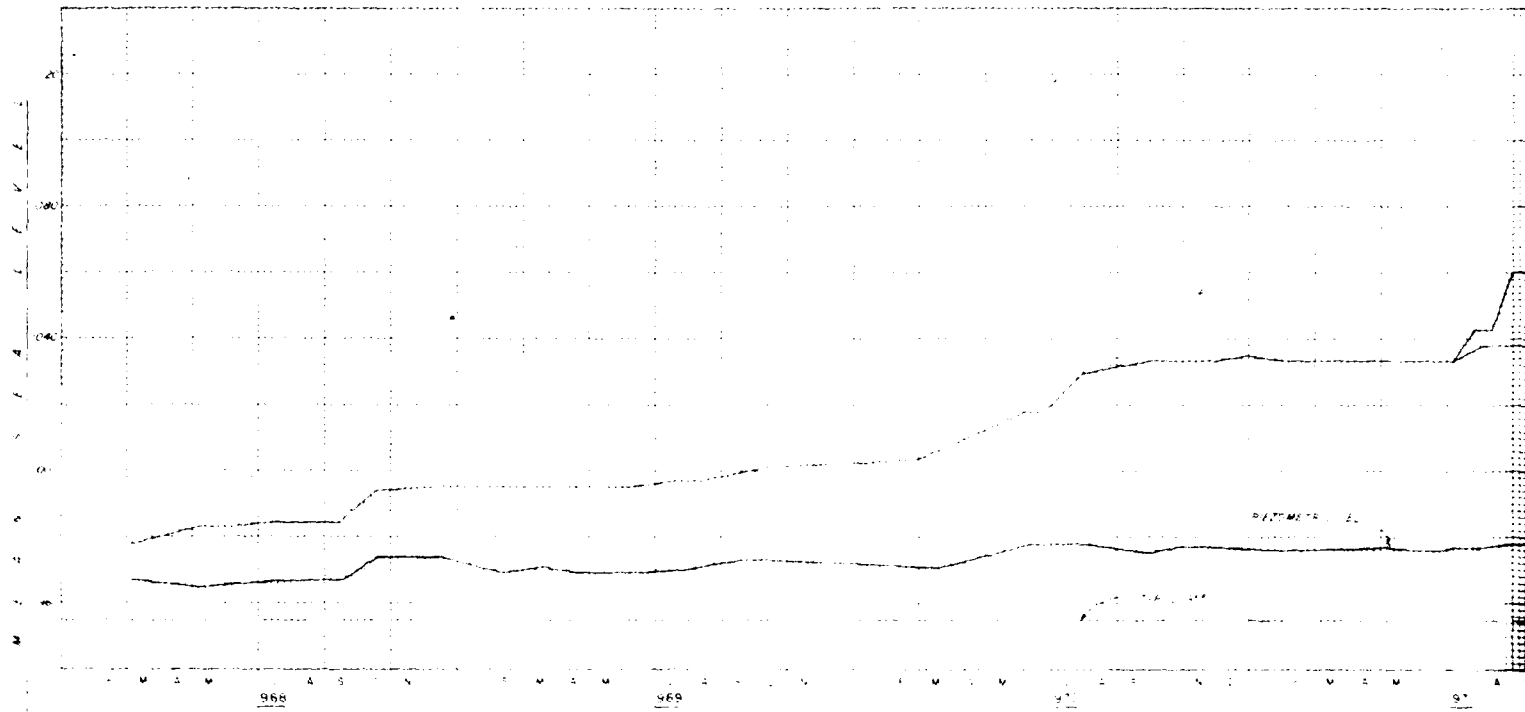
LEGEND
 OPEN TUBE ○
 PNEUMATIC CELL ●

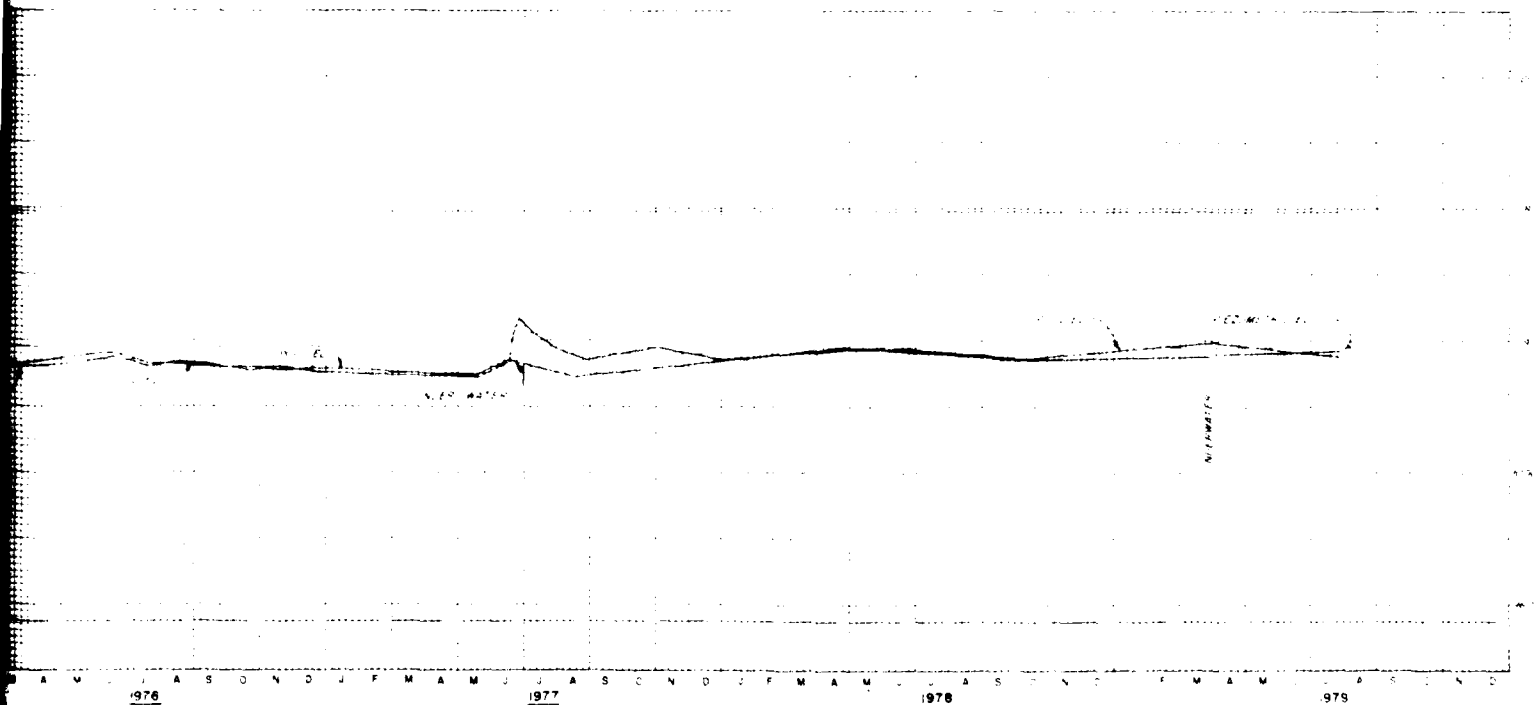
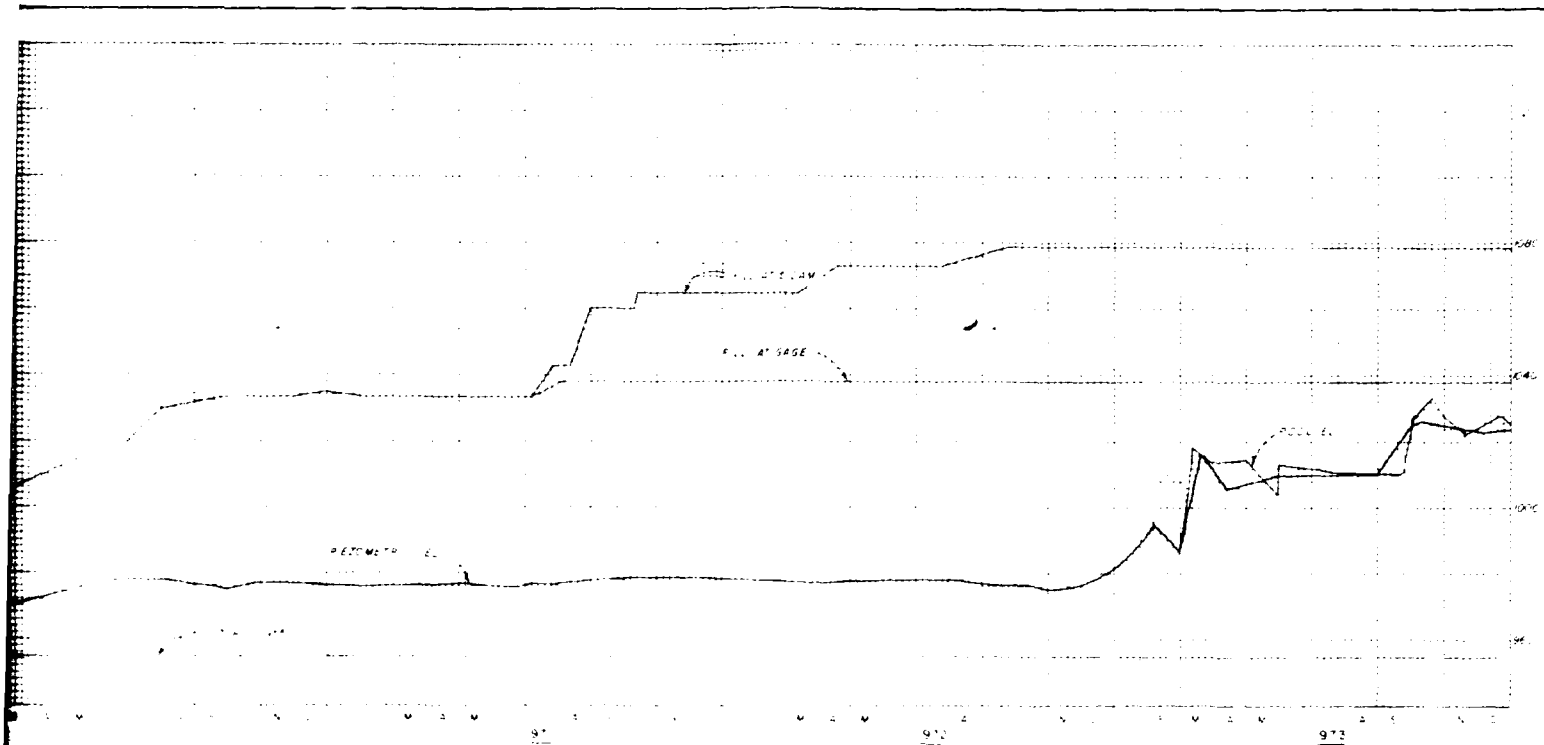
MARSH DES LYGNES RIVER KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
 PP-60-1A (OPEN TUBE)

Sheet No. 1
 KANSAS ENGINEERING
 FILE NO. 0-5-1295
 AUGUST 1974

2





DOWNSTREAM

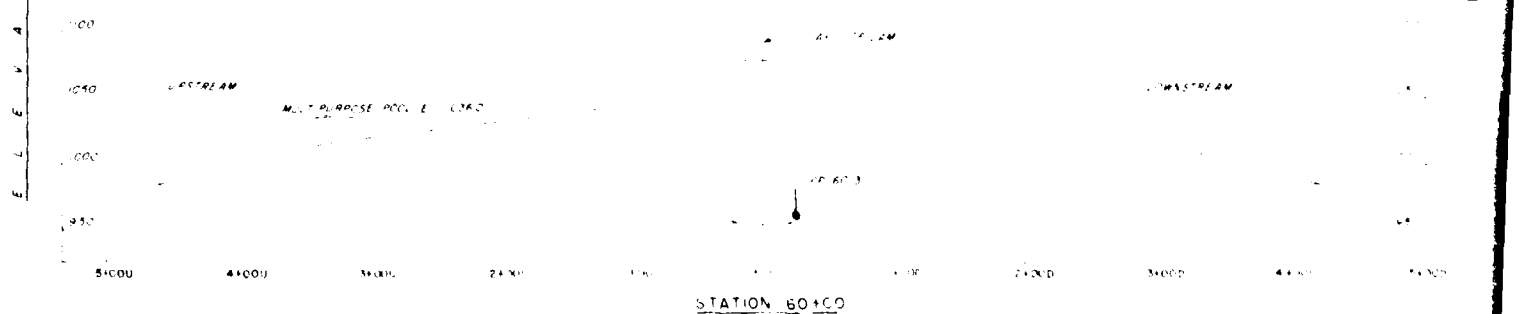
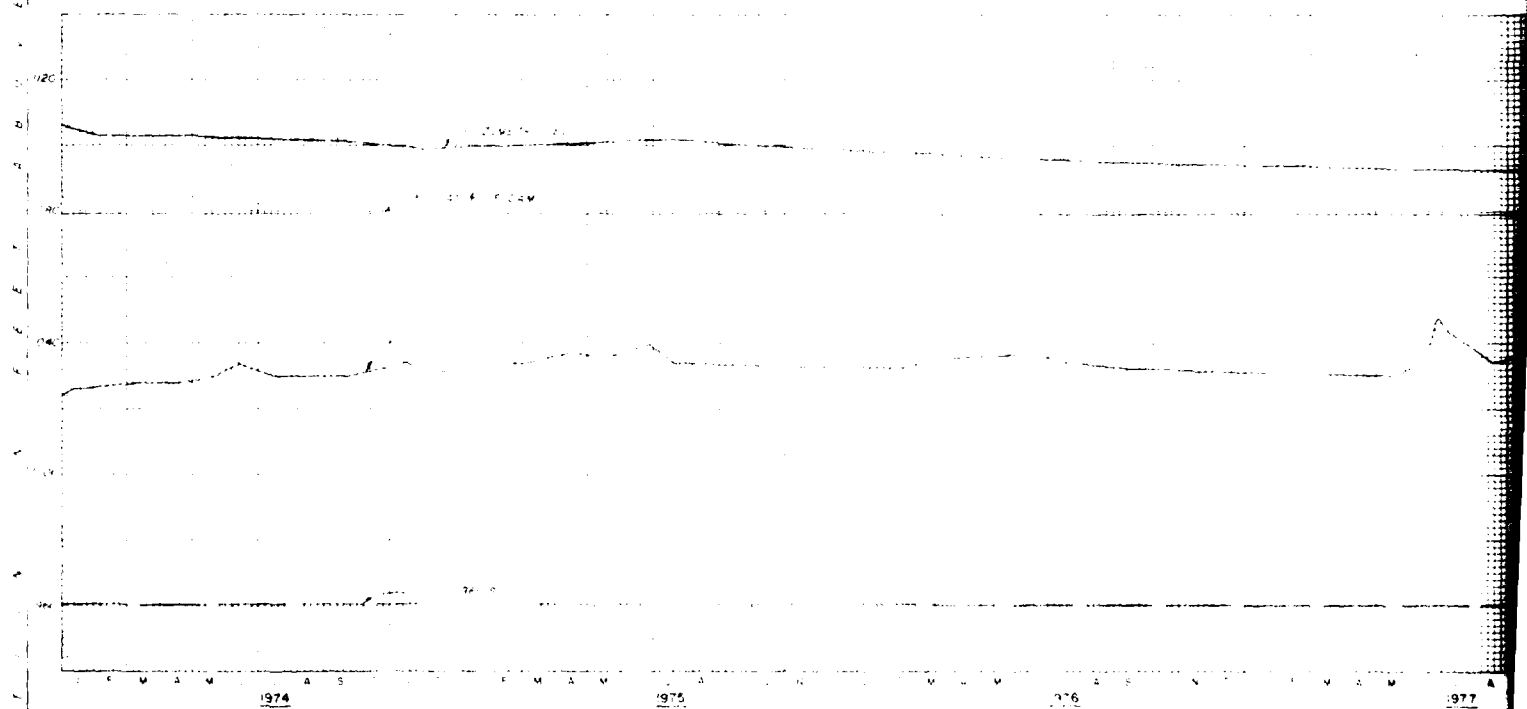
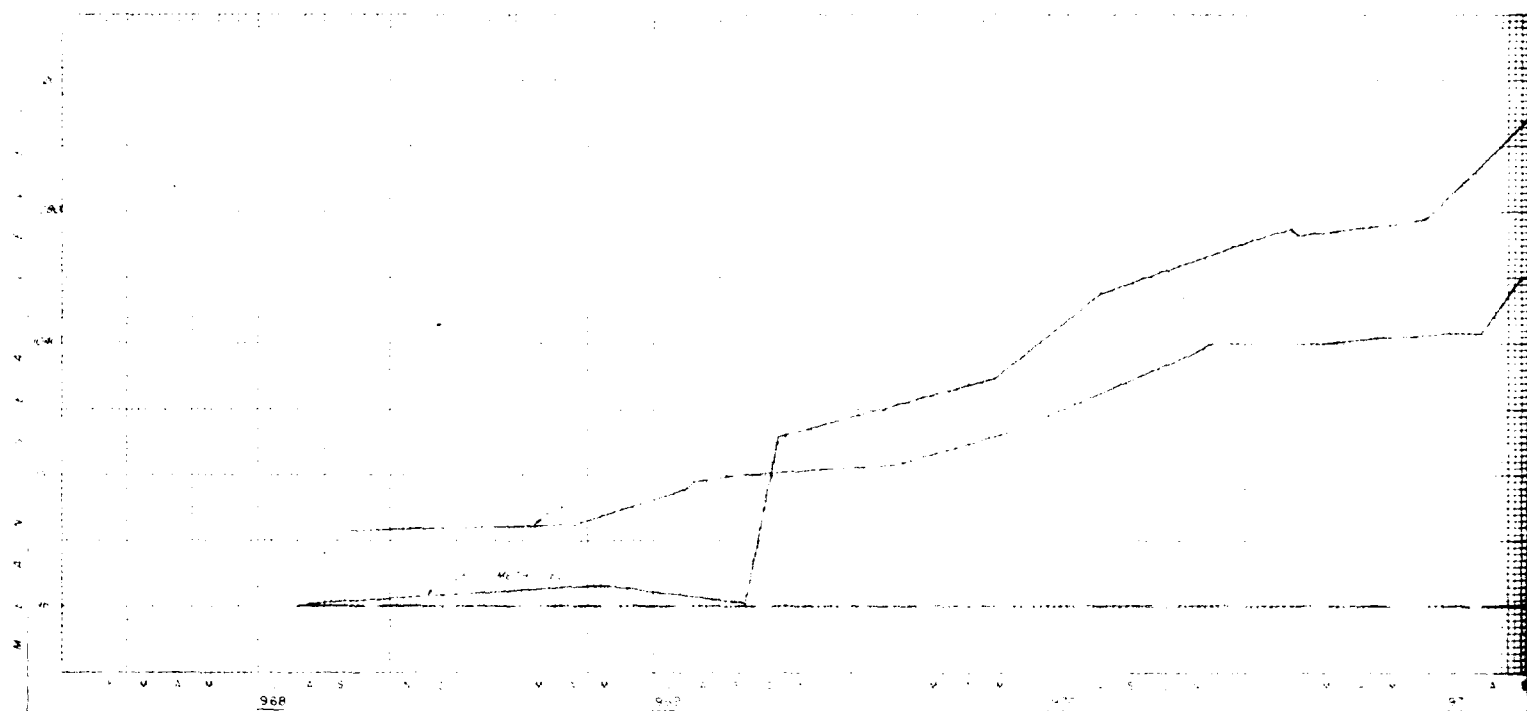
LEGEND

OPEN TUBE ○
PNEUMATIC CELL ●

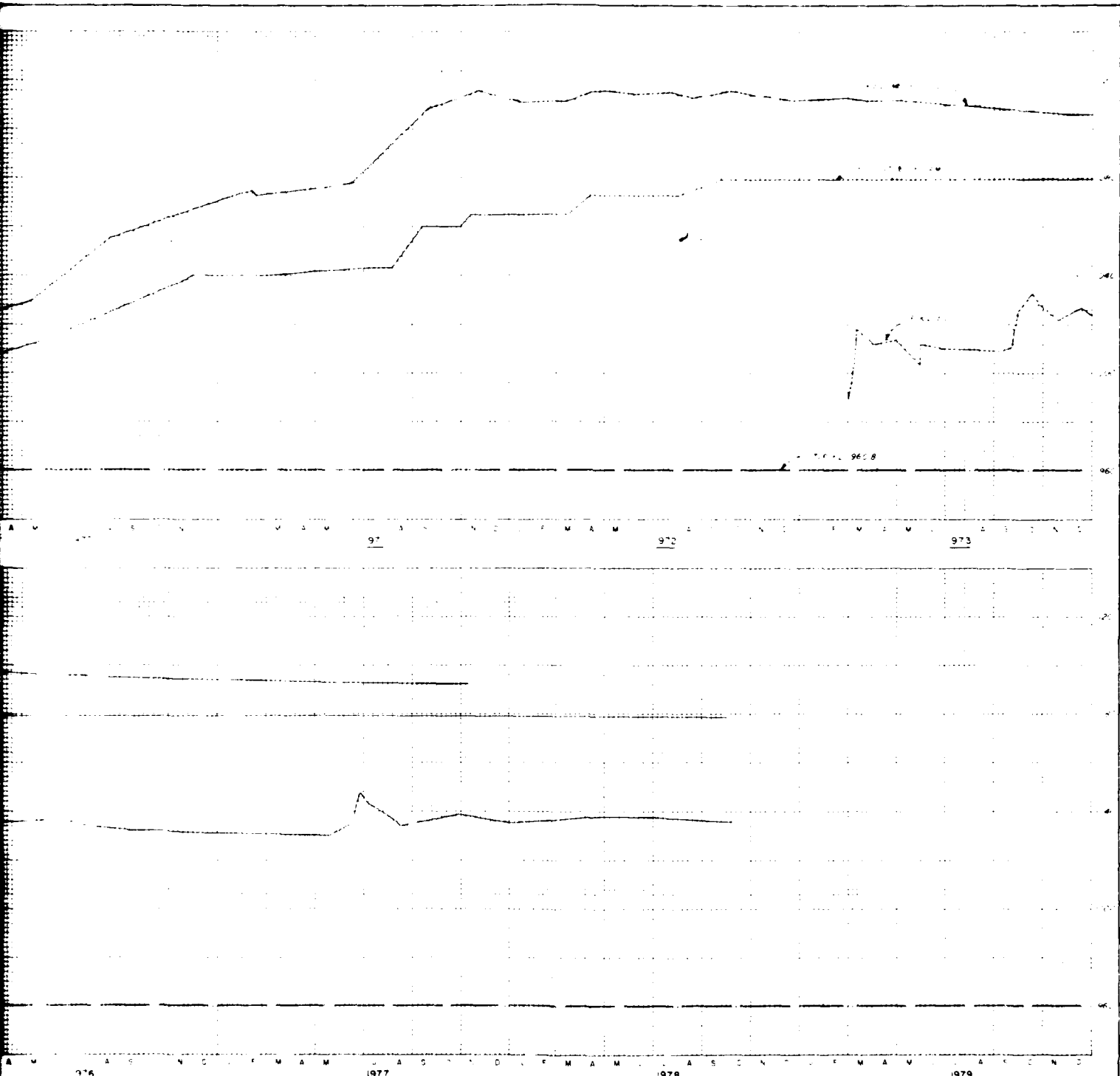
MELVERN LAKE

INSTRUMENTATION PLOTS
PP-60-2 (OPEN TUBE)

FILE NO 0-5-1296
AUGUST 1975



STATION 60+00



UPSTREAM

LEGEND

OPEN TUBE
PNEUMATIC CELL

MELVERN LAKE

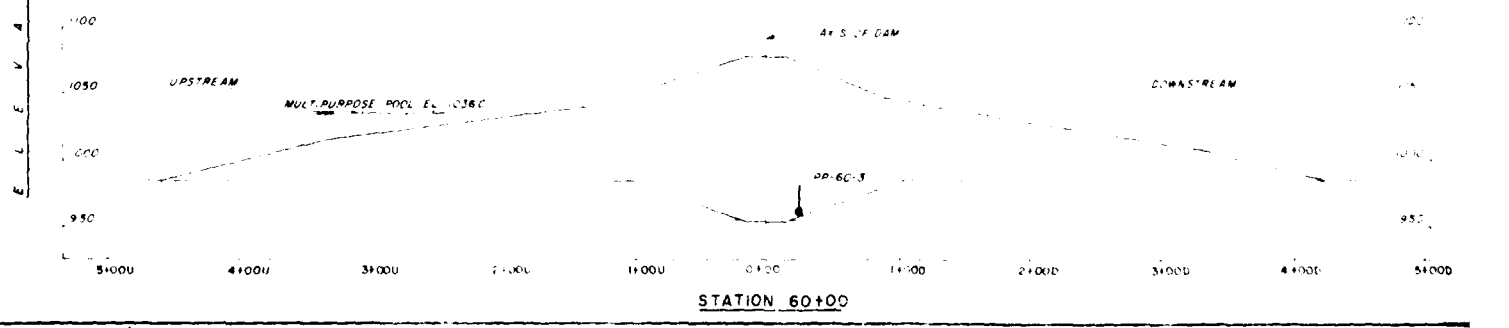
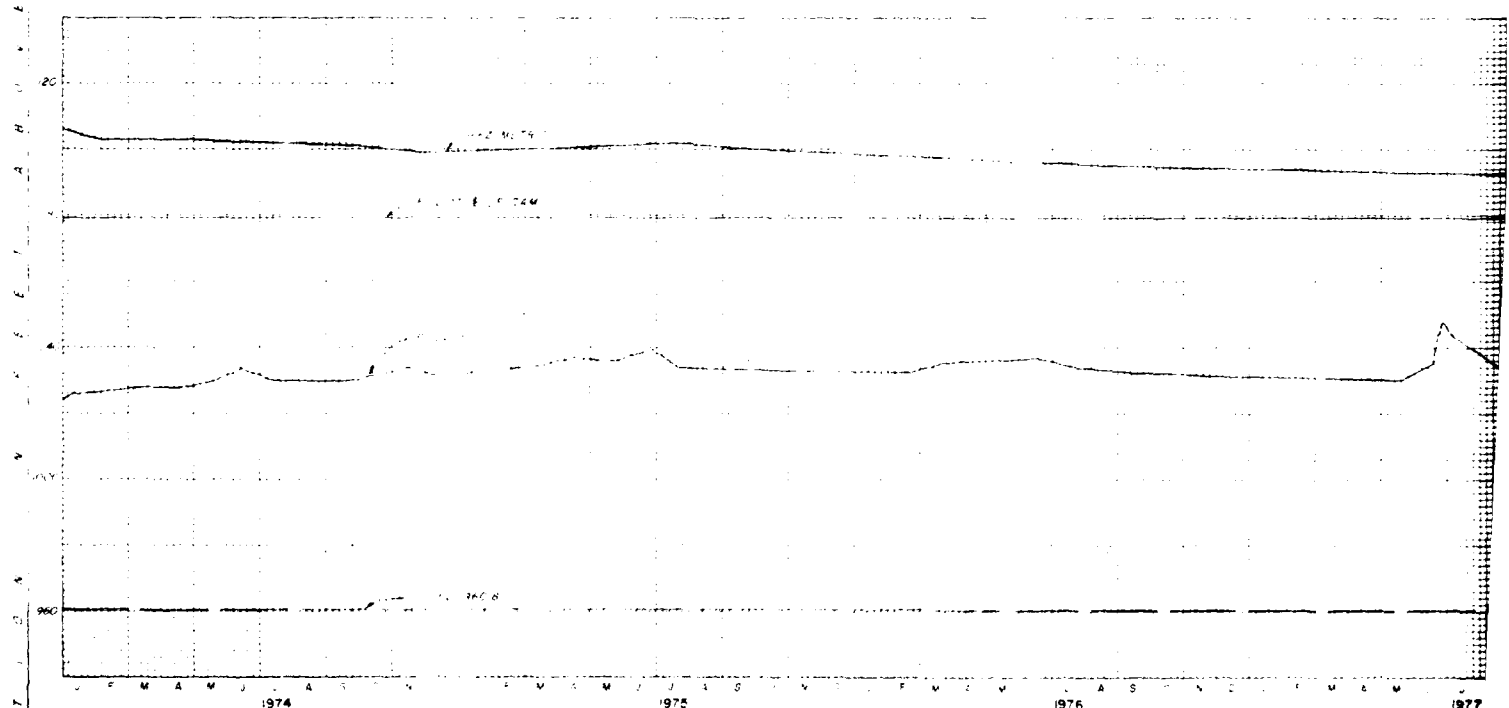
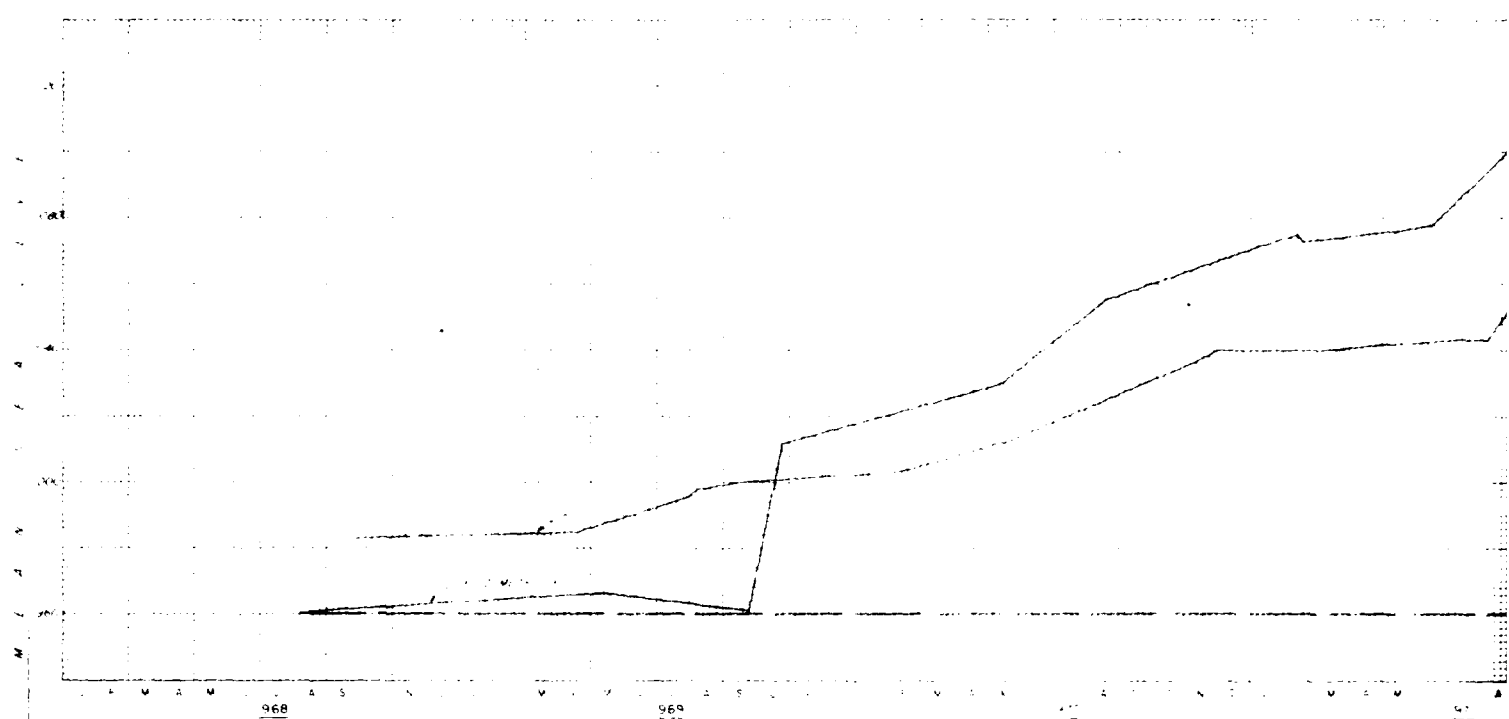
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PP-60-3 (SHANNON-WILSON CELL)

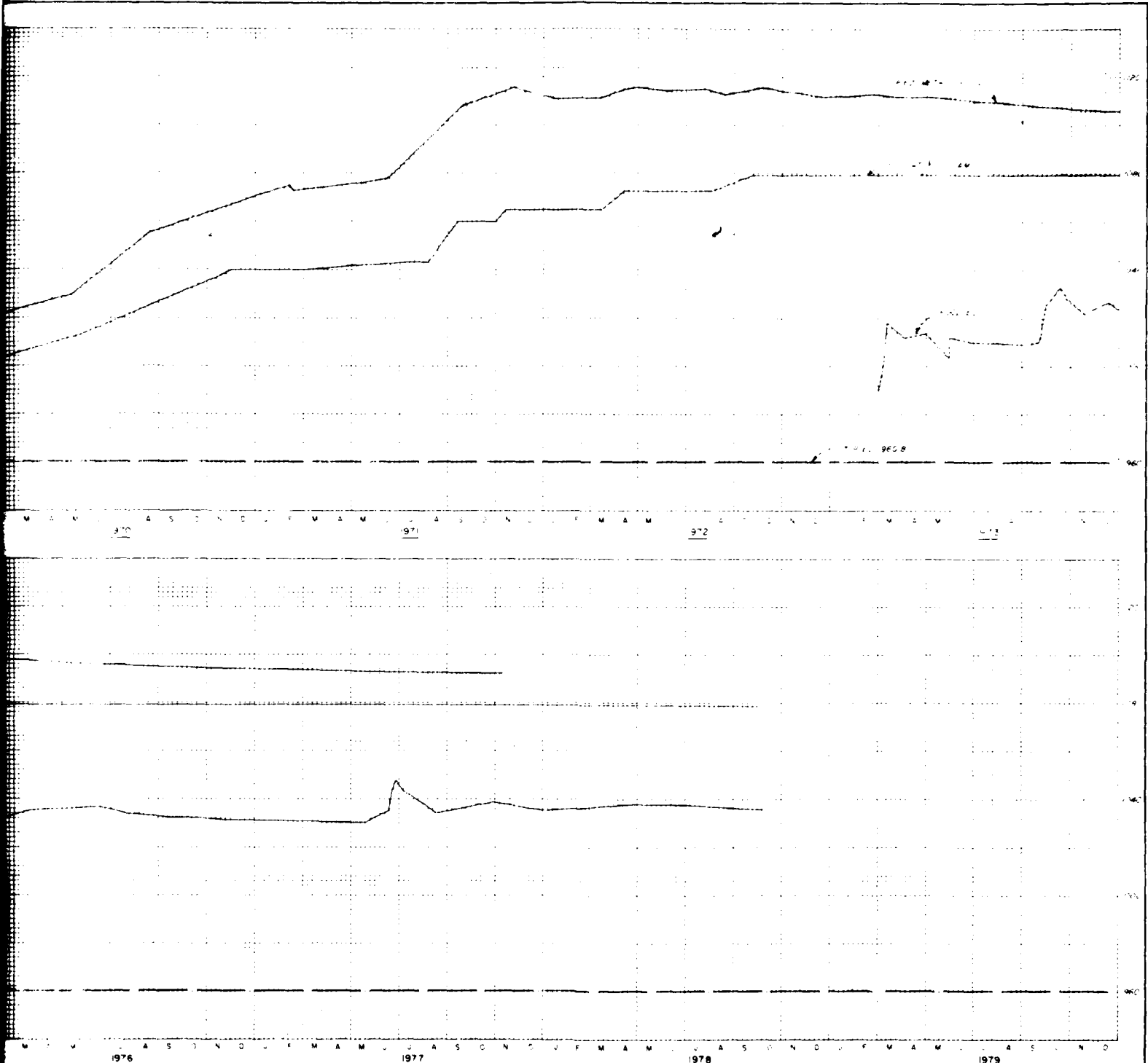
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Sheet No.

DATE PLOTTED

FILE NO 0-5-1297
AUGUST 1979





DOWNSTREAM

1100
1050
1000
950
900

LEGEND

OPEN TUBE
PNEUMATIC CELL

MANKINS DES. YGNES RIVER, KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
PP-60-3 (SHANNON-WILSON CELL)

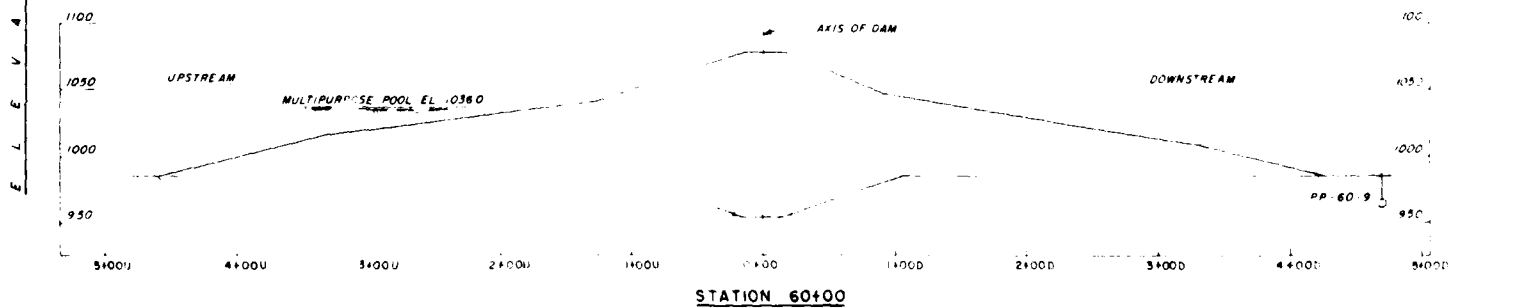
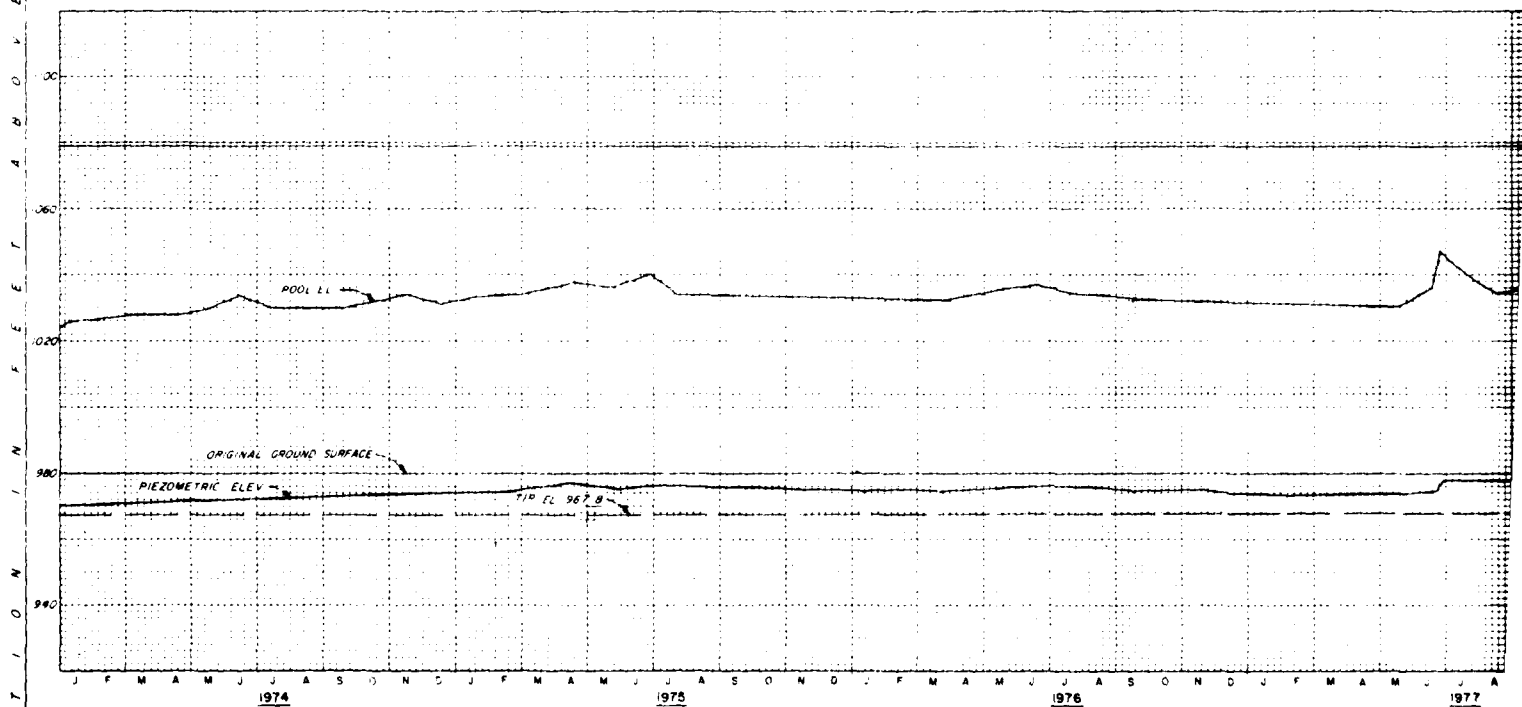
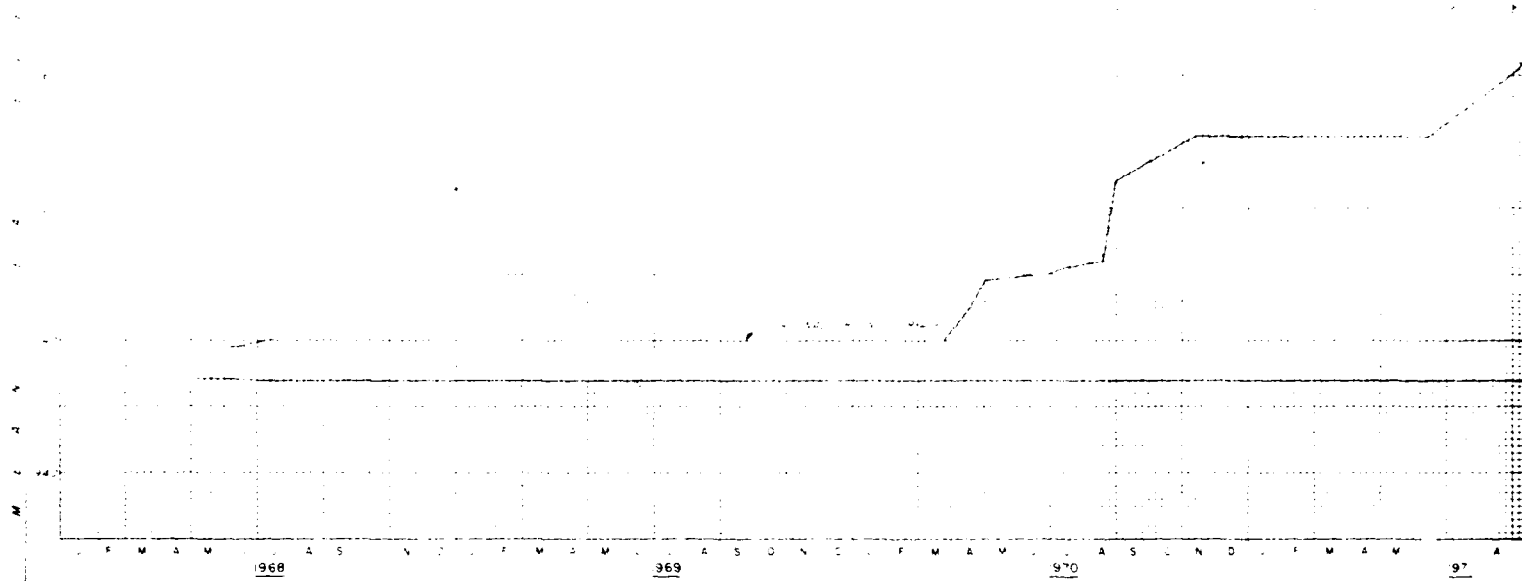
Sheet No. 1

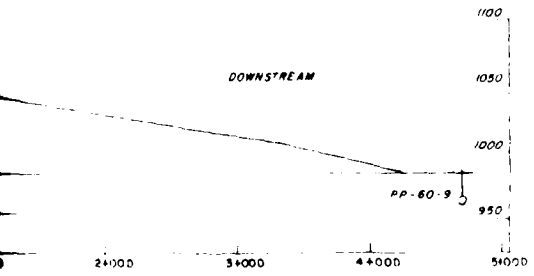
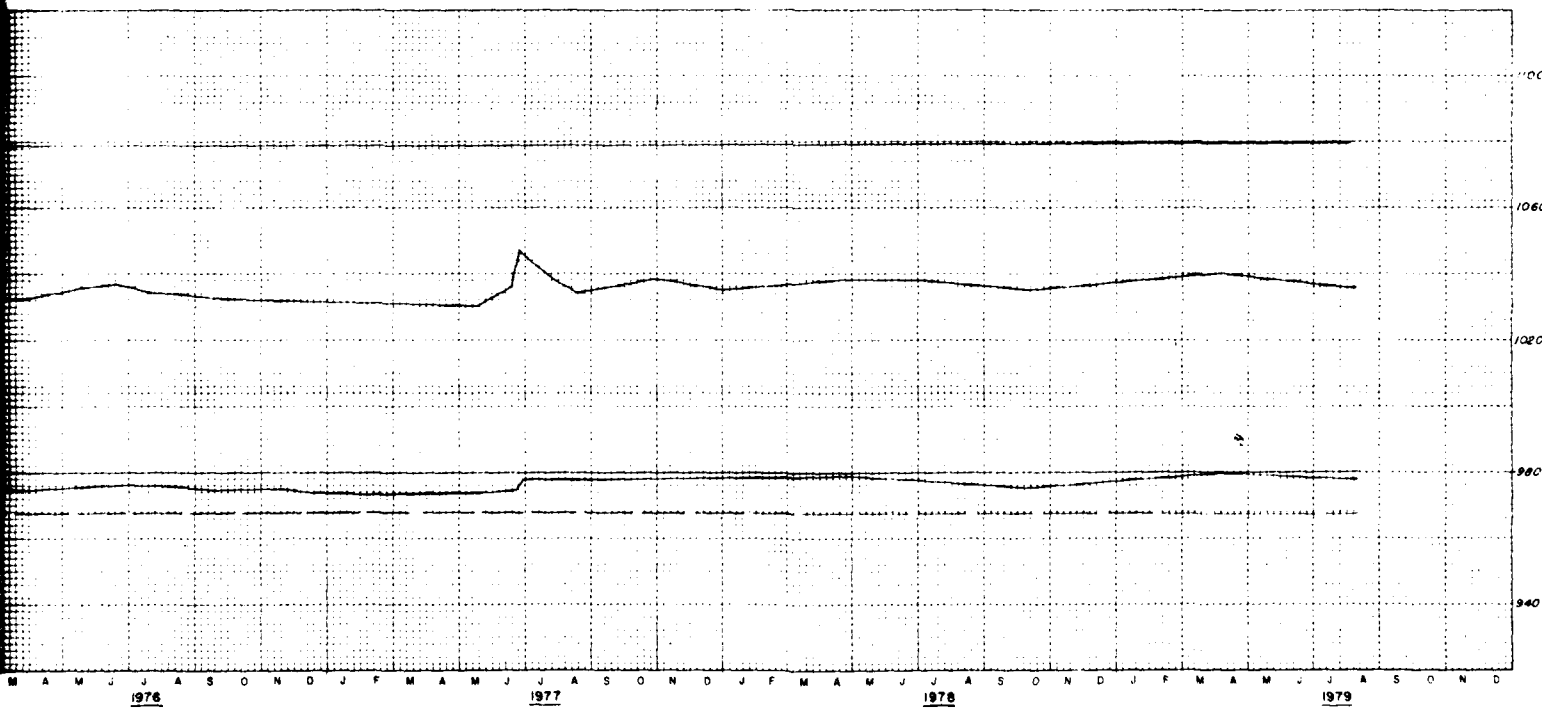
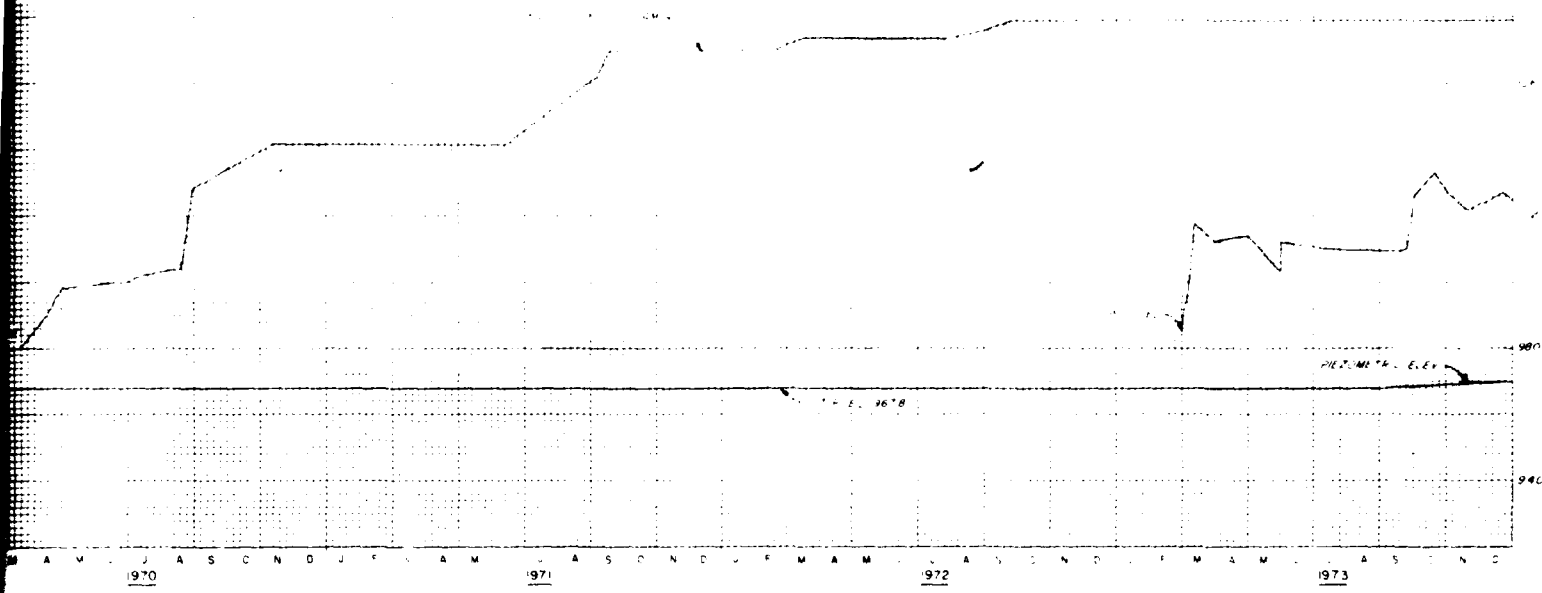
Sheet No. 1

Sheet No. 1

U.S. ARMY
KANSAS DISTRICT

FILE NO. 0-5-1297
AUGUST 1975





LEGEND
 OPEN TUBE — ○
 PNEUMATIC CELL — ●

Revised August 1979
 MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
 PP-60-9 (OPEN TUBE)

In 1 sheet

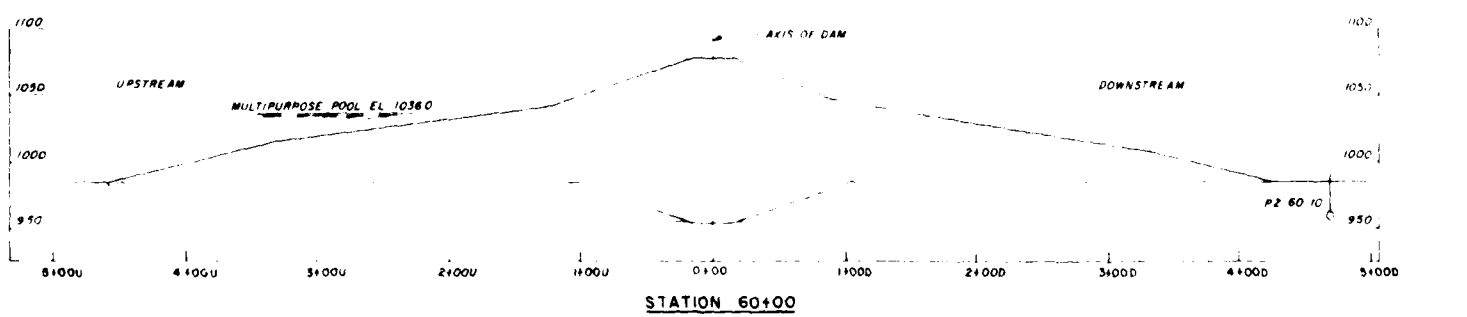
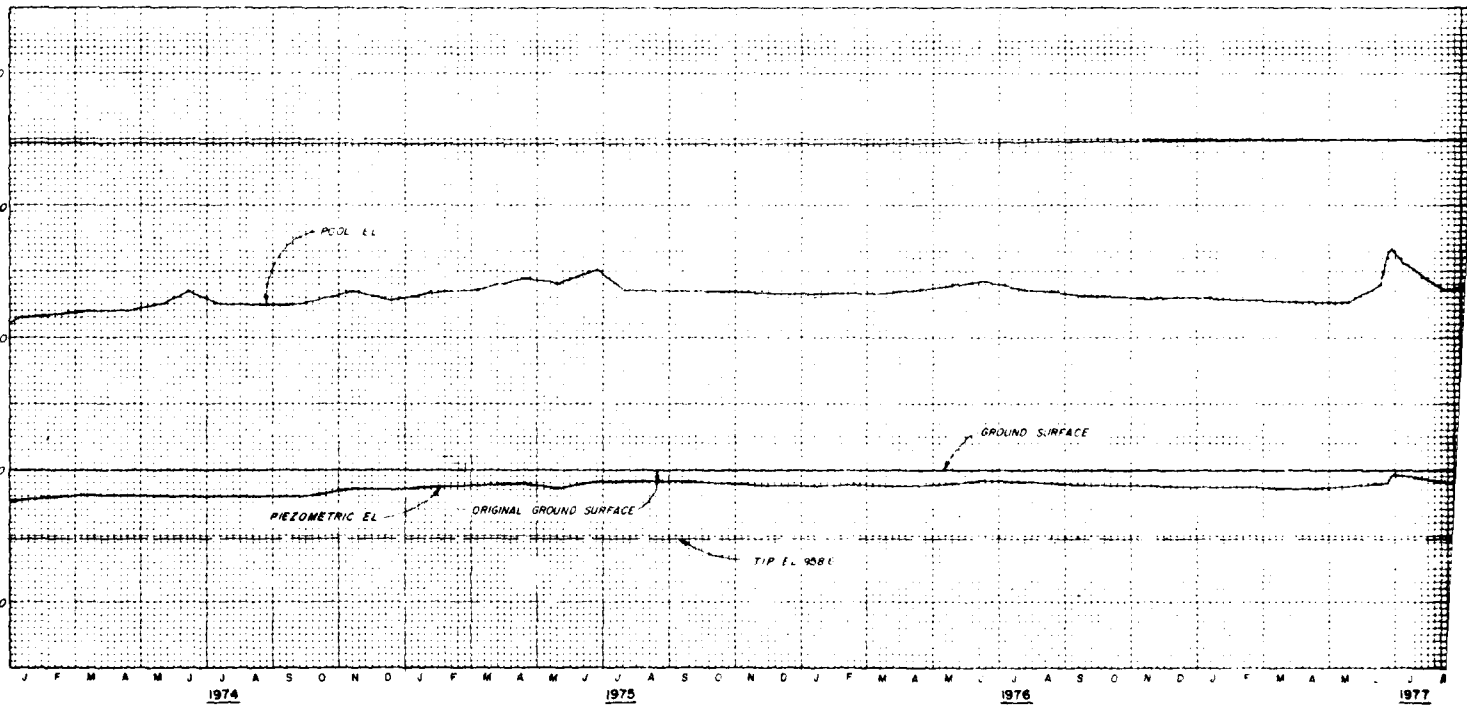
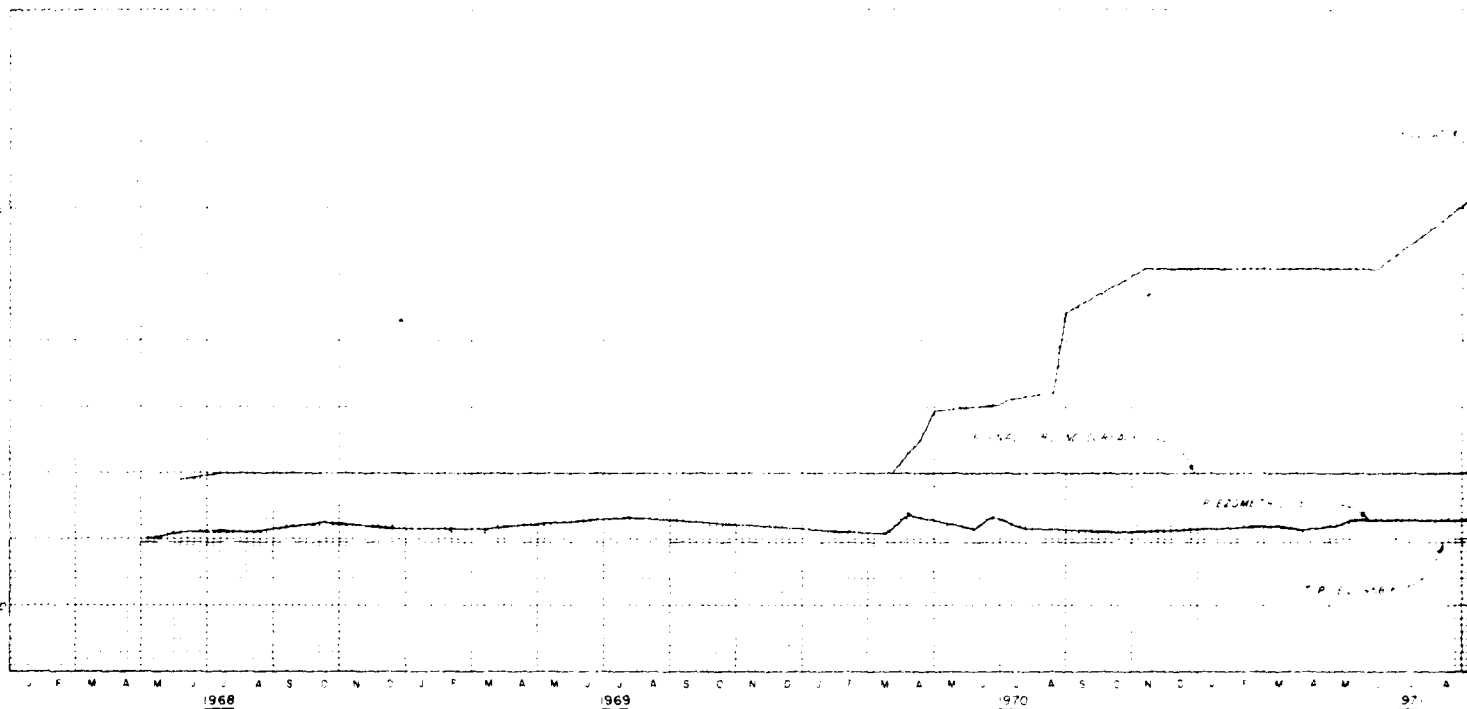
Sheet No. 1

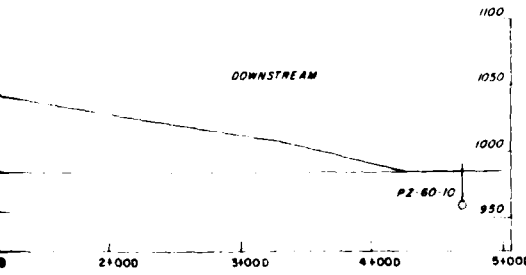
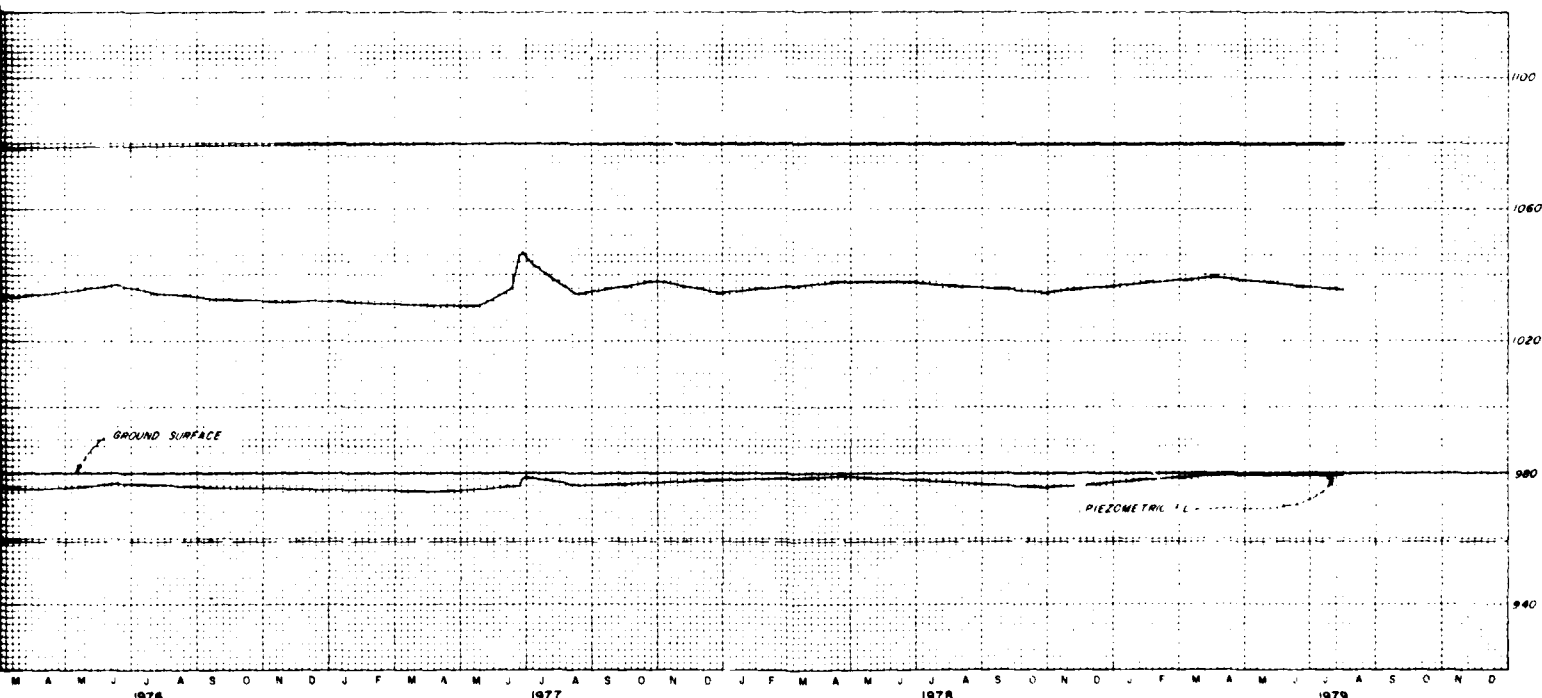
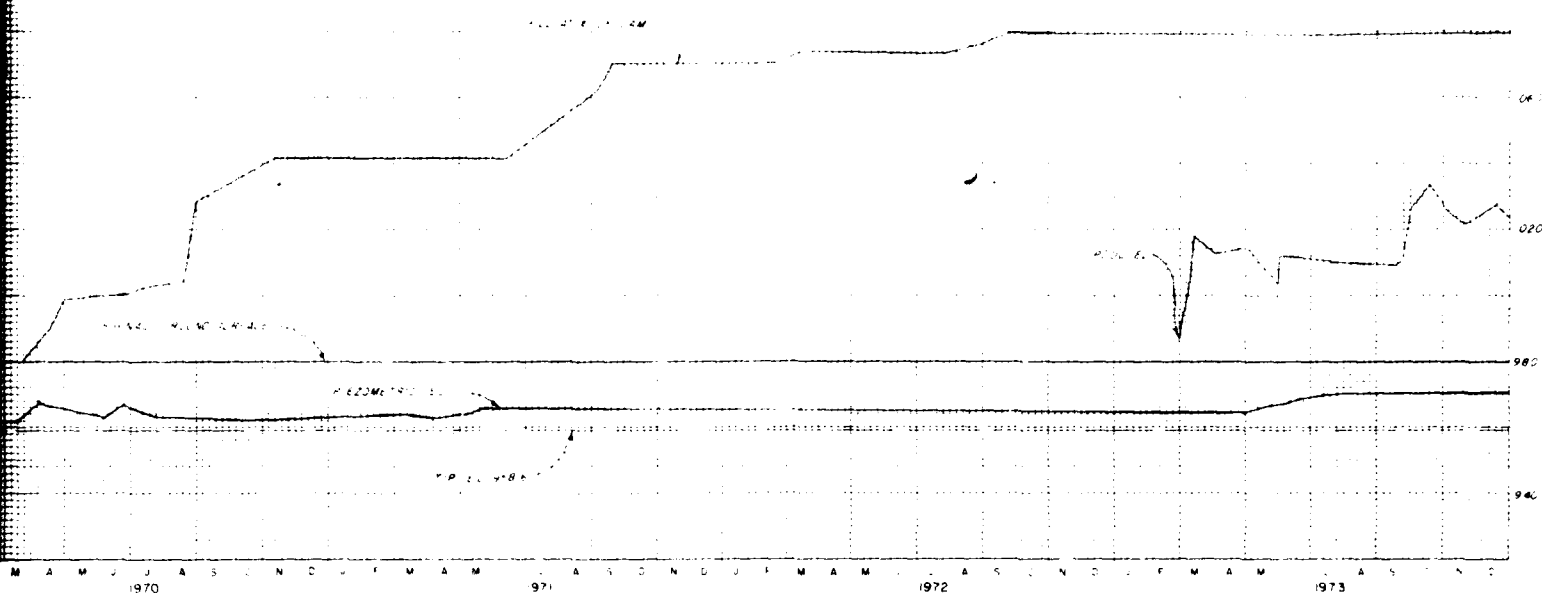
Scale as shown

CORPS OF ENGINEERS U.S. ARMY
 KANSAS CITY DISTRICT

FILE NO. 0-5-1298
 AUGUST 1975

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LEGEND
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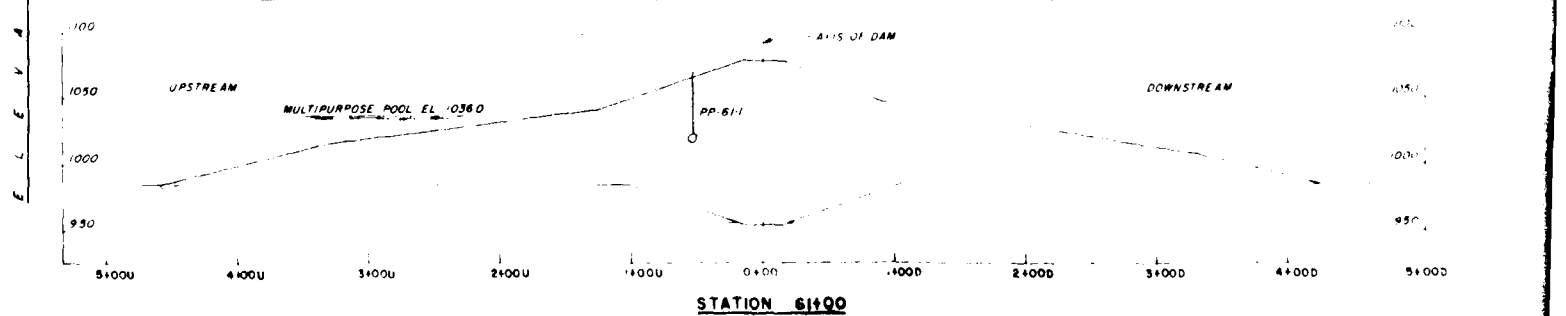
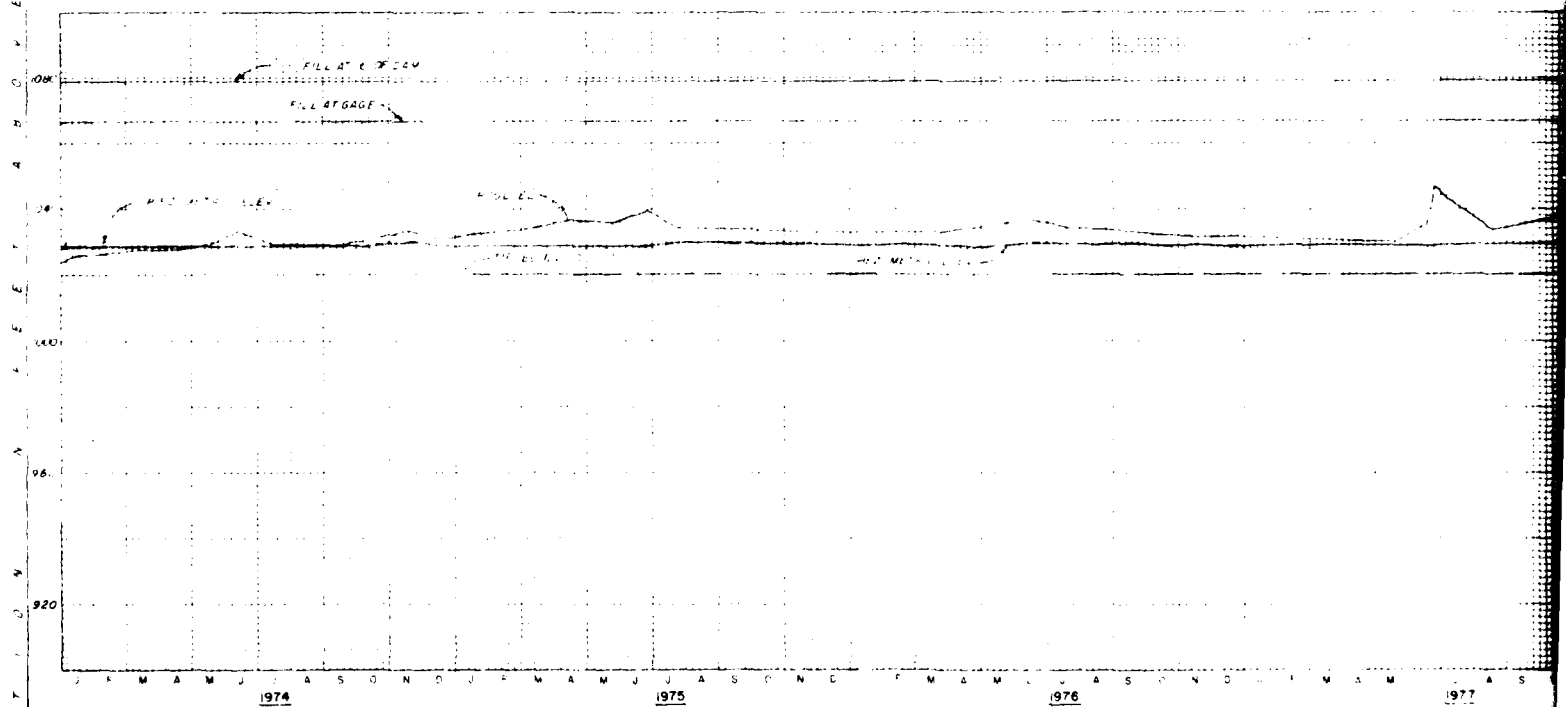
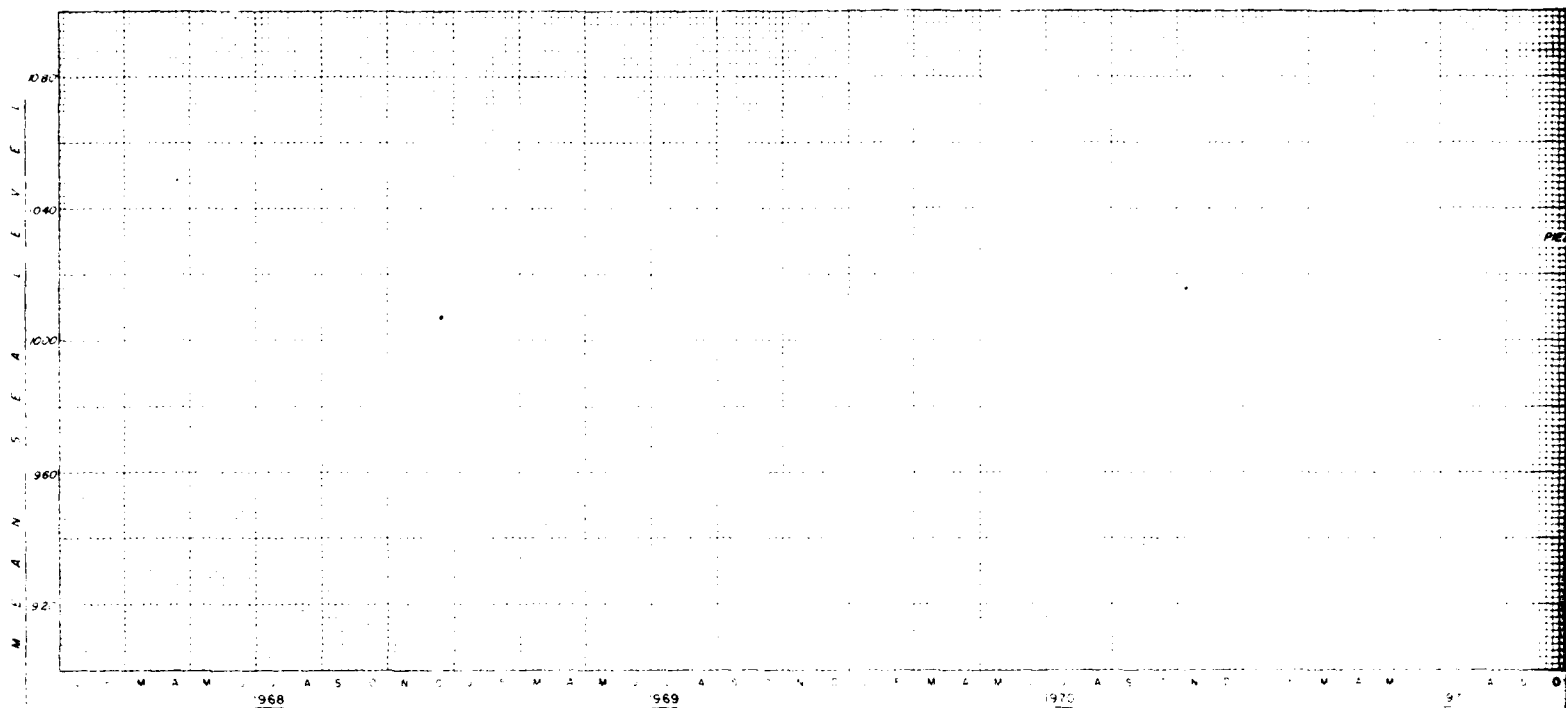
MARSH DES CYGNES RIVER, KANSAS
MELVERN LAKE

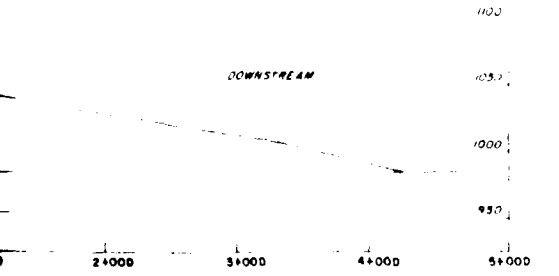
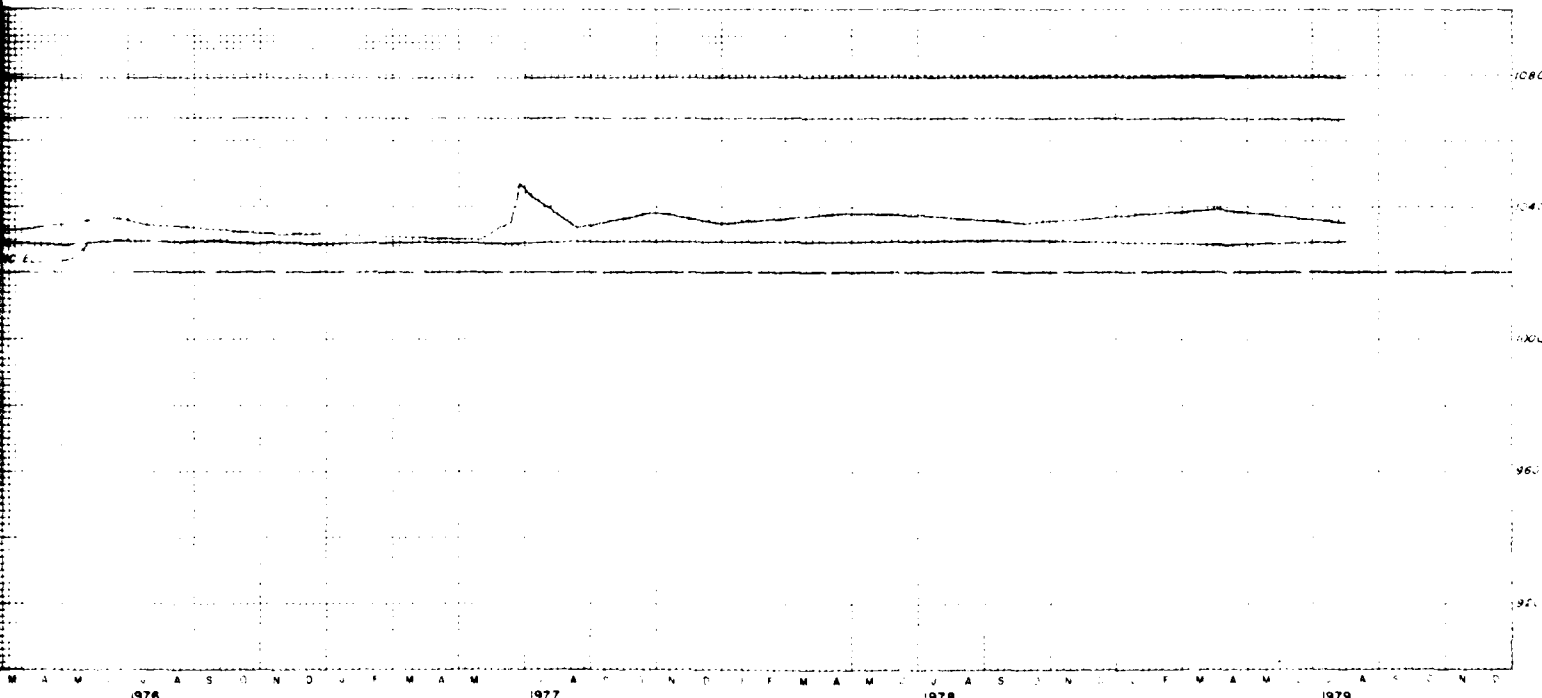
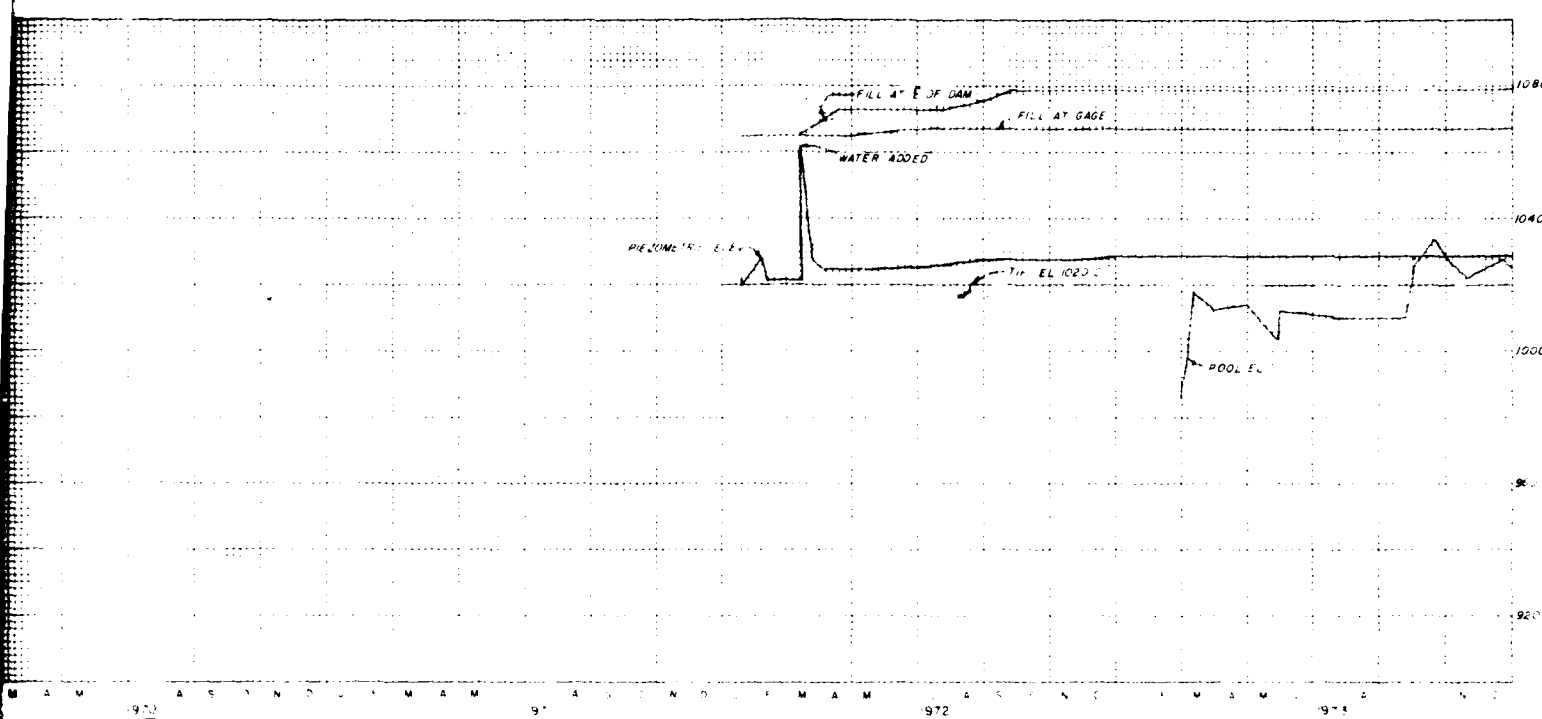
INSTRUMENTATION PLOTS
 PZ-60-10(OPEN TUBE)

Sheet No. 1
 CORPS OF ENGINEERS, U.S. ARMY
 KANSAS CITY DISTRICT
 FILE NO 0-5-1299
 AUGUST 1975

SCALE AS SHOWN

In 1 sheet





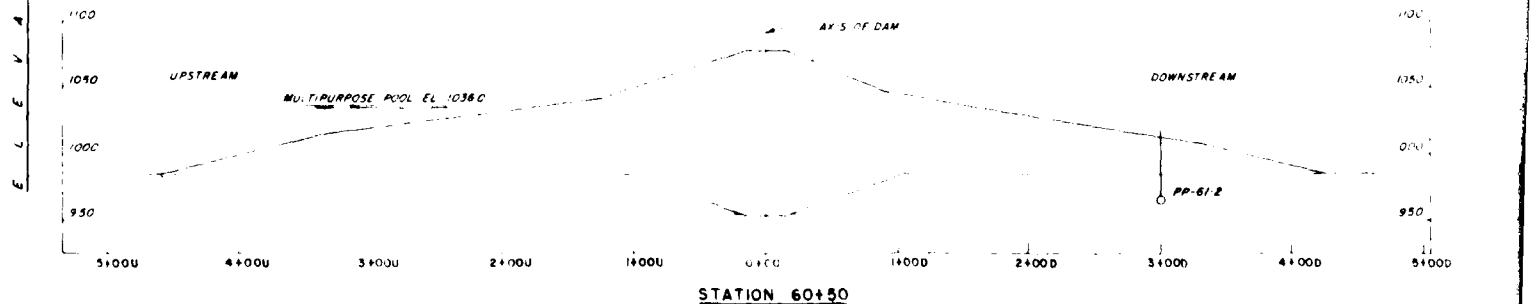
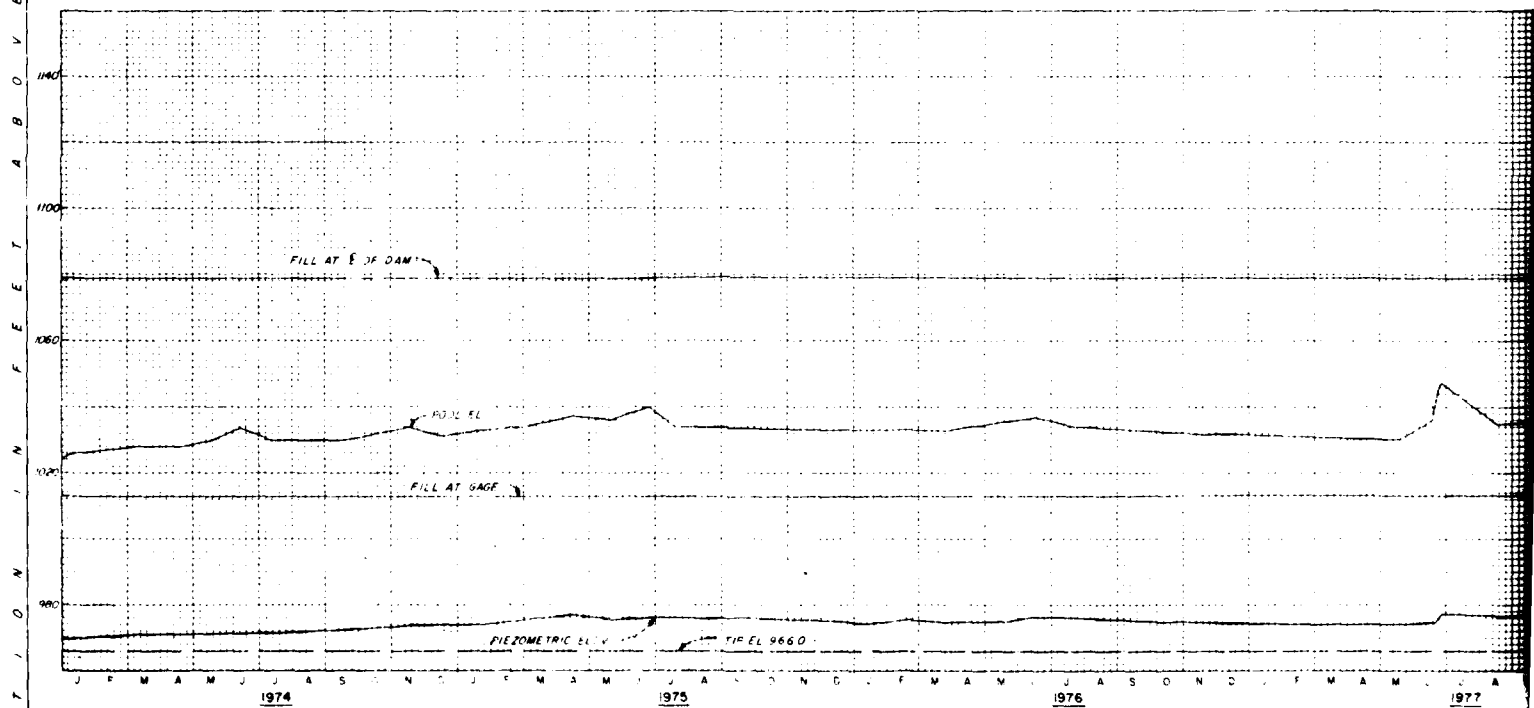
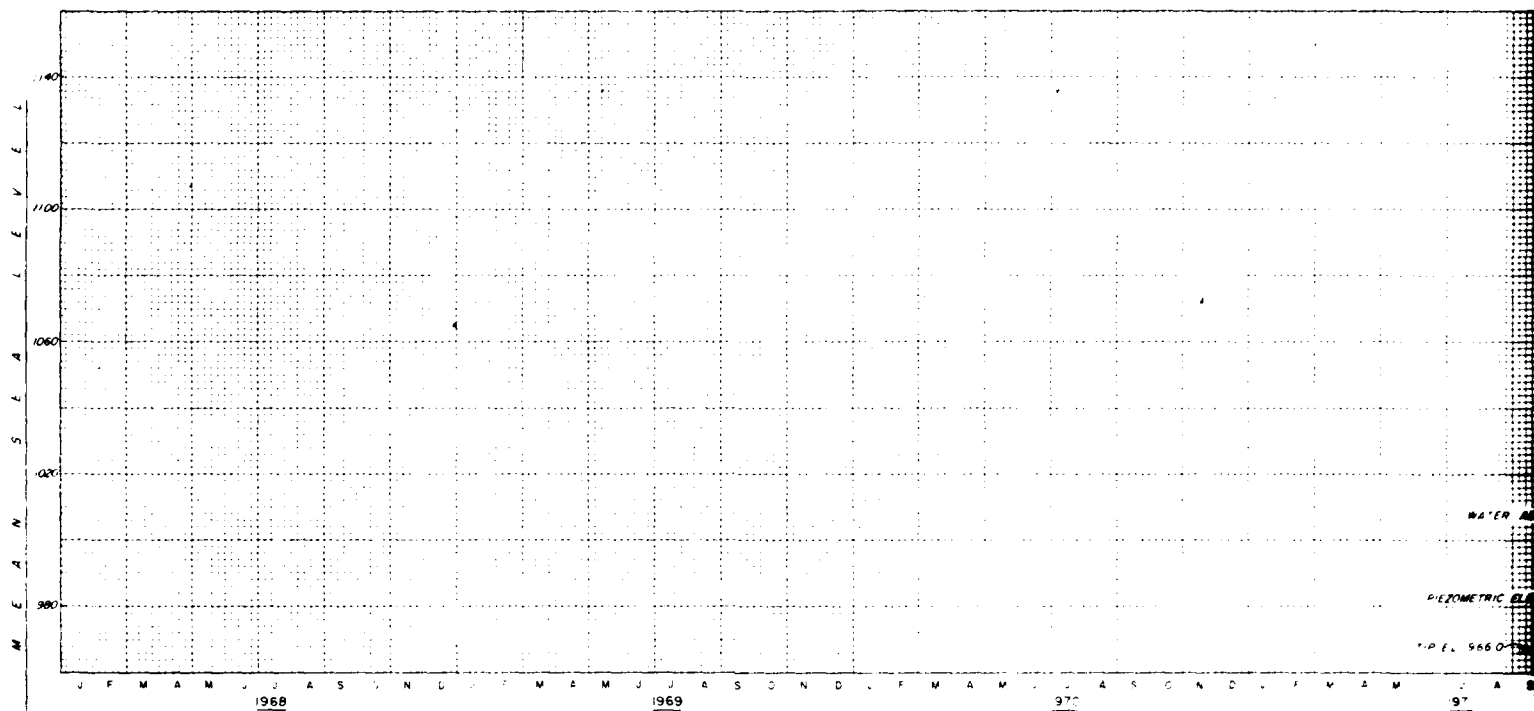
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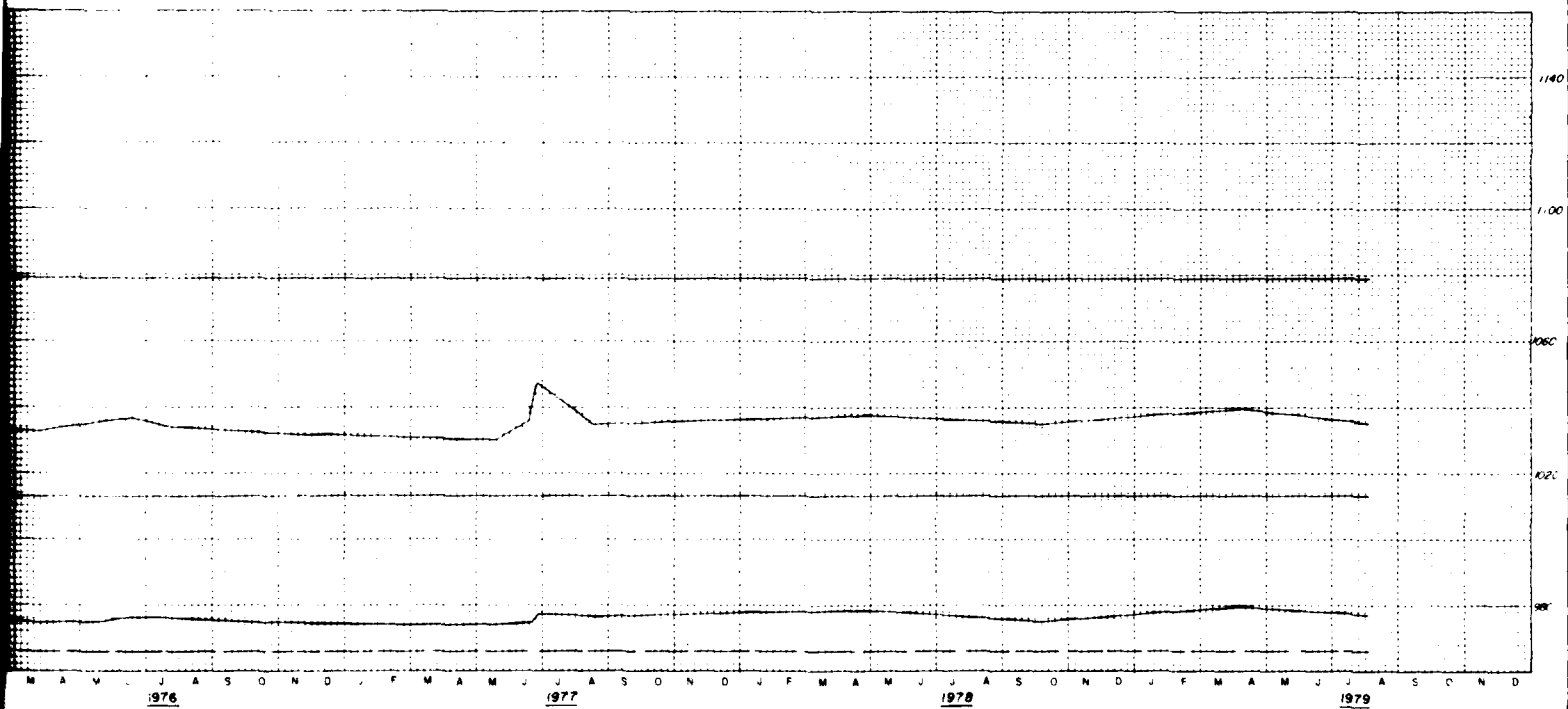
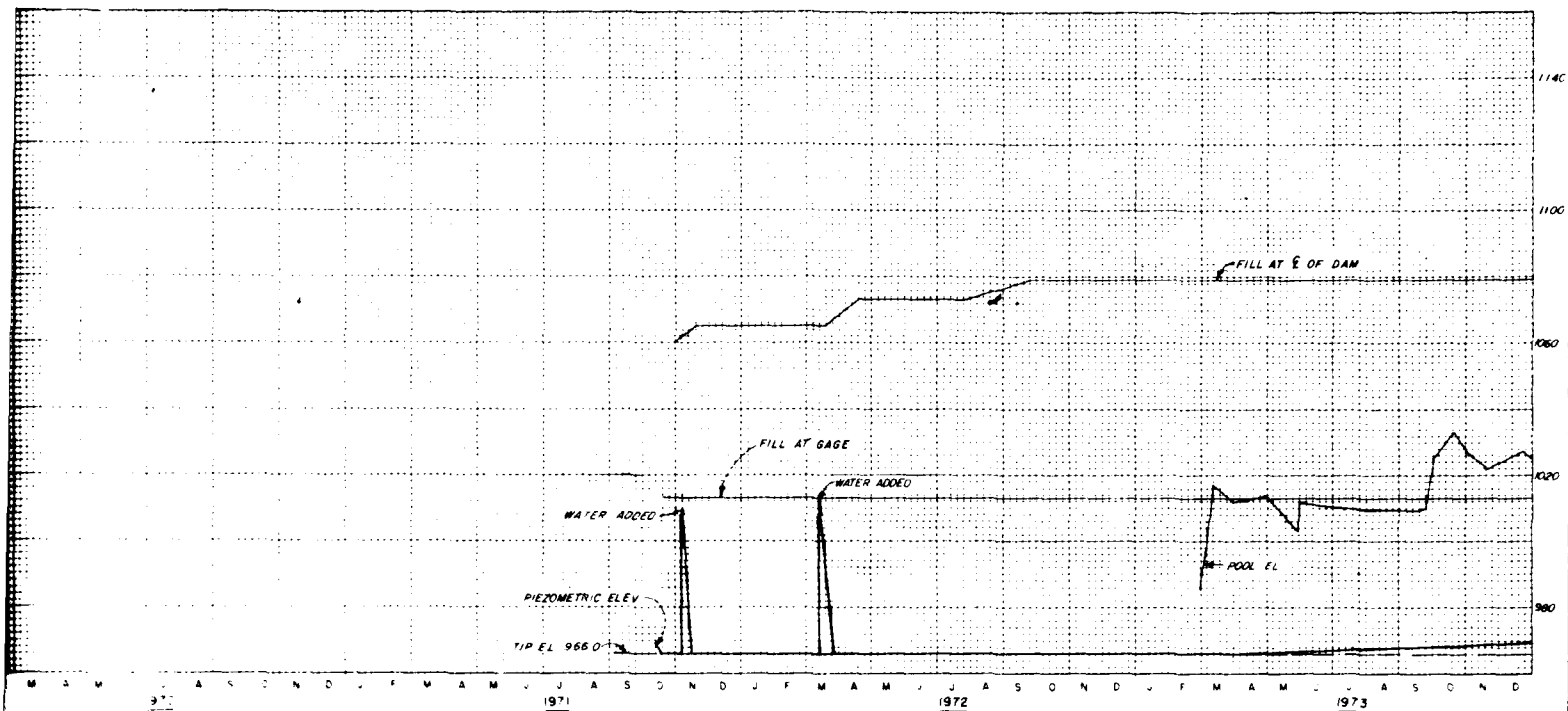
- OPEN TUBE ○
- PNEUMATIC CELL ●

MELVERN LAKE

INSTRUMENTATION PLOTS
PP-61-1 (OPEN TUBE)

Sheet No. 1
Scale as shown
FILE NO 0-5-1300
AUGUST 1975





DOWNSTREAM

PP-61-B

LEGEND

OPEN TUBE
PNEUMATIC CELL

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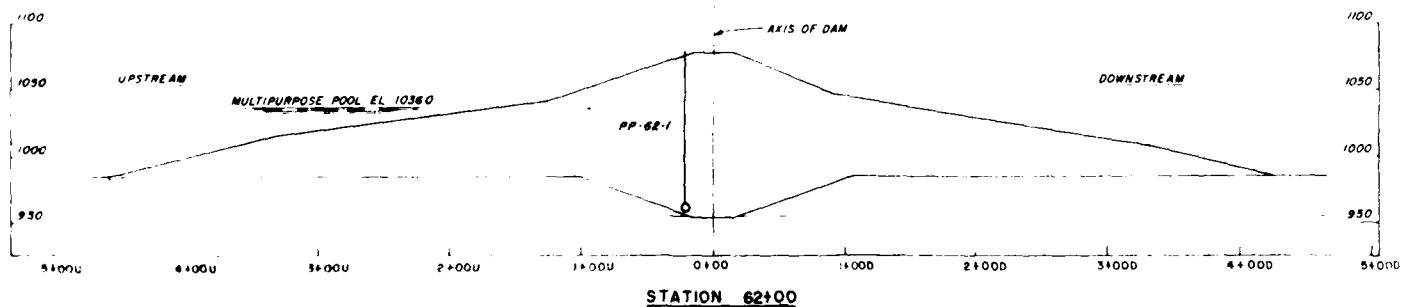
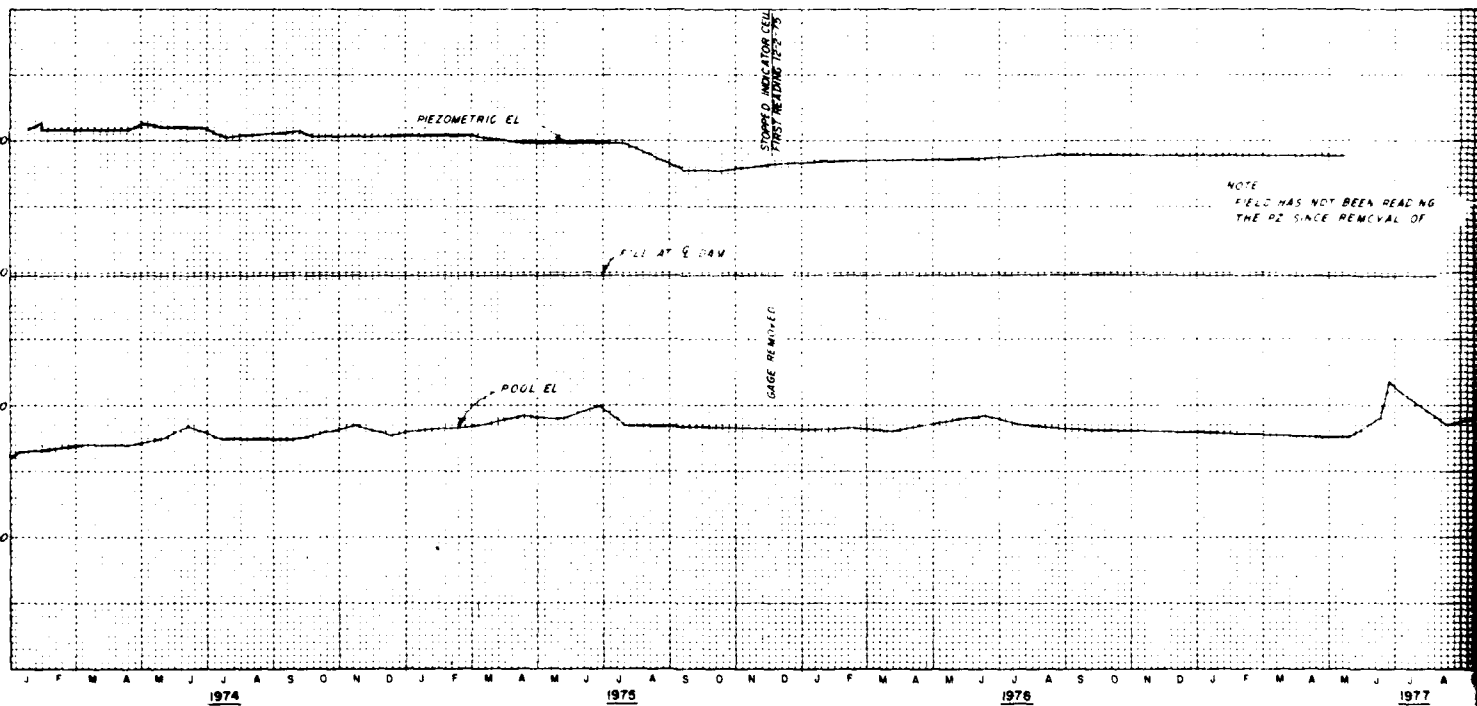
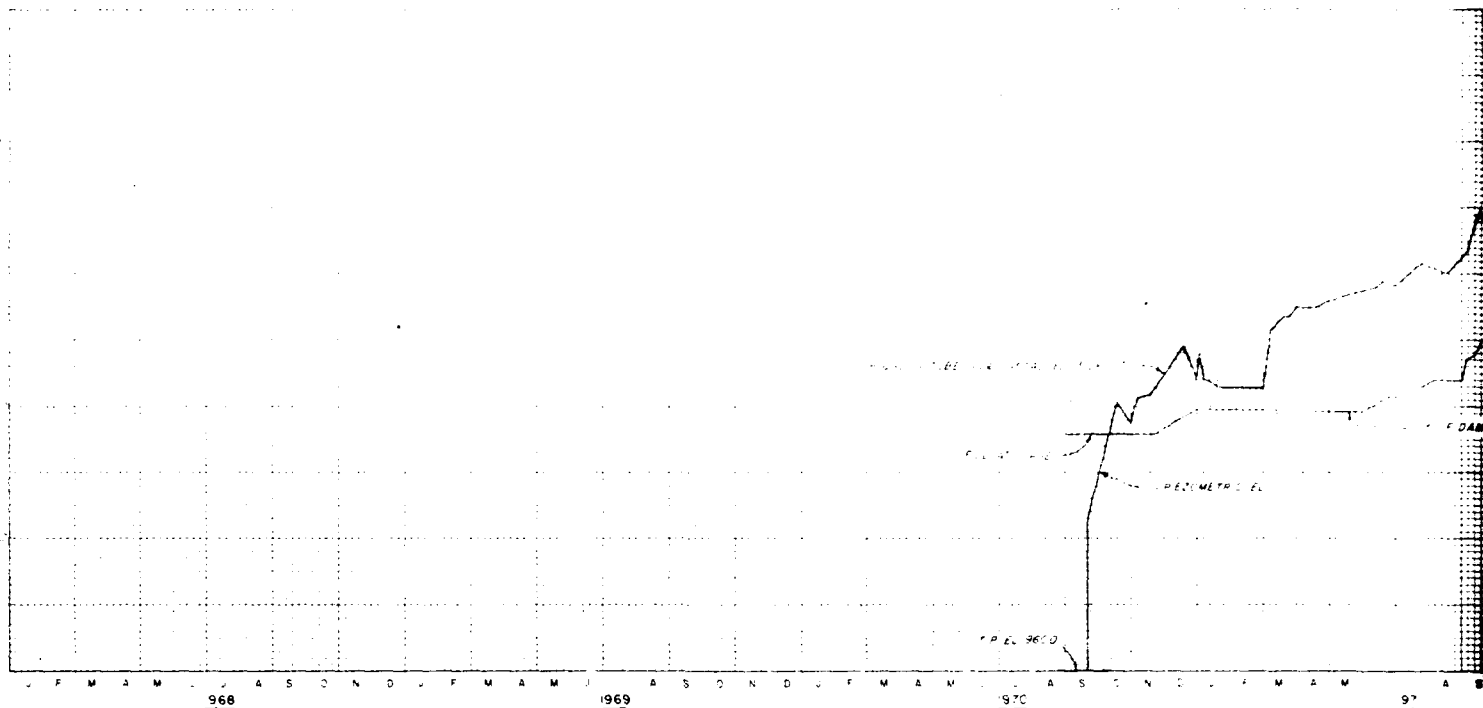
MELVERN LAKE

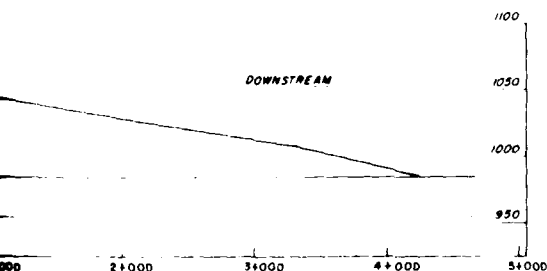
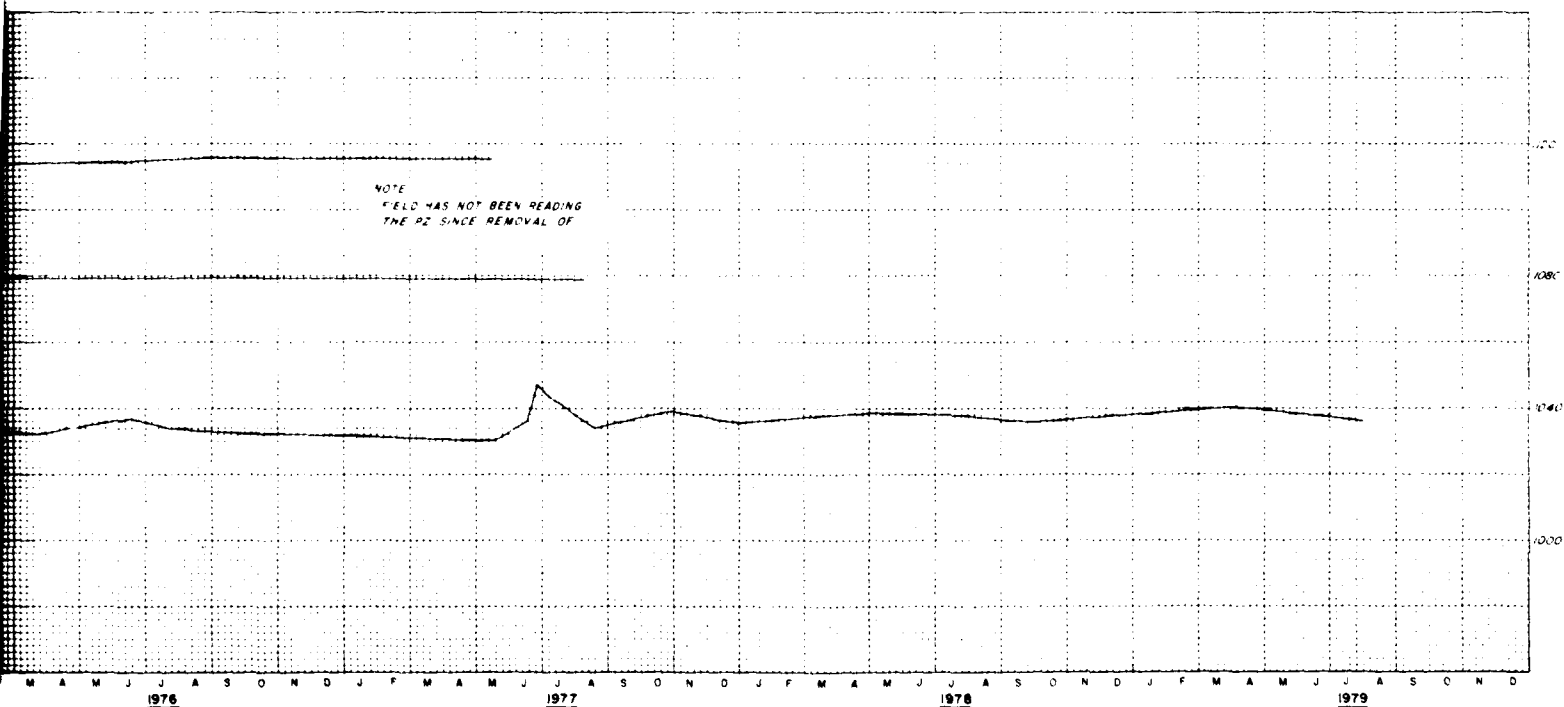
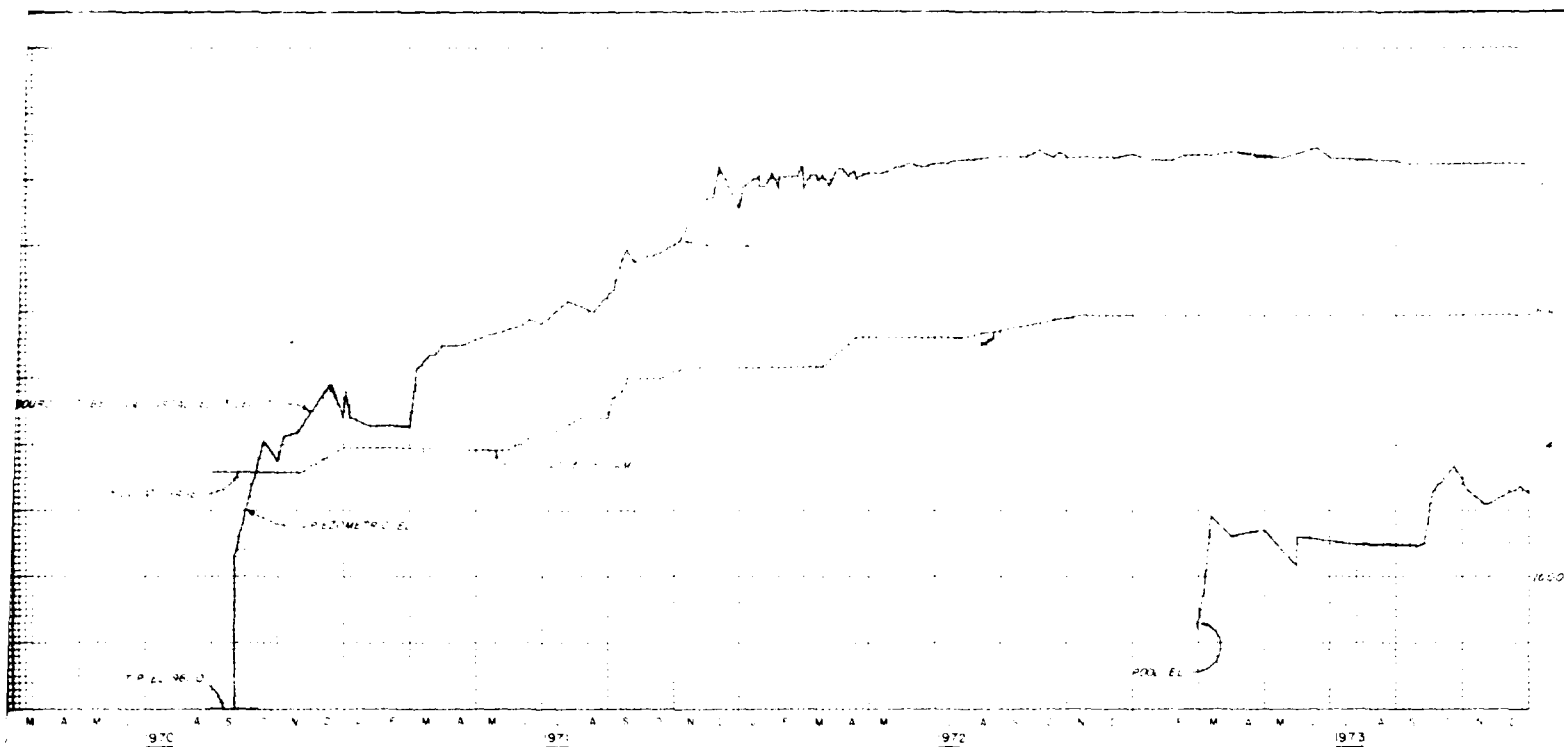
INSTRUMENTATION PLOTS
PP-61-2 (OPEN TUBE)

FILE NO 0-5-1301
AUGUST 1974

Scale as shown

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LEGEND

OPEN TUBE O
PNEUMATIC CELL ●

Revised August 1979
MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

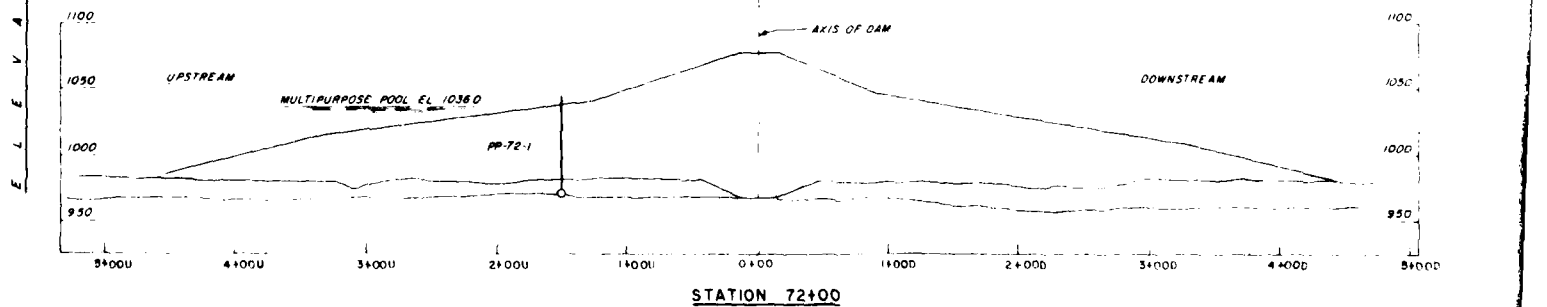
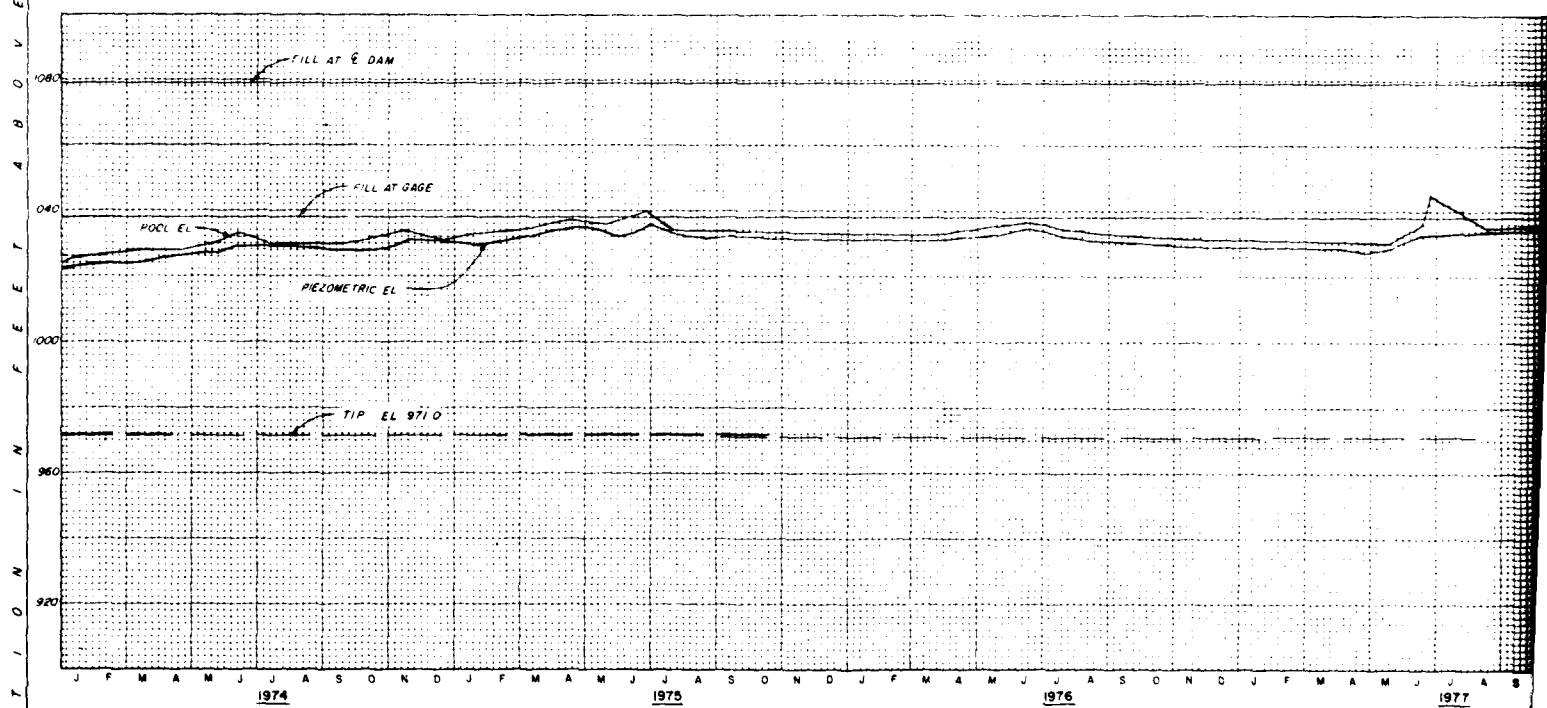
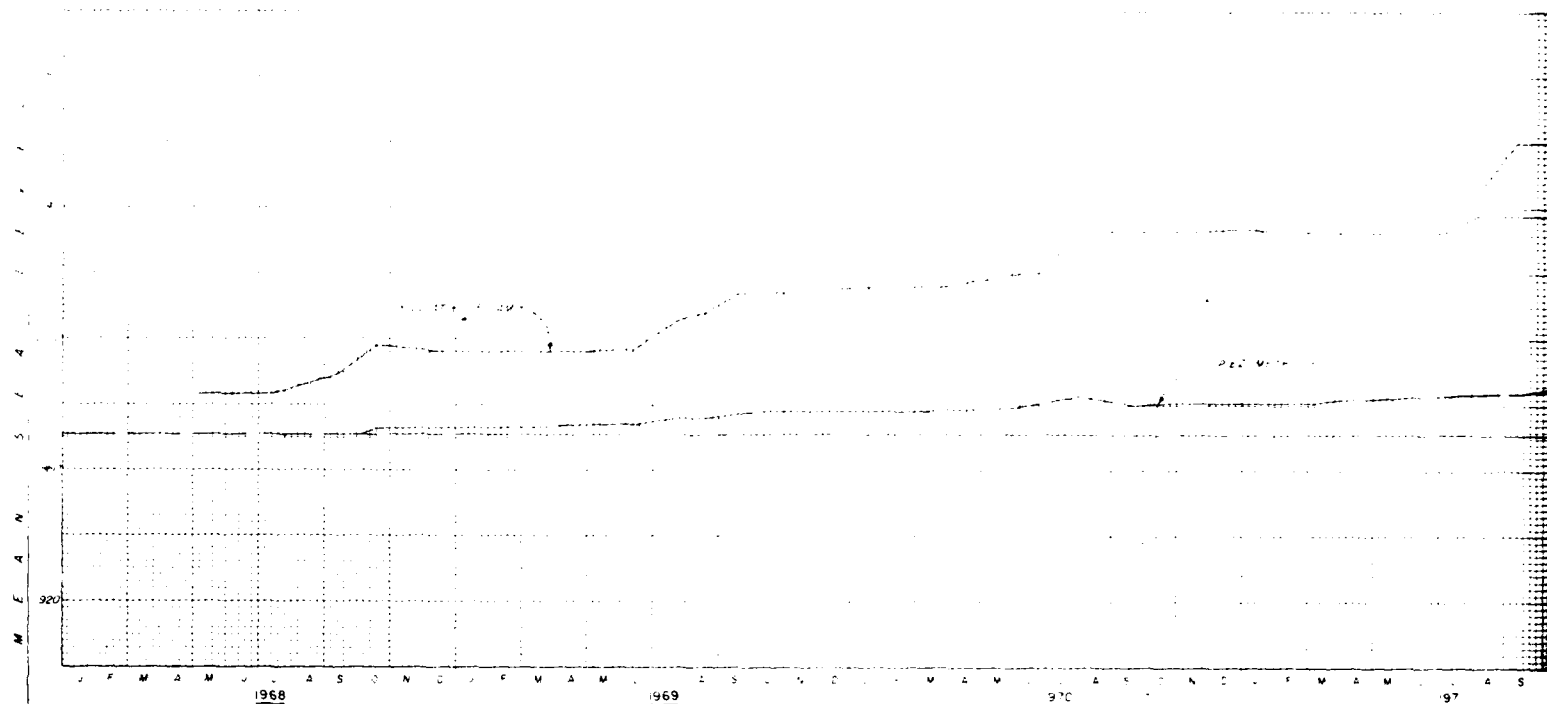
INSTRUMENTATION PLOTS
PP-62-1 (OPEN TUBE)

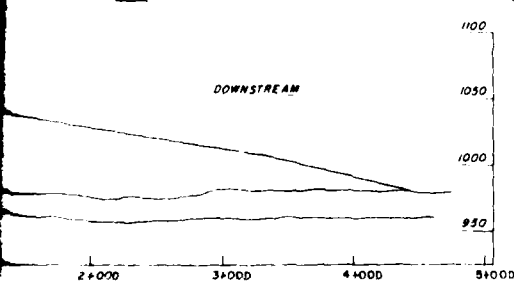
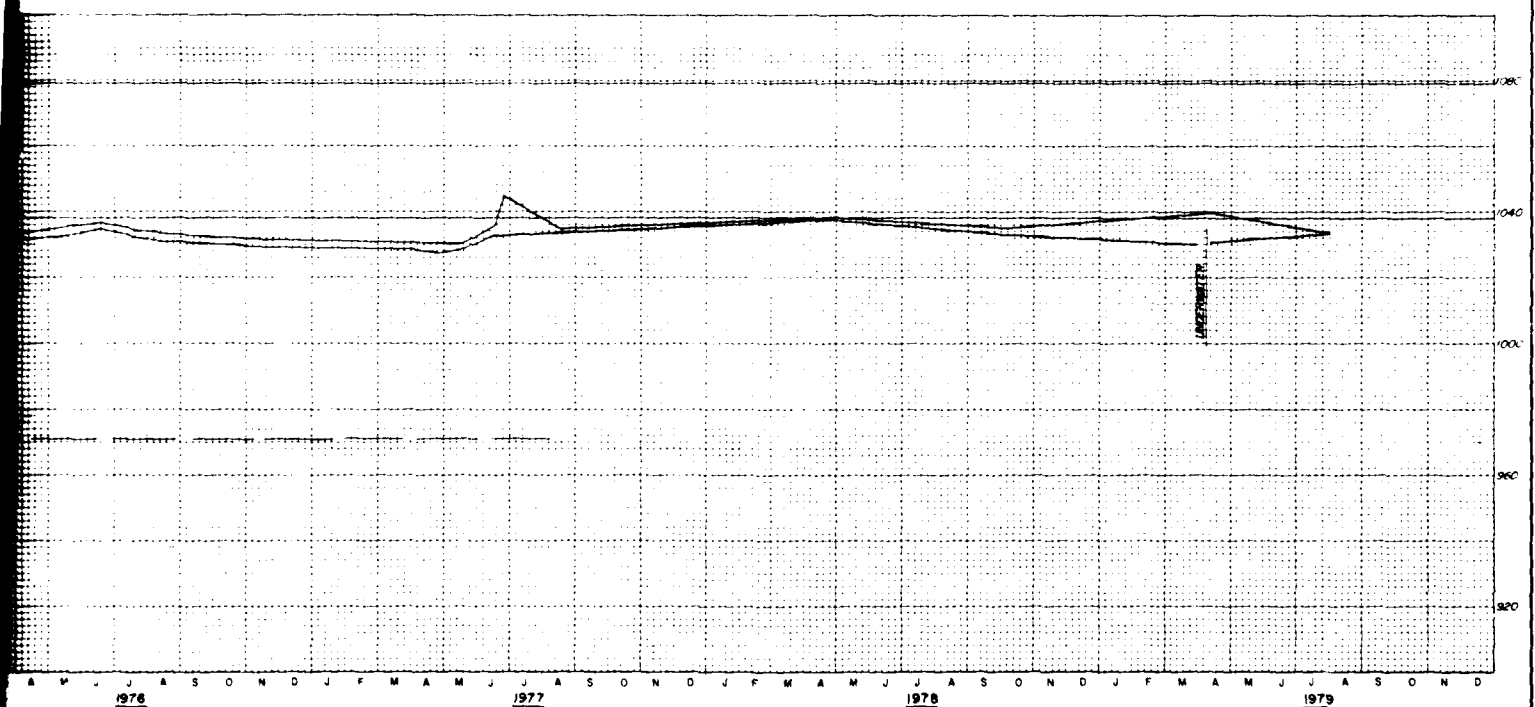
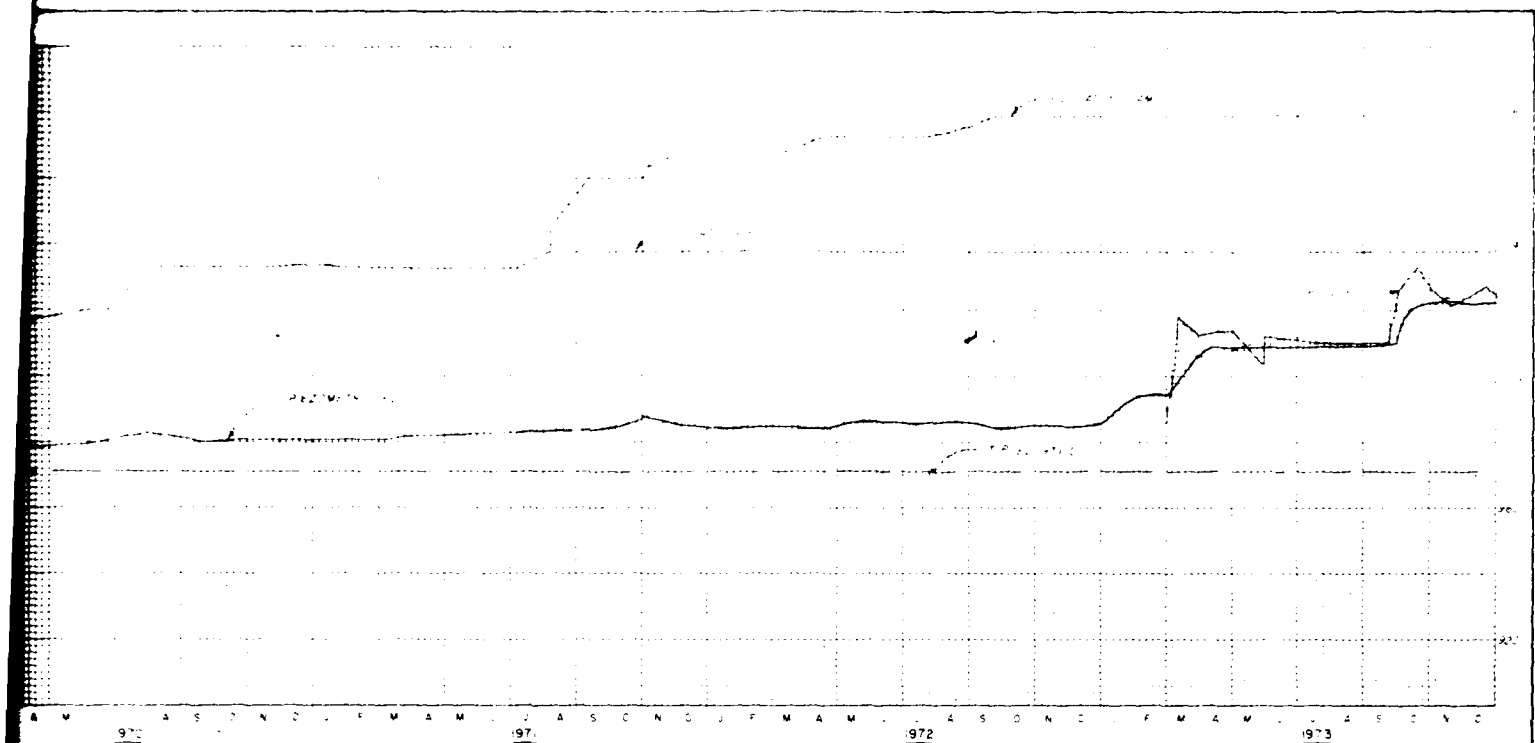
In 1 sheet

Sheet No. 1

Scale as shown

CORPS OF ENGINEERS U.S. ARMY
KANSAS CITY DISTRICT
FILE NO 0-5-1302
AUGUST 1975





LEGEND

OPEN TUBE — ○
PNEUMATIC CELL — ●

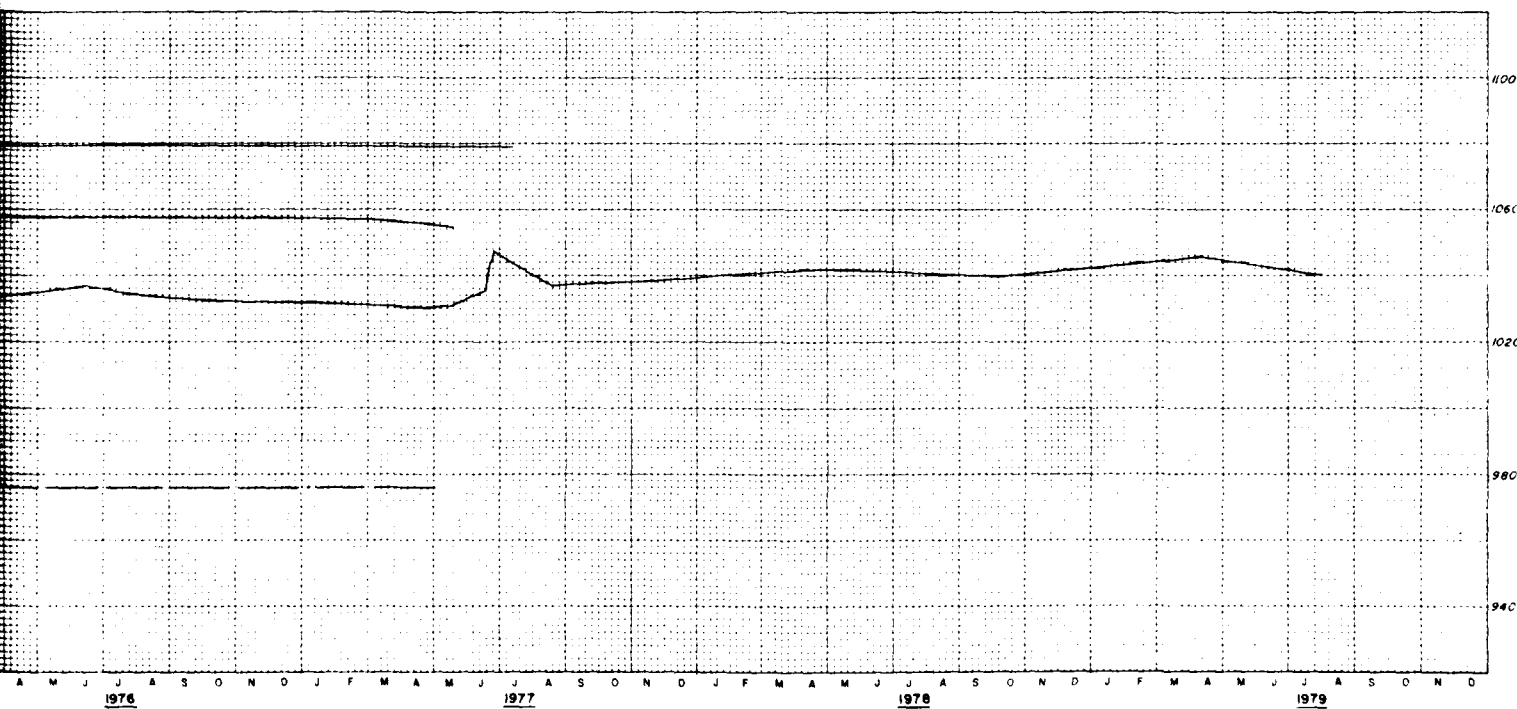
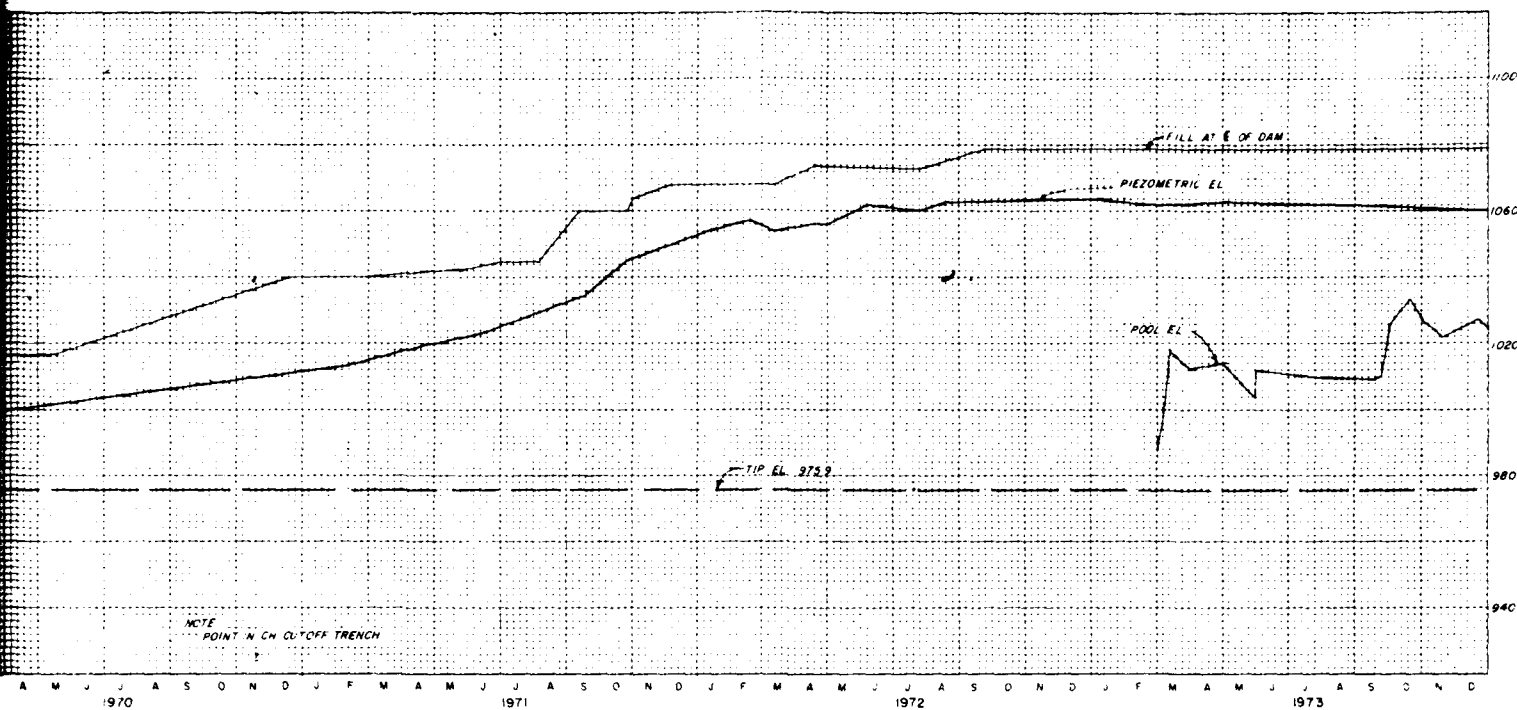
Revised August 1979
MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
PP-72-1 (OPEN TUBE)

In 1 sheet

Sheet No. 1
CORPS OF ENGINEERS U.S. ARMY
KANSAS CITY DISTRICT
FILE NO. 0-5-1303
AUGUST 1975

Scale as shown



DOWNSTREAM

LEGEND

OPEN TUBE ○
PNEUMATIC CELL ●

MELVERN LAKE

INSTRUMENTATION PLOTS
PP-72-2 (SHANNON-WILSON CELL)

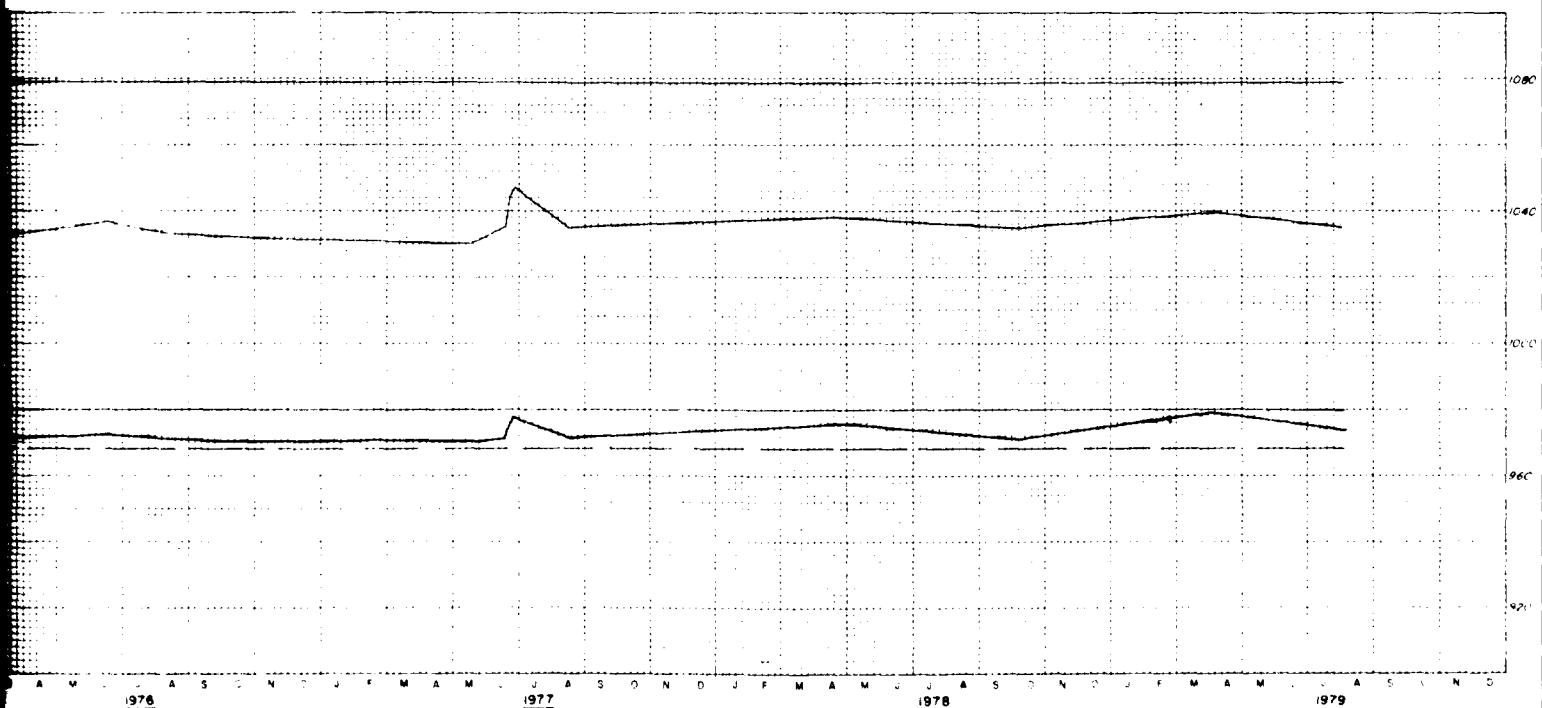
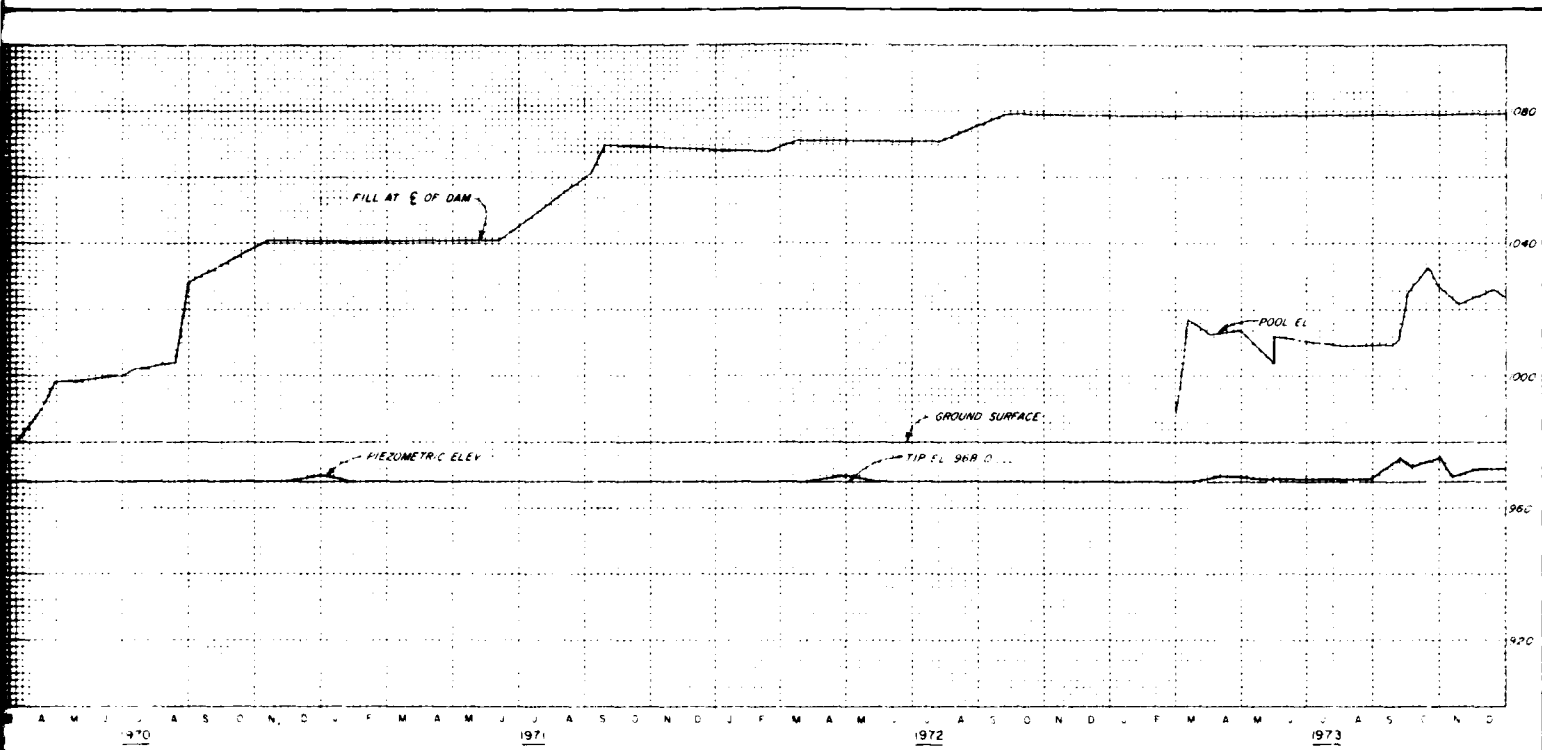
In 1 sheet

Sheet No. 1

Scale as shown

CORPS OF ENGINEERS U.S. ARMY
KANSAS CITY DISTRICT

FILE NO 0-5-1304
AUGUST 1975



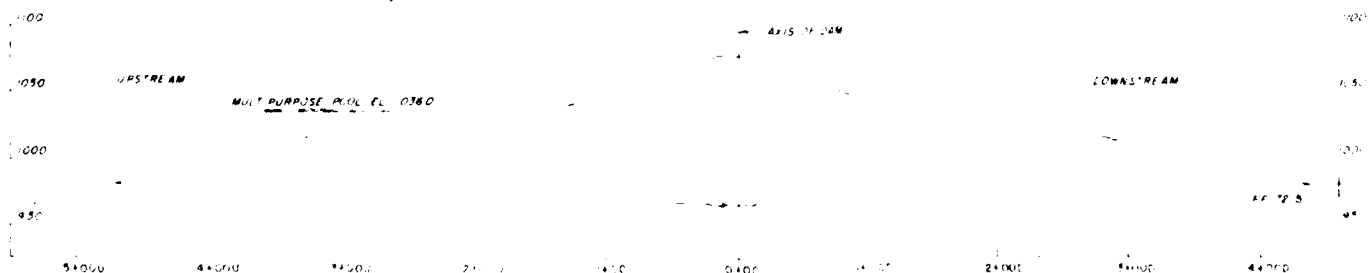
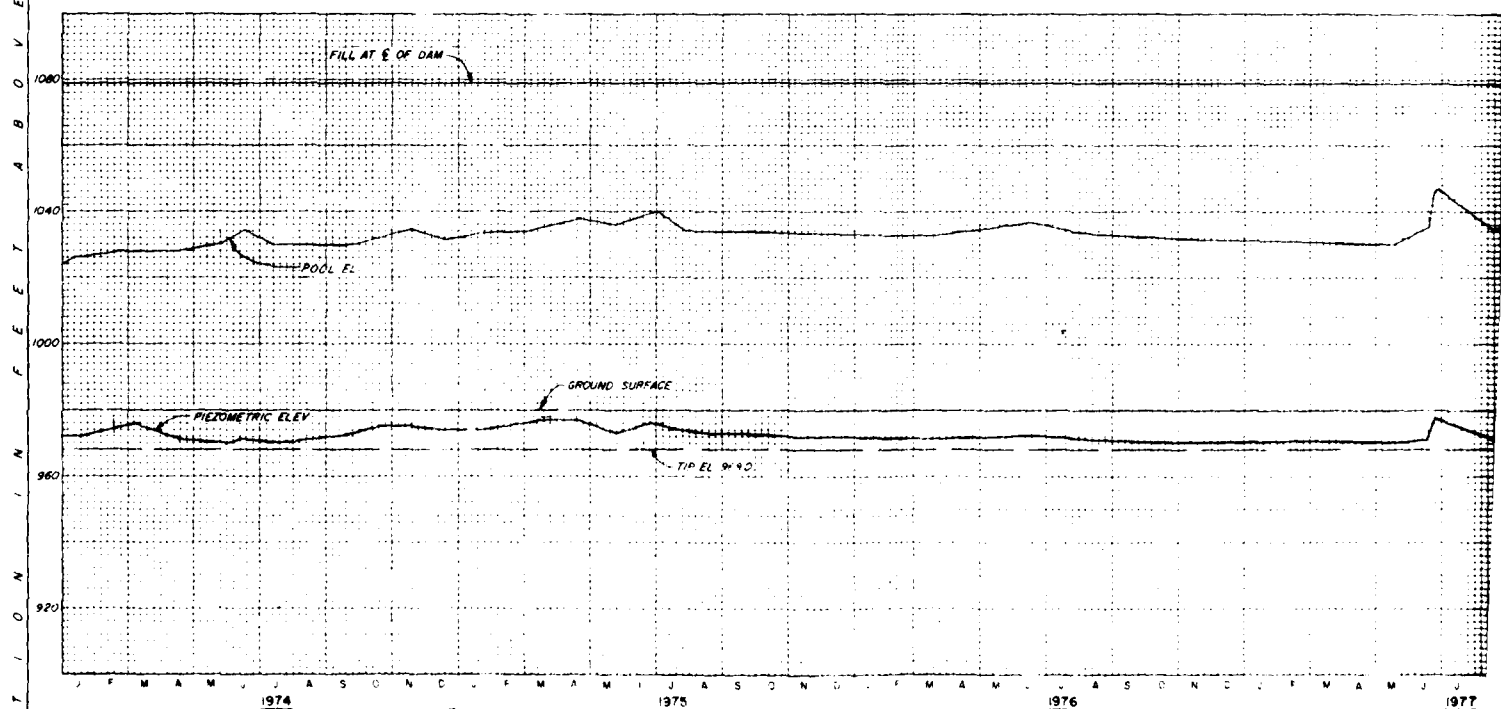
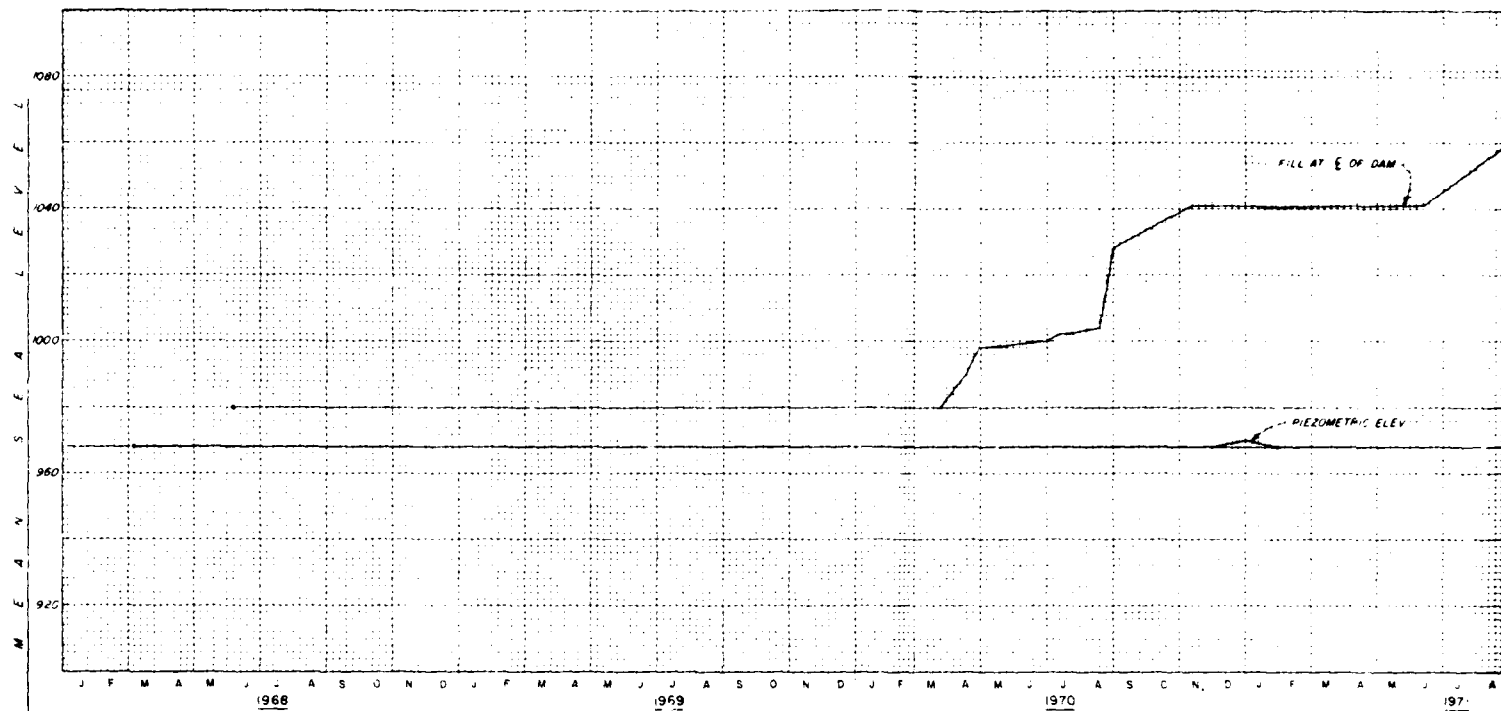
LEGEND

OPEN TUBE
PNEUMATIC CELL

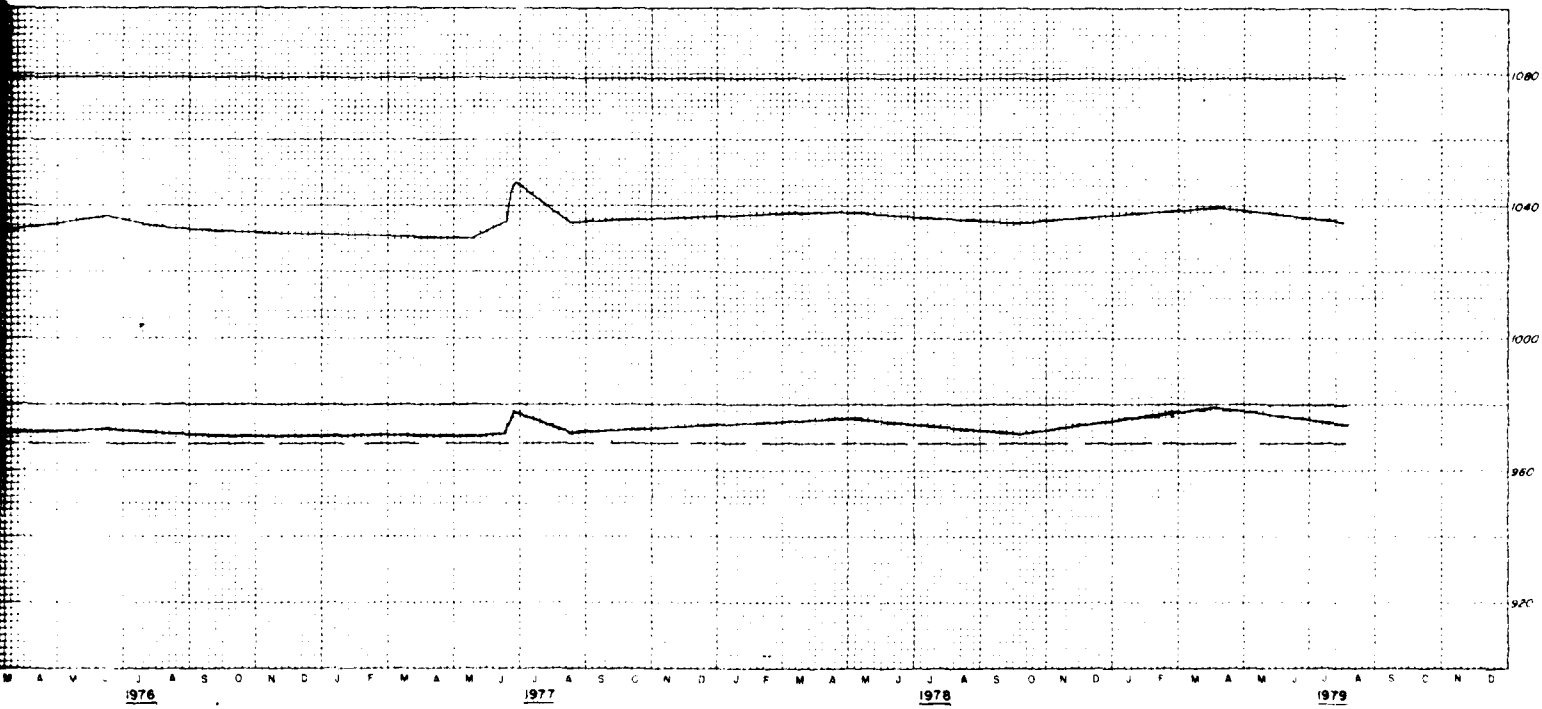
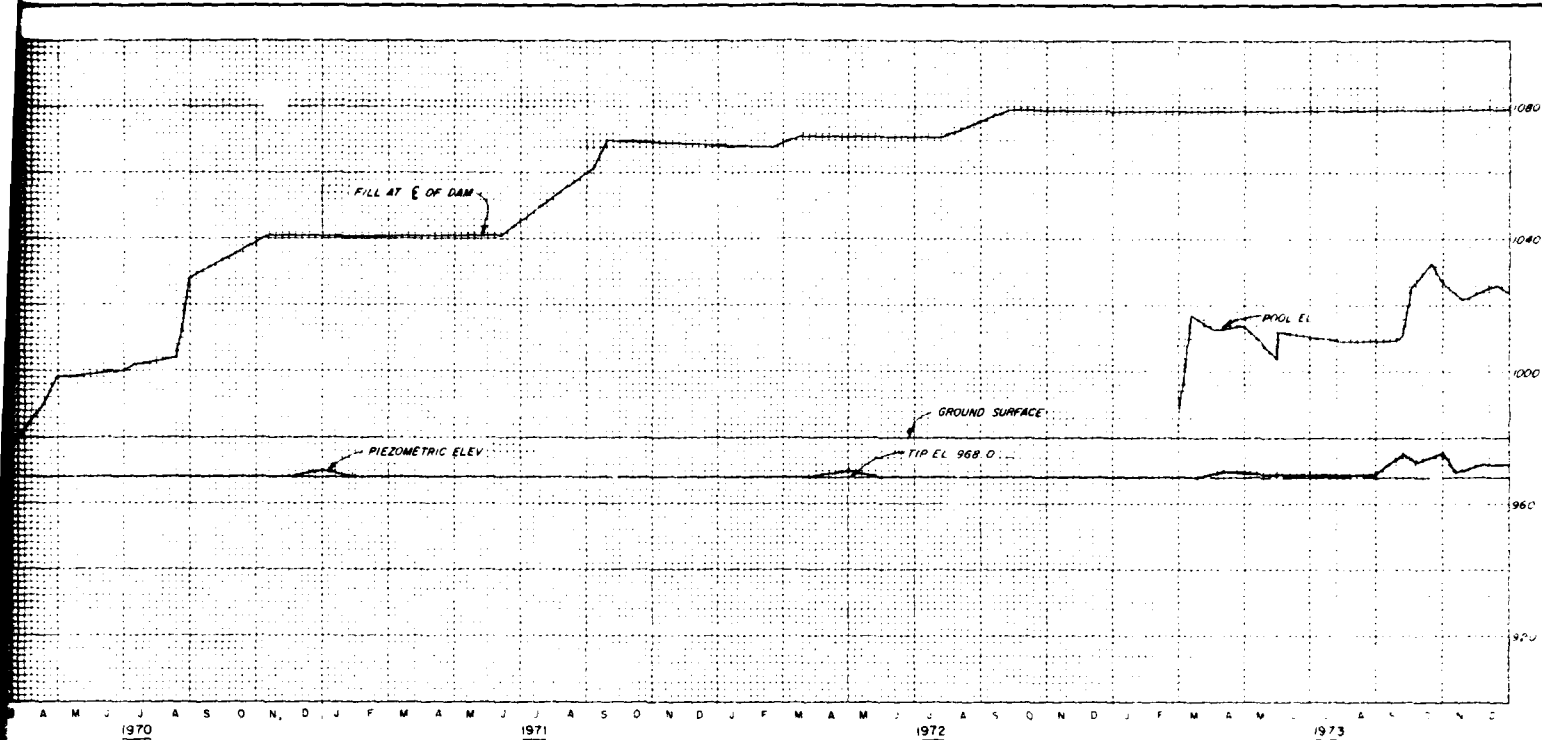
MAHAR DE LA RIVER KANUN
MELVERN LAKE

INSTRUMENTATION PLOTS
PP 72-5 (OPEN TUBE)

FILE NO. 0-5-1305



STATION 72+00



DOWNSTREAM

P-72-5

LEGEND

OPEN TUBE
PNEUMATIC CELL

MAHAIS DESIGNER RIVER KANSAS
MELVERN LAKE

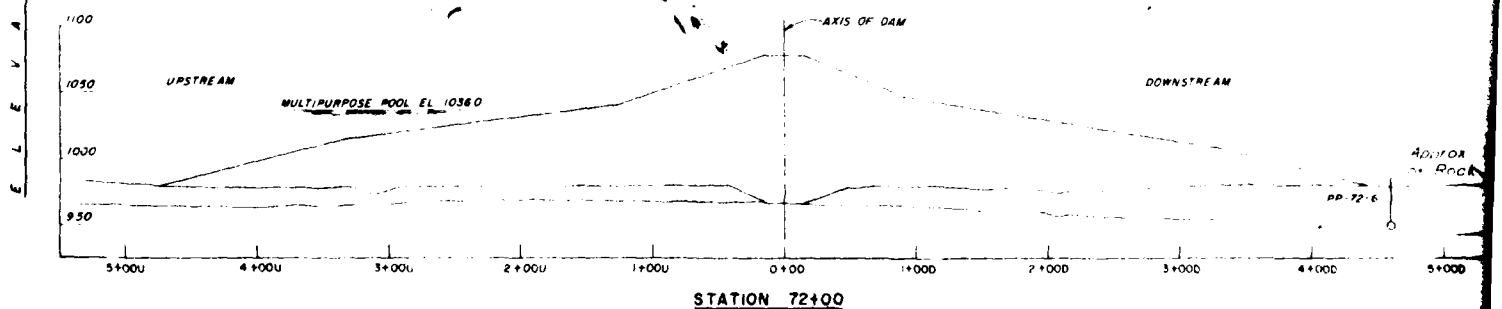
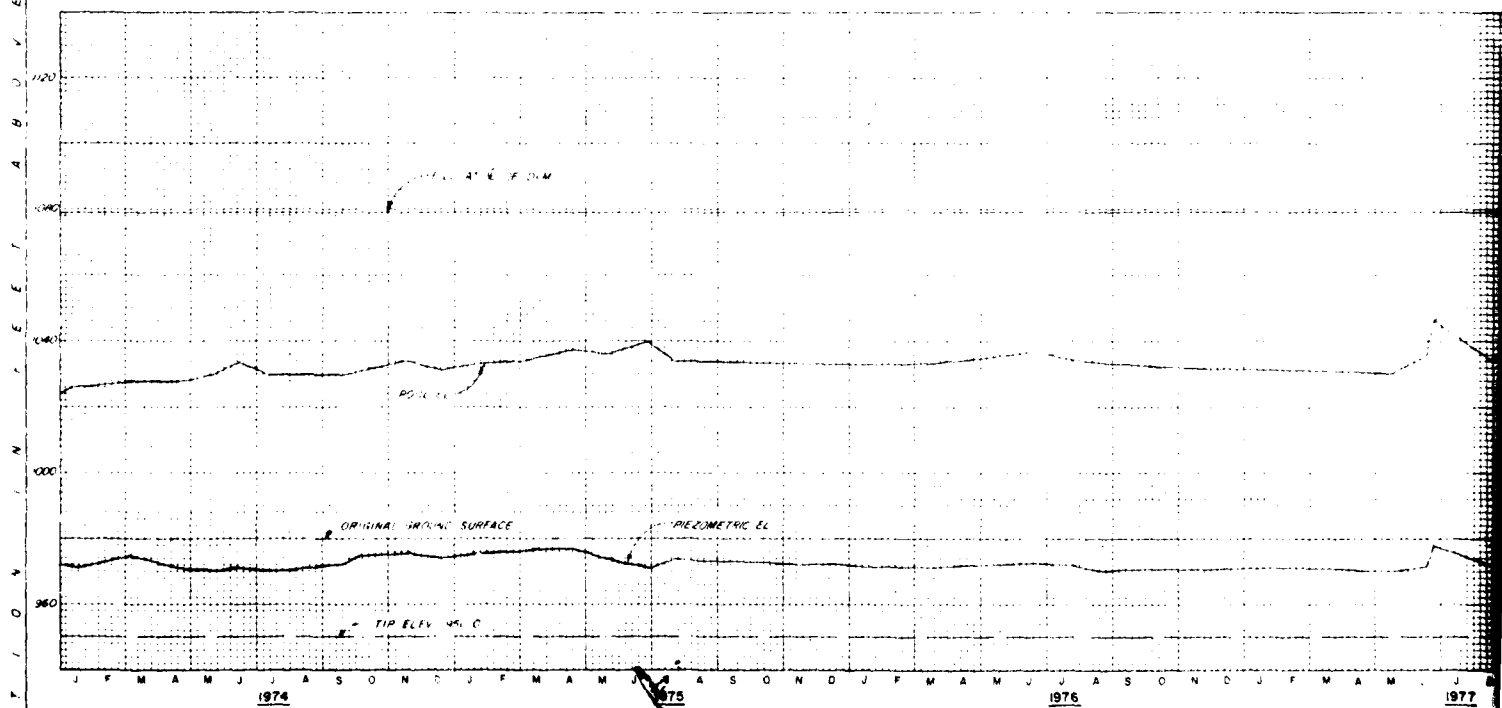
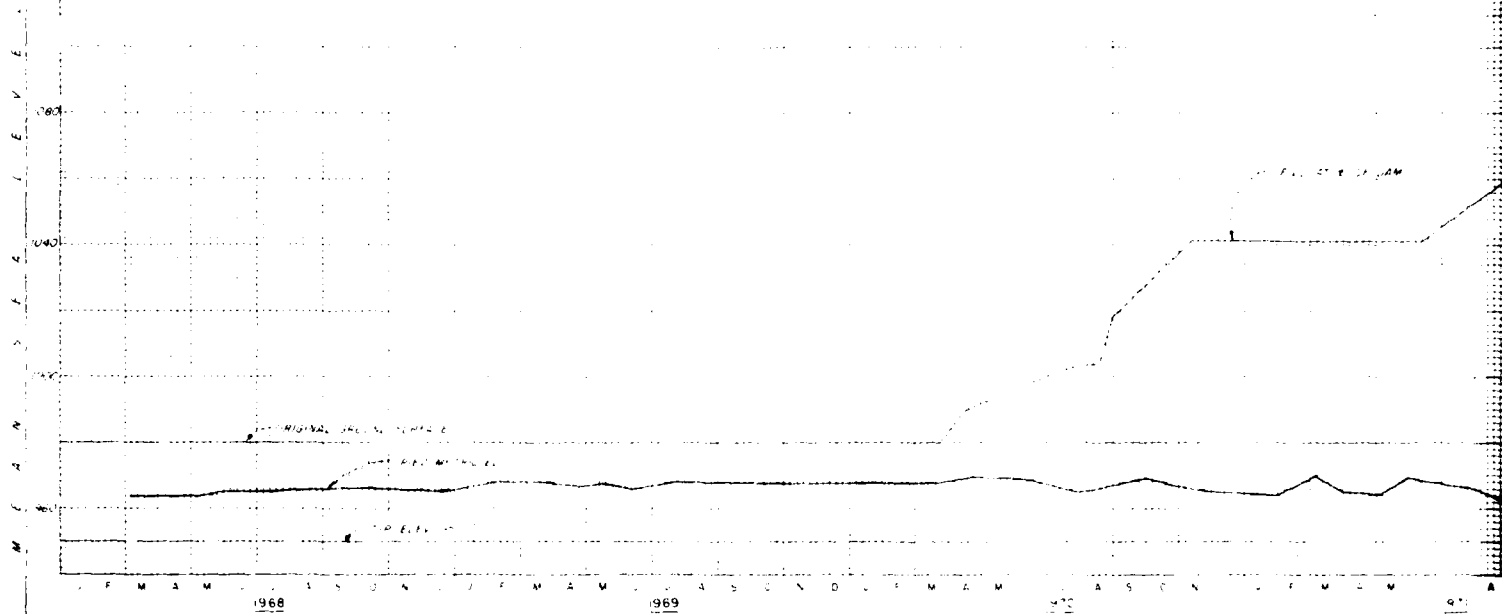
INSTRUMENTATION PLOTS
PP 72-5 (OPEN TUBE)

In 1 Sheet

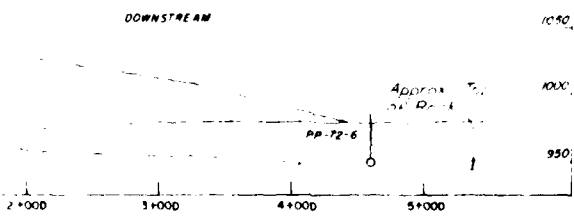
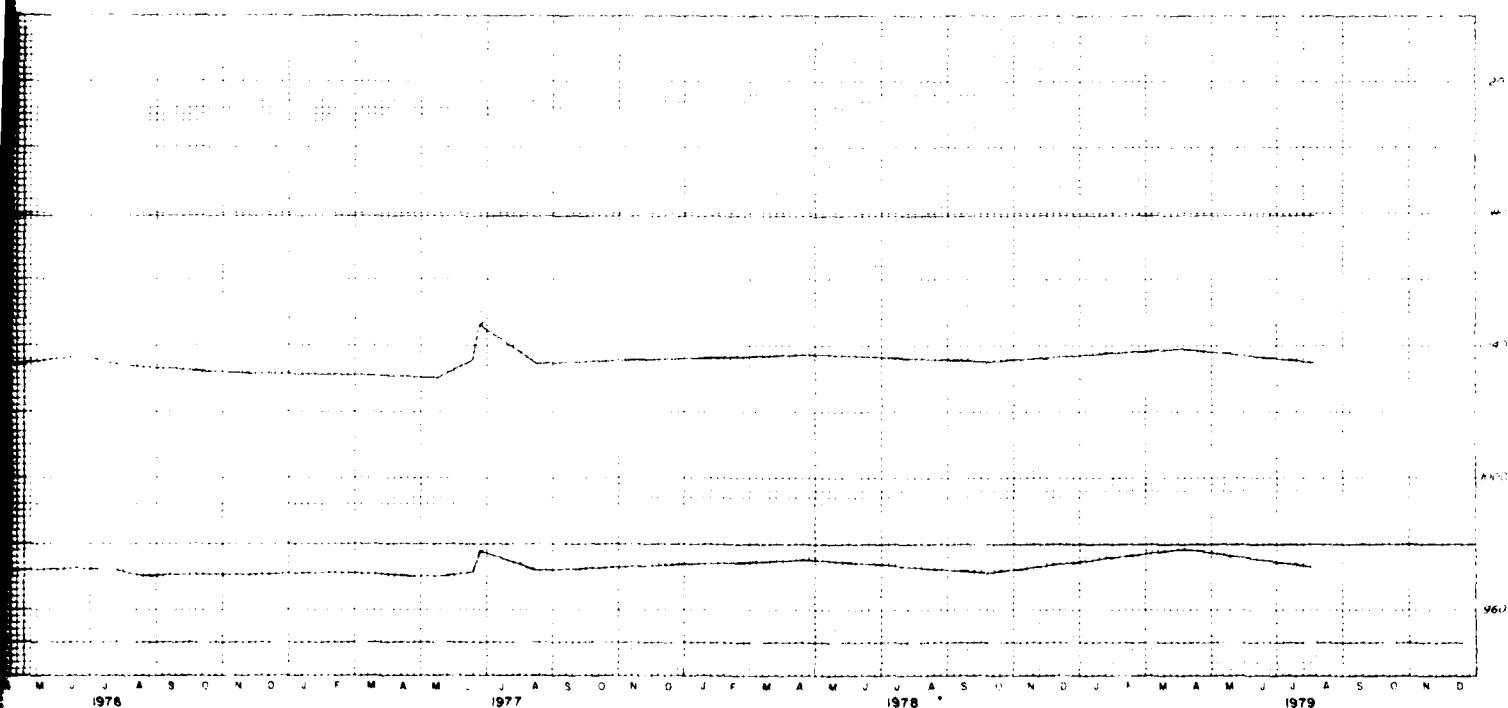
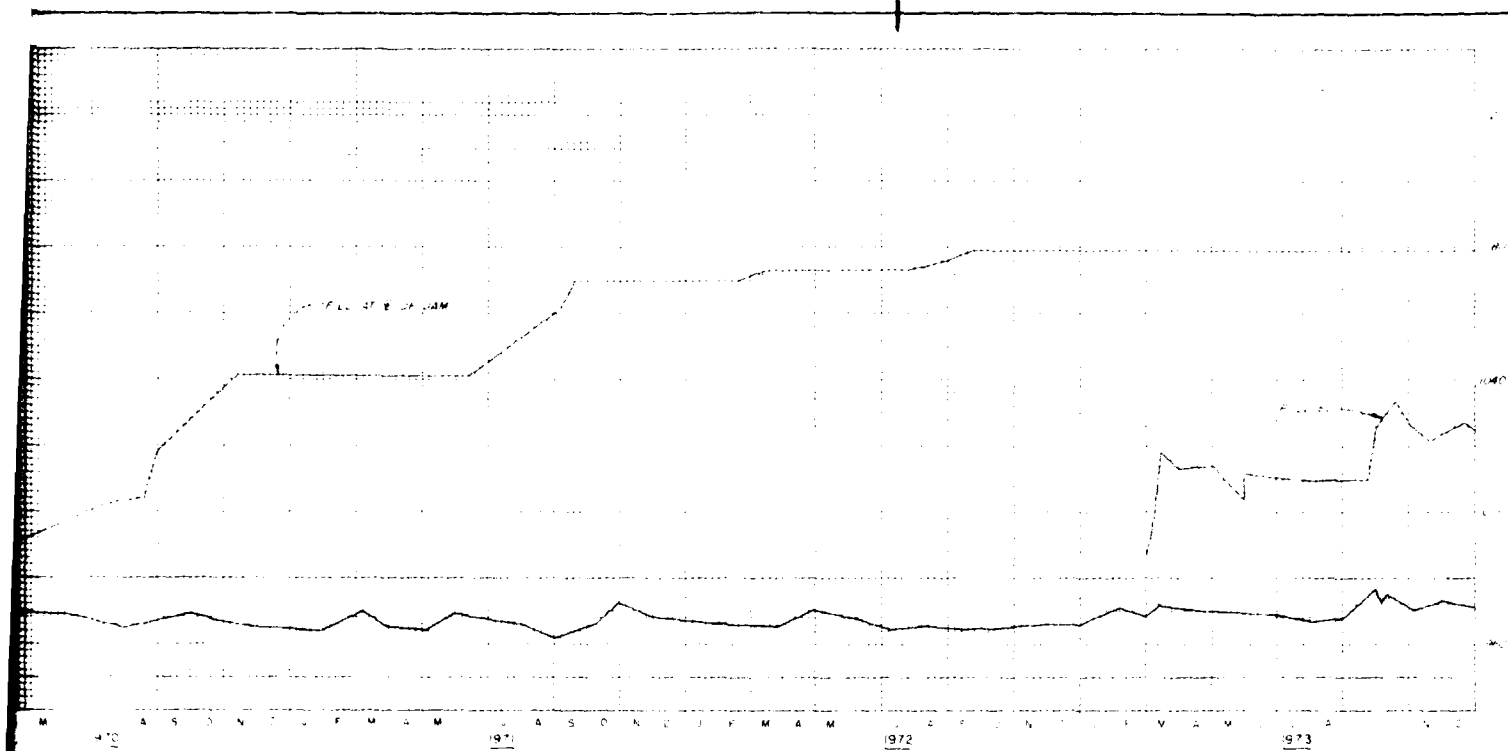
PROJECT NO. 1
BUREAU OF REVENUE
KANSAS STATE DEPT. OF REVENUE

FILE NO 0-5-1305
AUGUST 1978

SCALE AS SHOWN



STATION 72+00



LEGEND

OPEN TUBE
PNEUMATIC CELL

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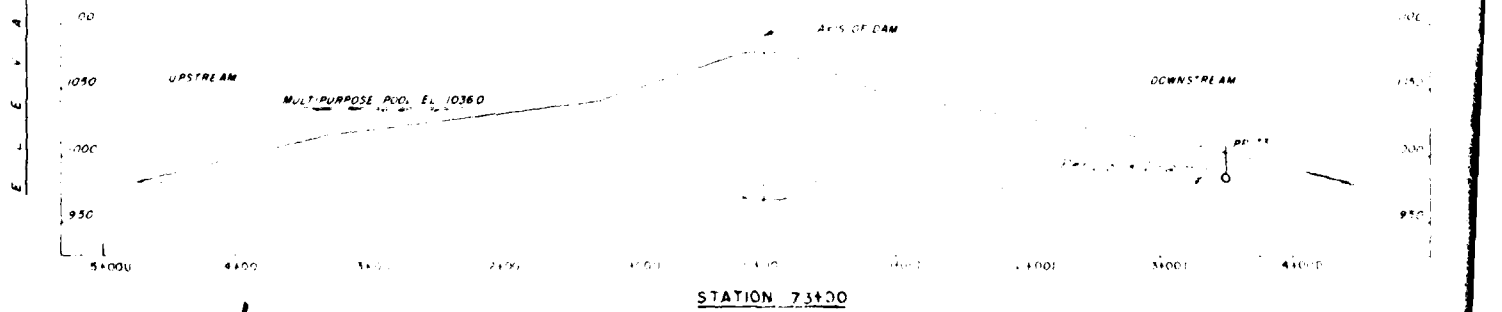
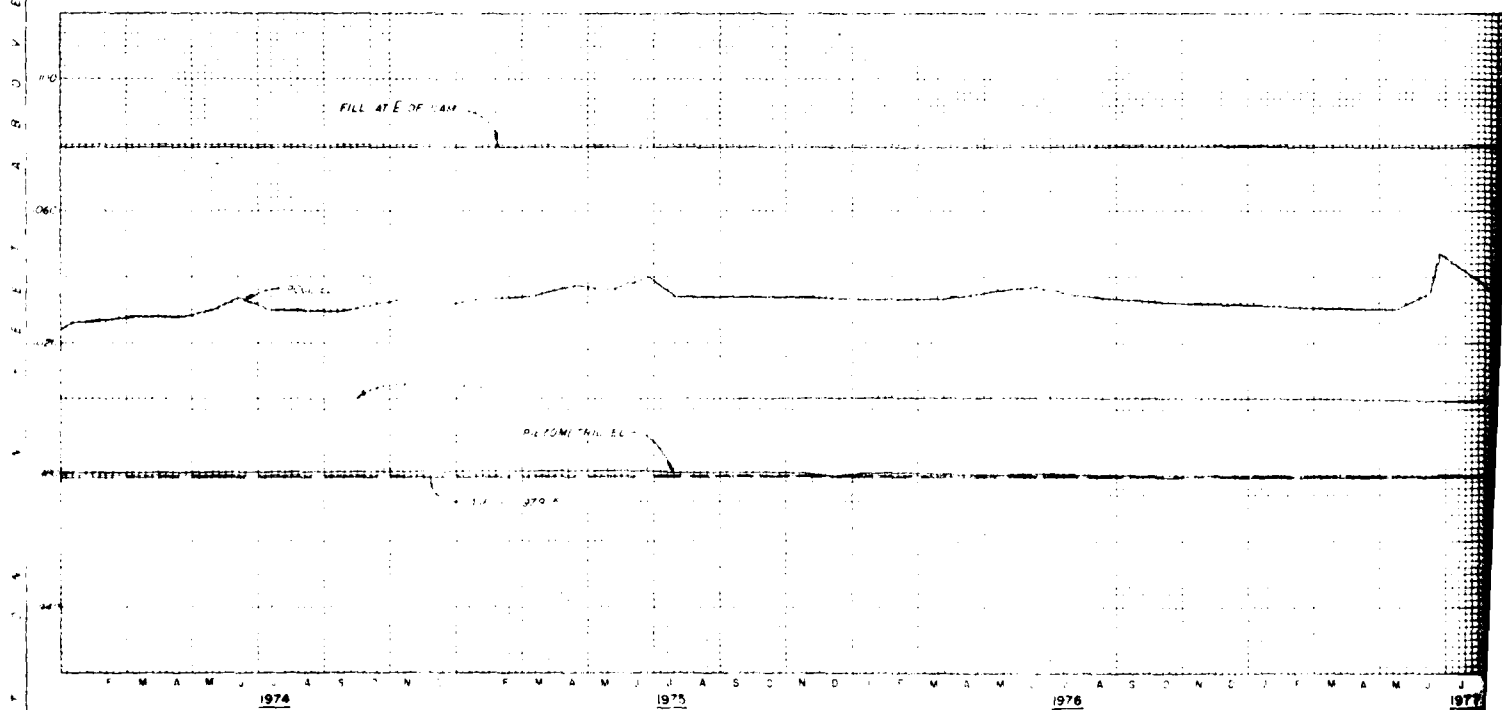
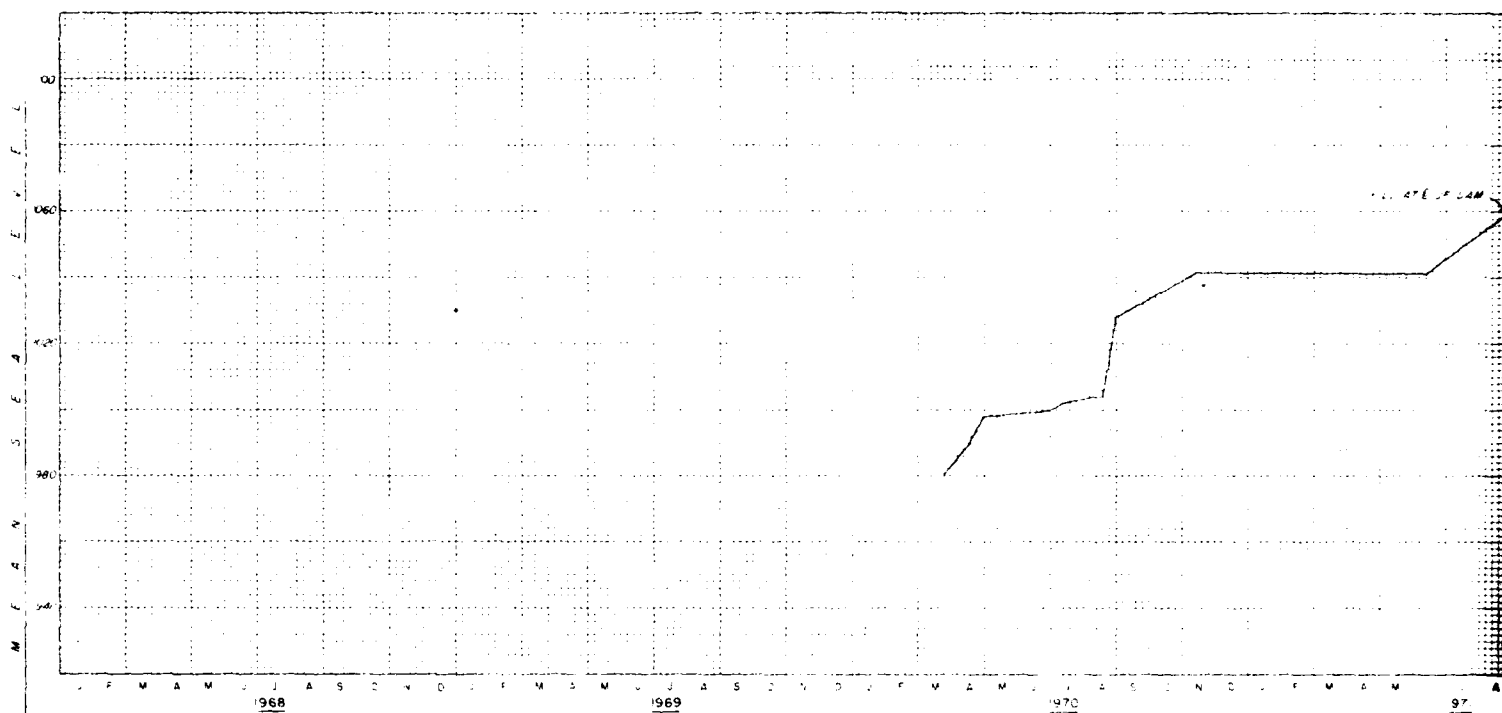
Revised August 1979
MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
PP-72-6 (OPEN TUBE)

In 1 sheet

Sheet No. 1
CORPS OF ENGINEERS U.S. ARMY
KANSAS CITY DISTRICT
FILE NO 0-5-1306
AUGUST 1975

Scale as shown



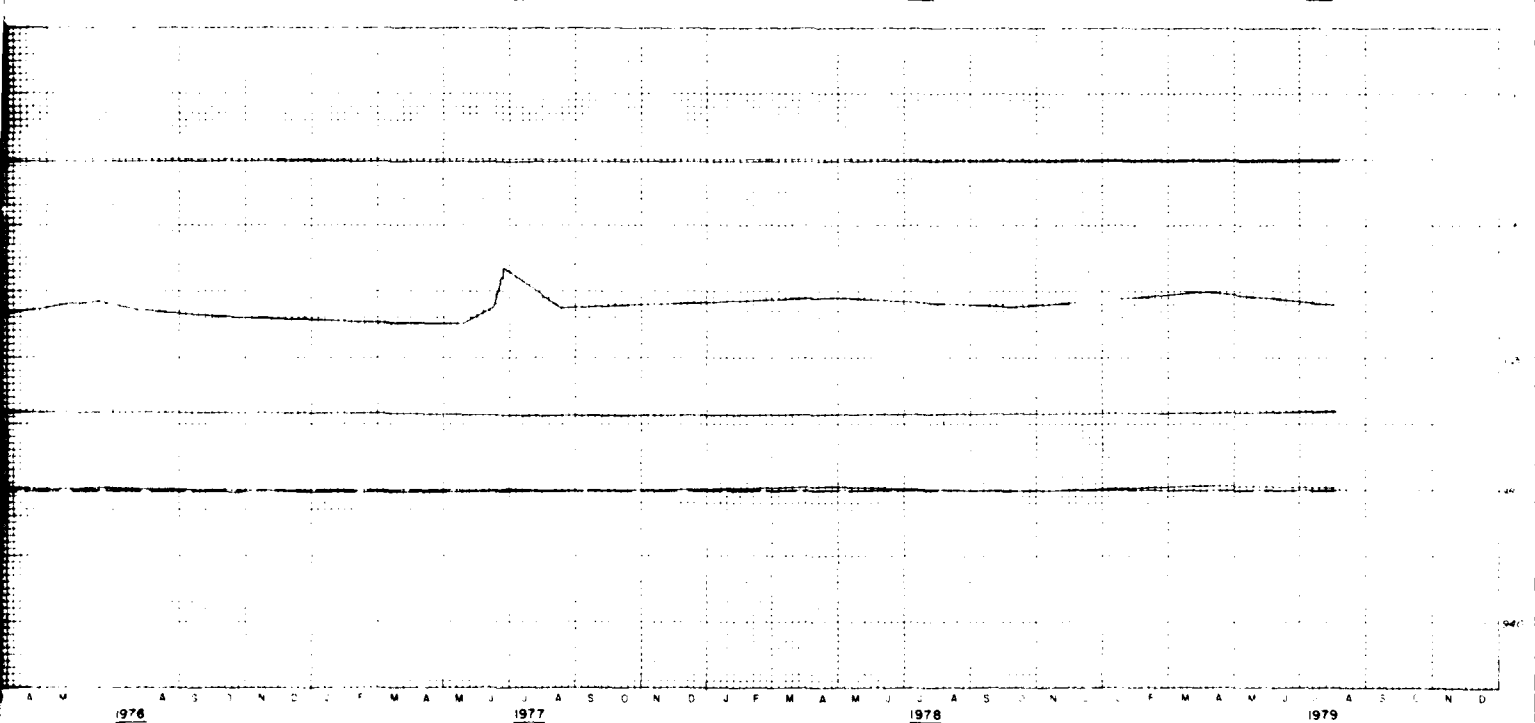
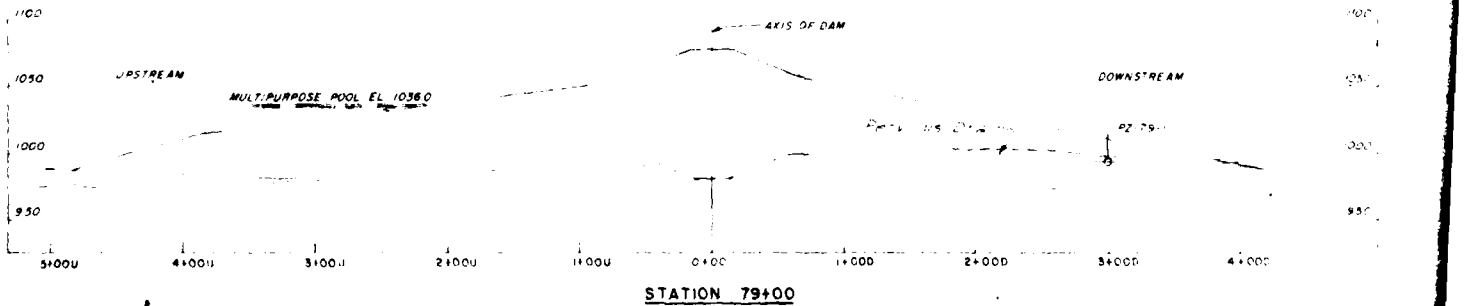
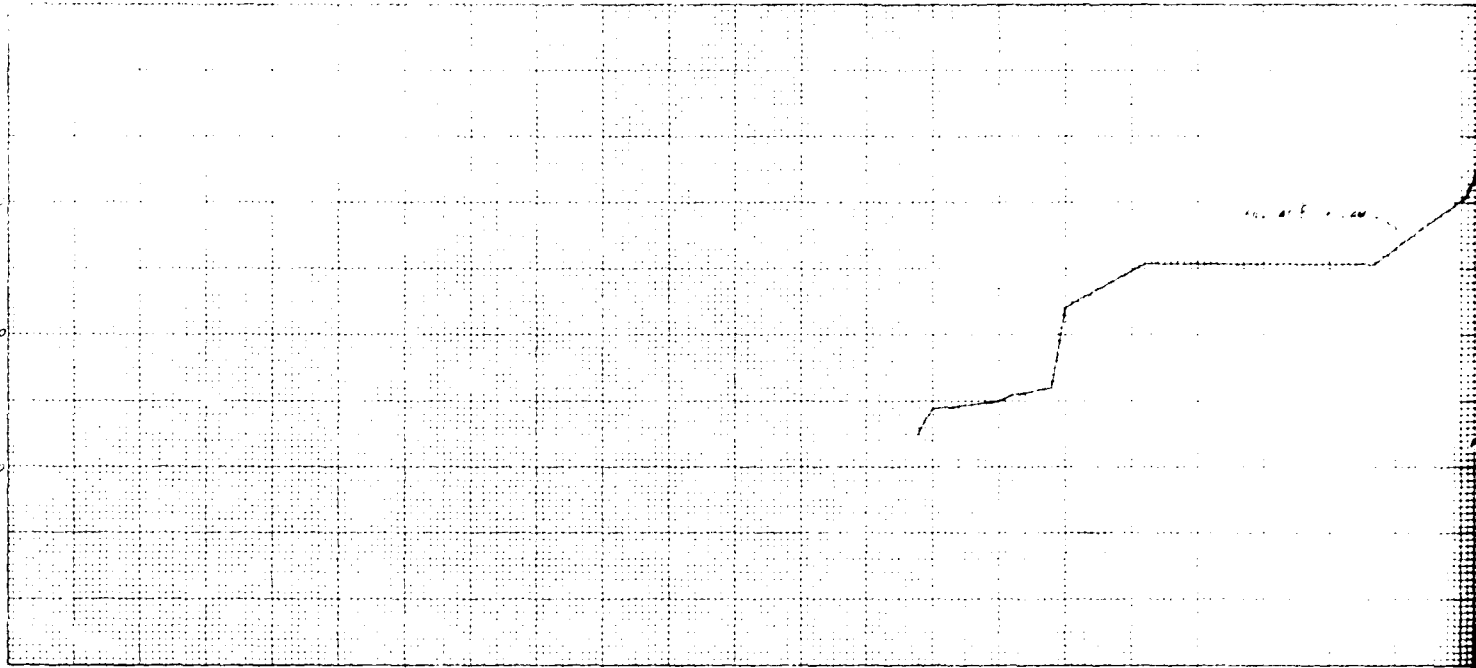
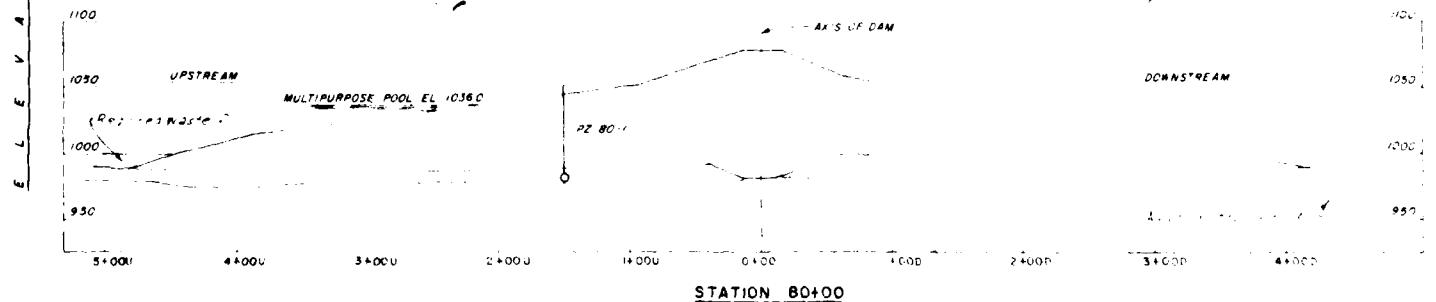
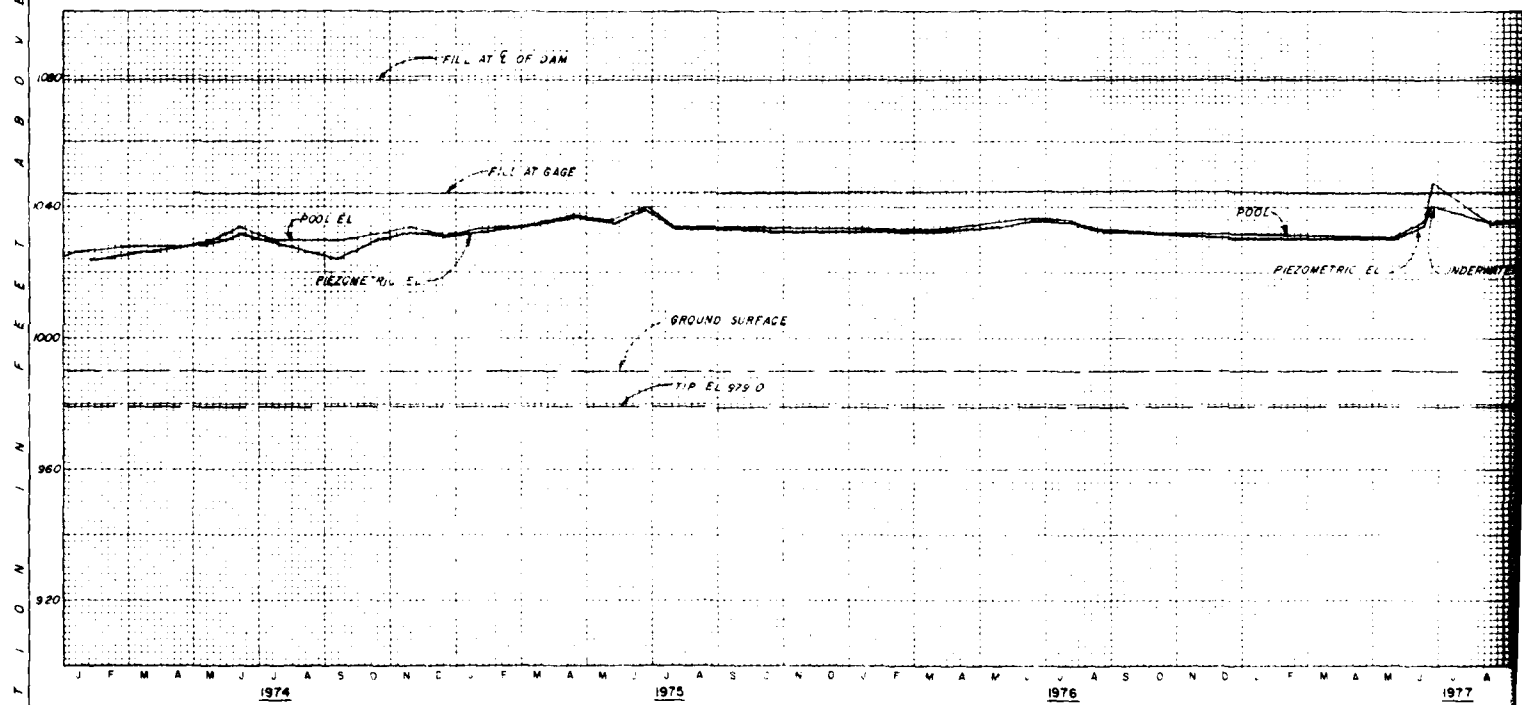
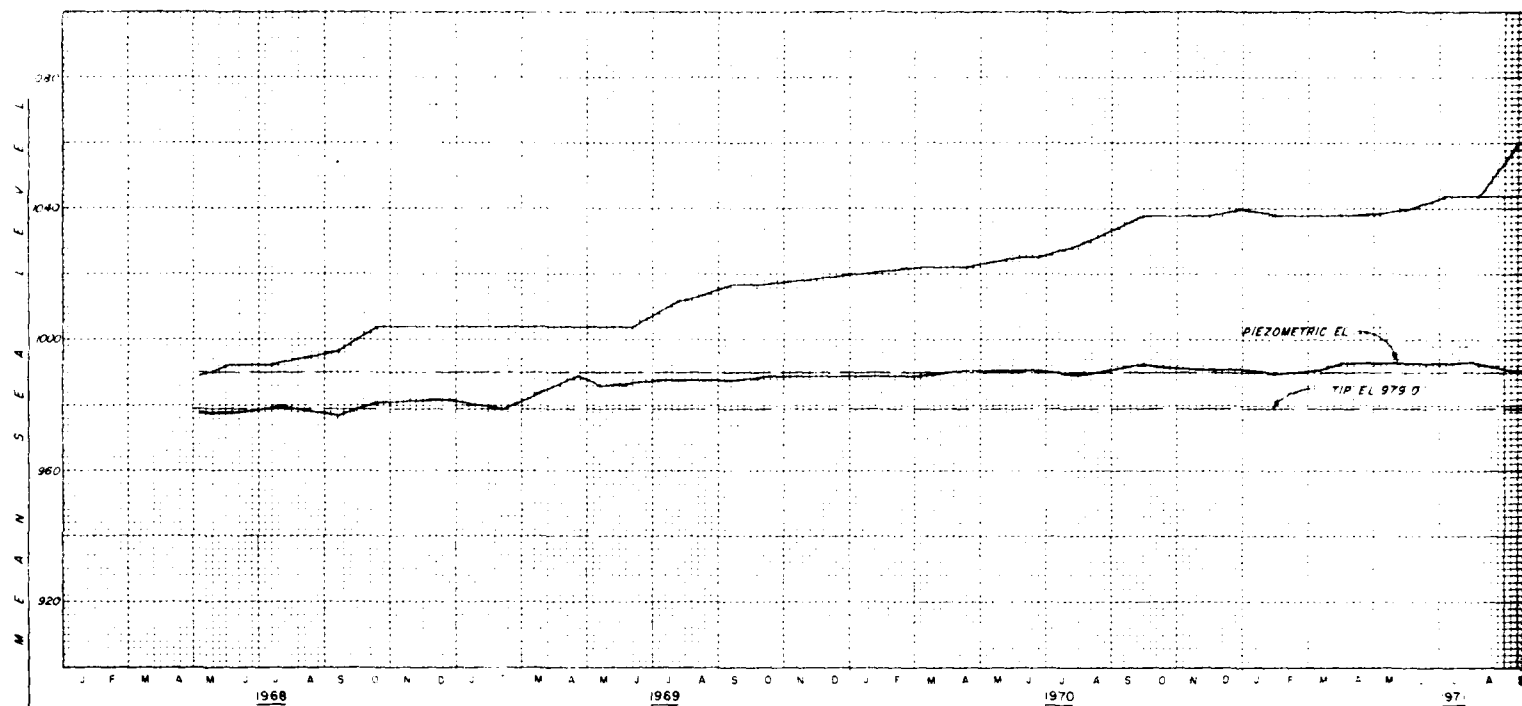
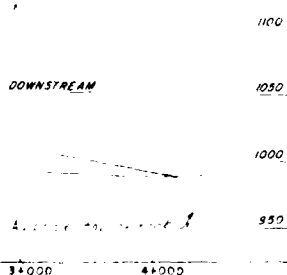
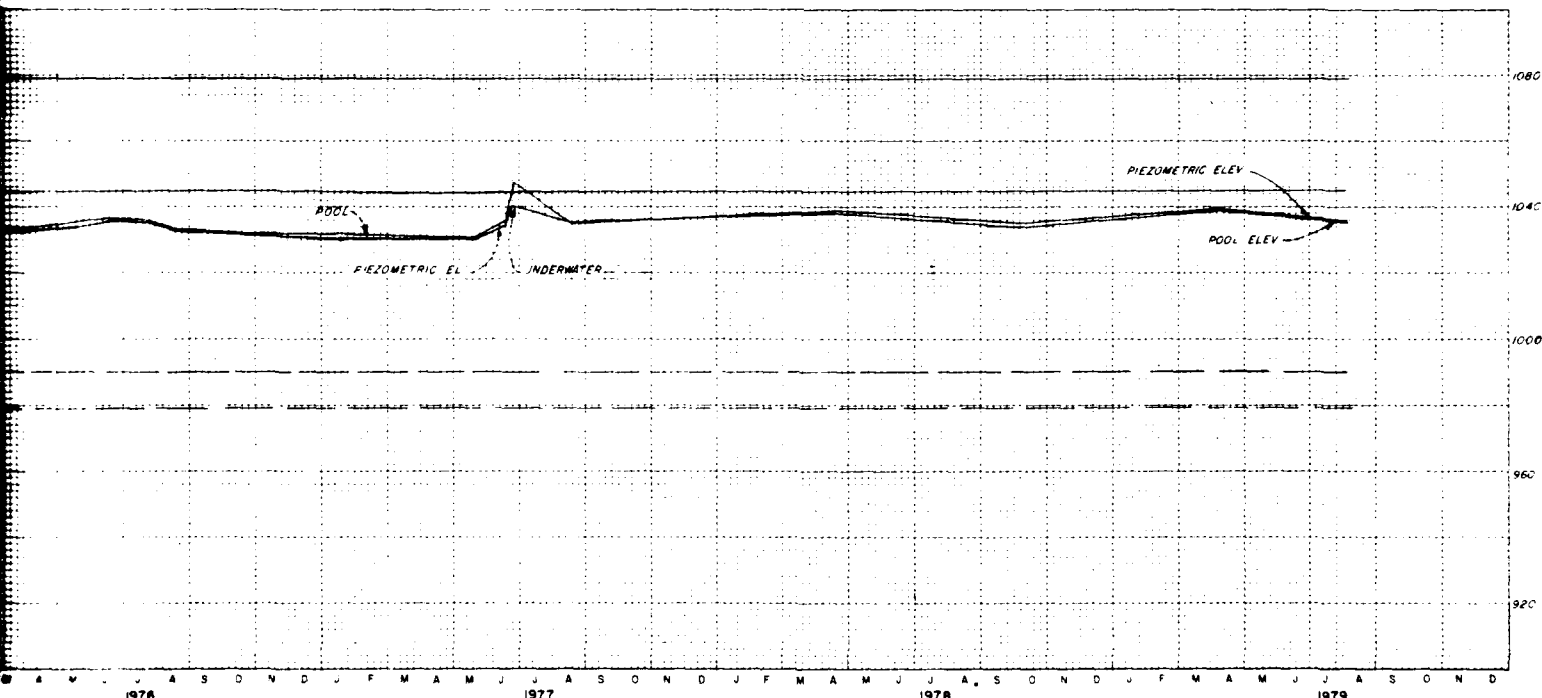
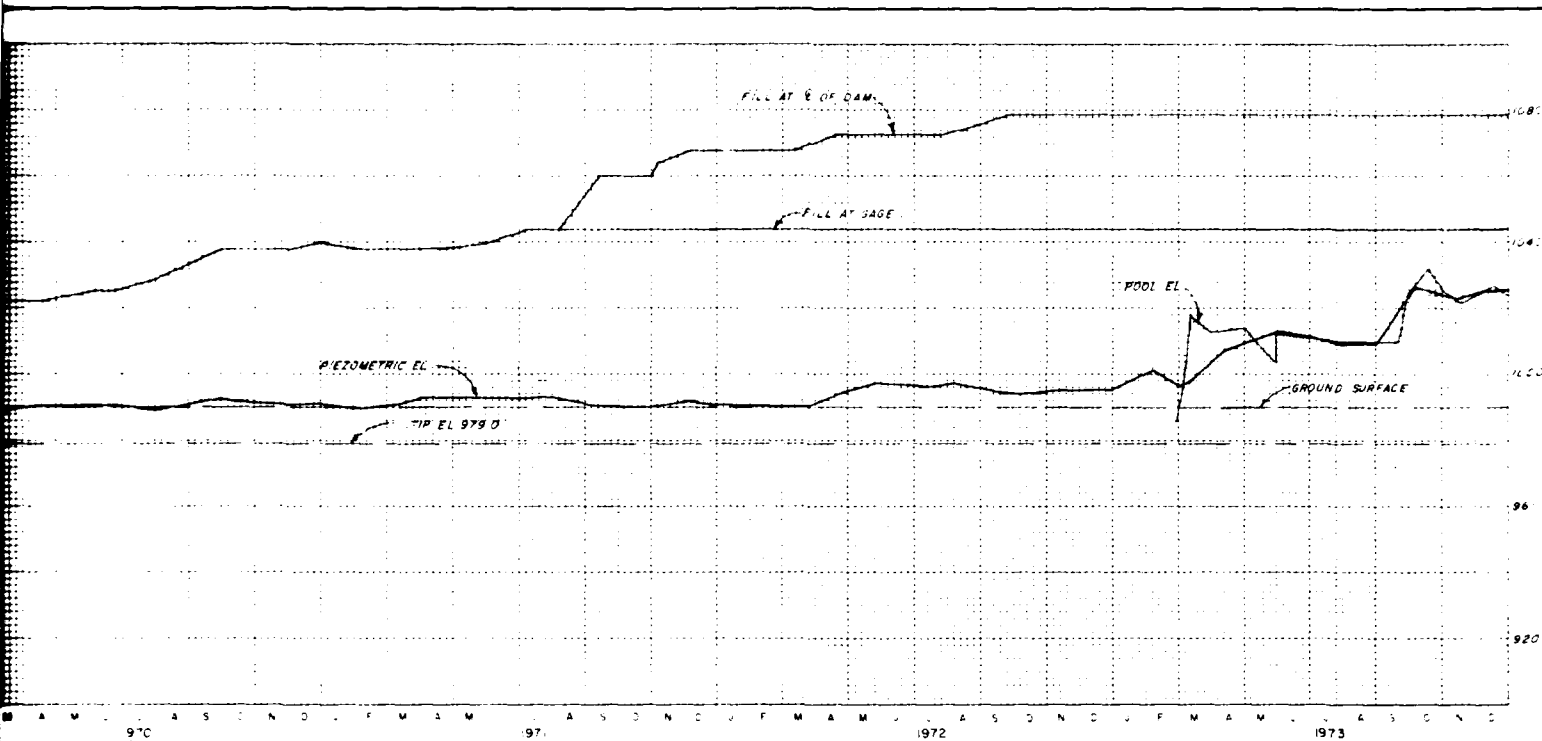


PLATE NO 59

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LEGEND
 OPEN TUBE O
 PNEUMATIC CELL ●

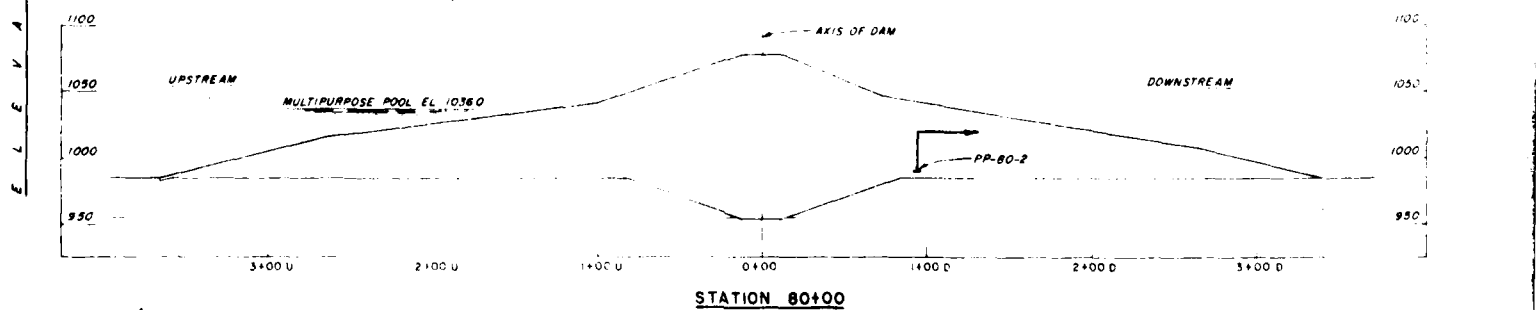
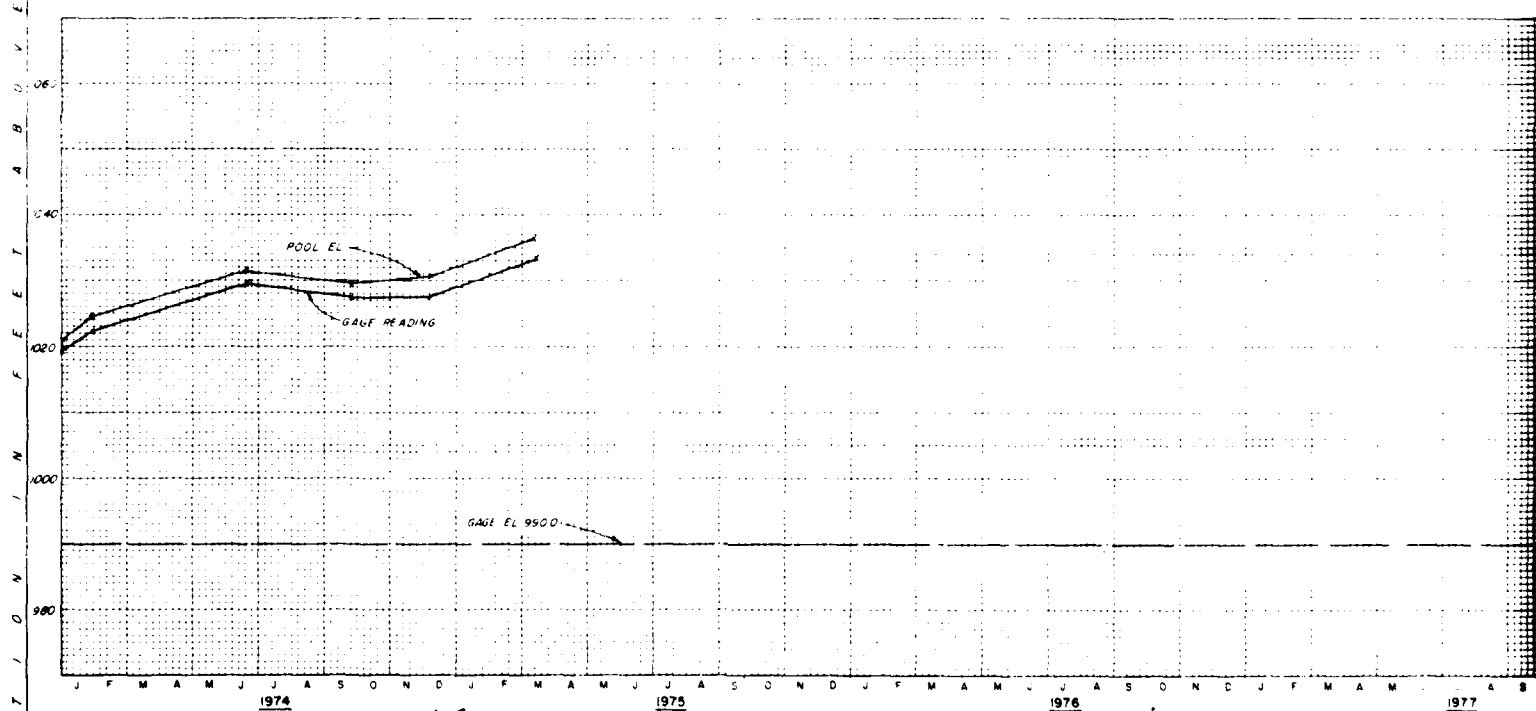
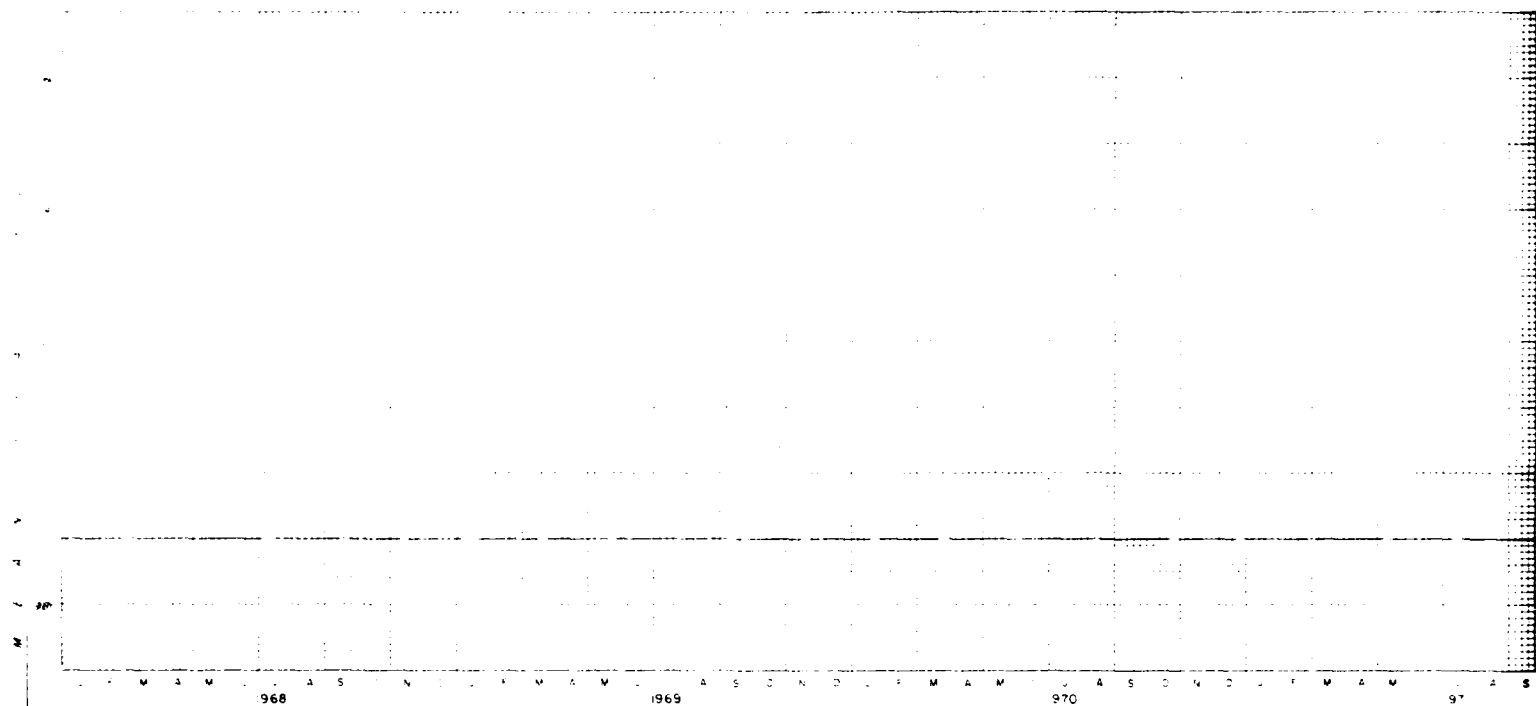
Revised August 5-75
 MARAIS DES CYGNES RIVER KANSAS
MELVERN LAKE

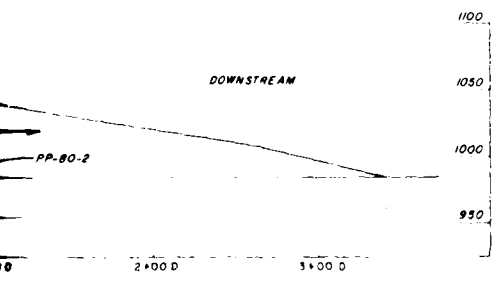
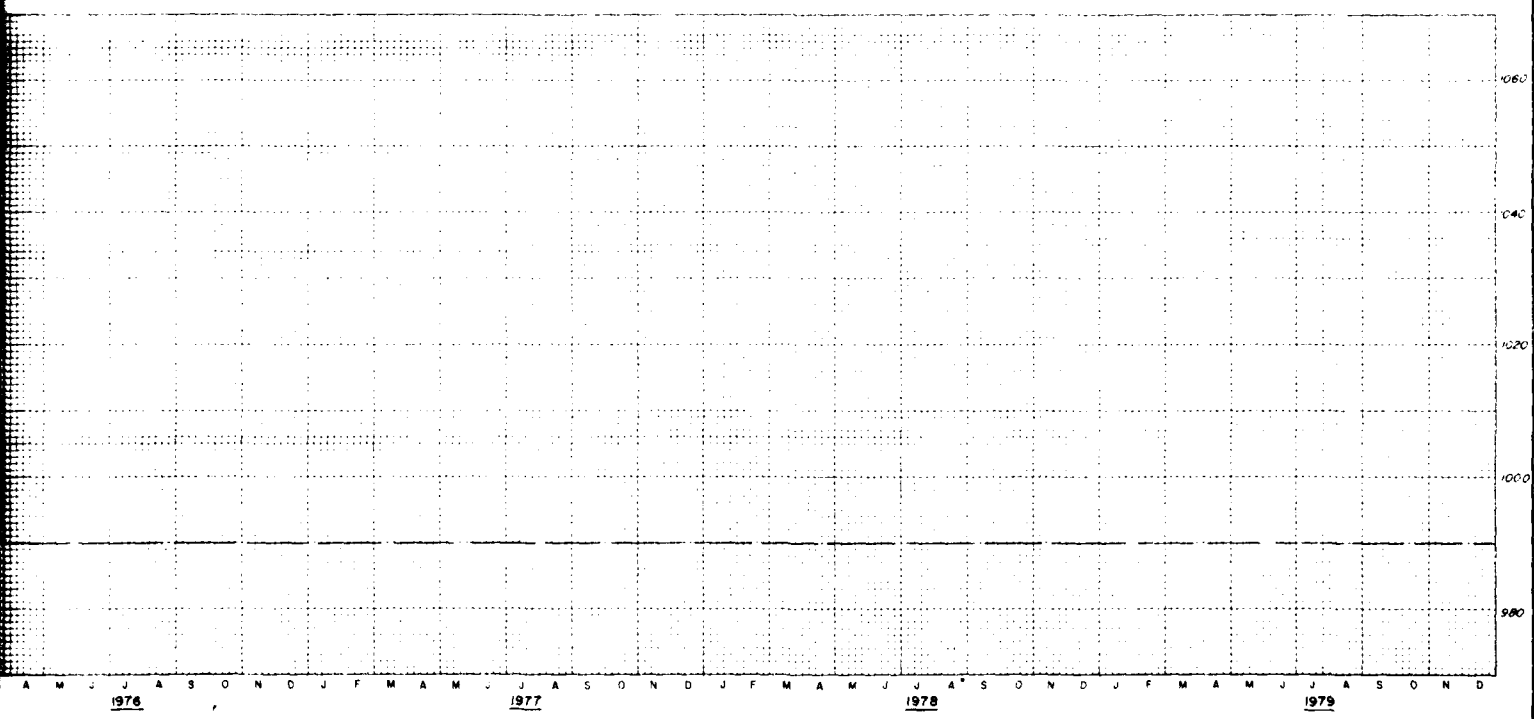
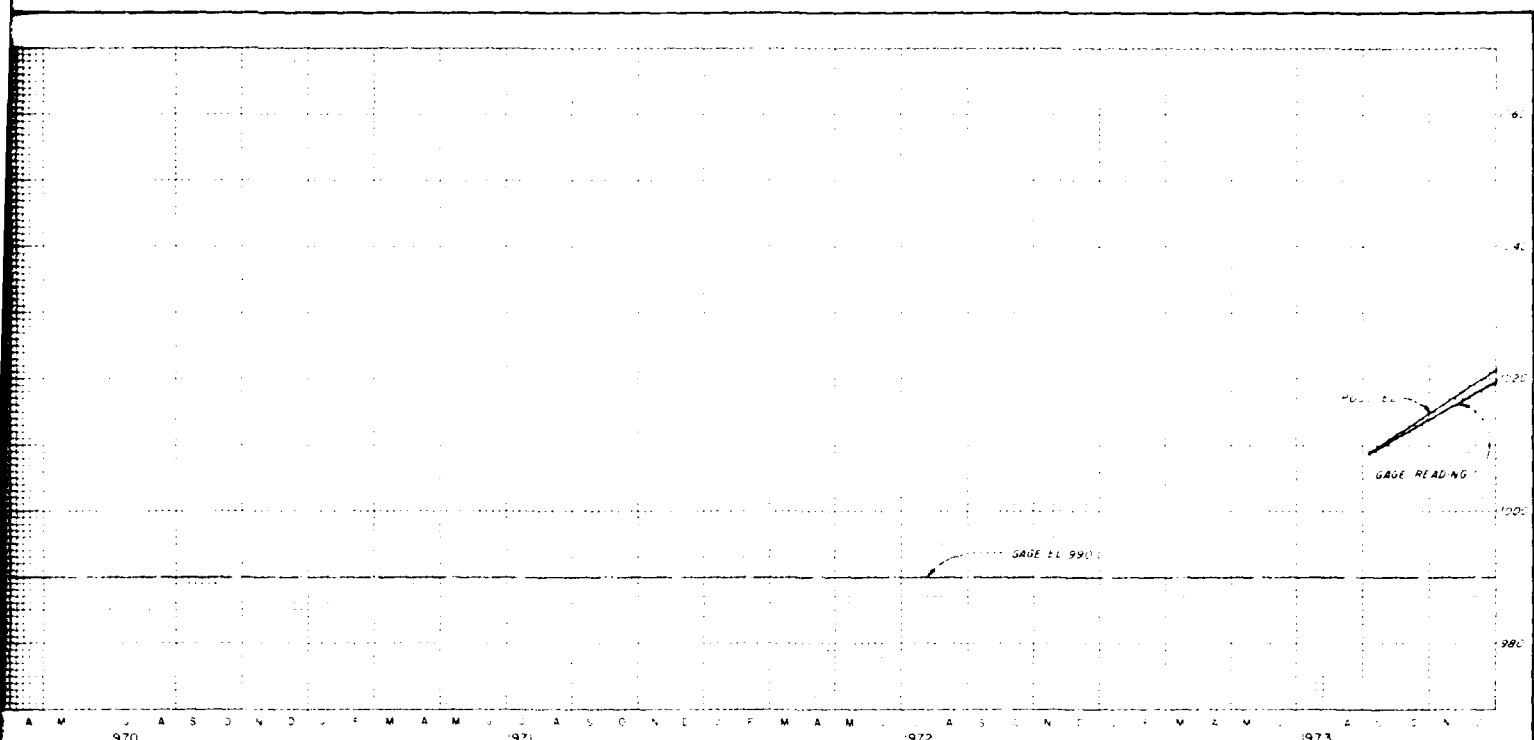
INSTRUMENTATION PLOTS
 PZ 80-1 (OPEN TUBE)

In 1 sheet

Scale as shown

Sheet No. 1
 CORPUS OF ENGINEERS U.S. ARMY
 KANSAS CITY DISTRICT
FILE NO. 0-5-1309
 AUGUST 1975





NOTE
45-6 = GAGE ON THE 4" FLANGE
AT MONITOR BOX

Revised August 1979
MARAIS DES CYGNES RIVER KANSAS
MELVERN LAKE

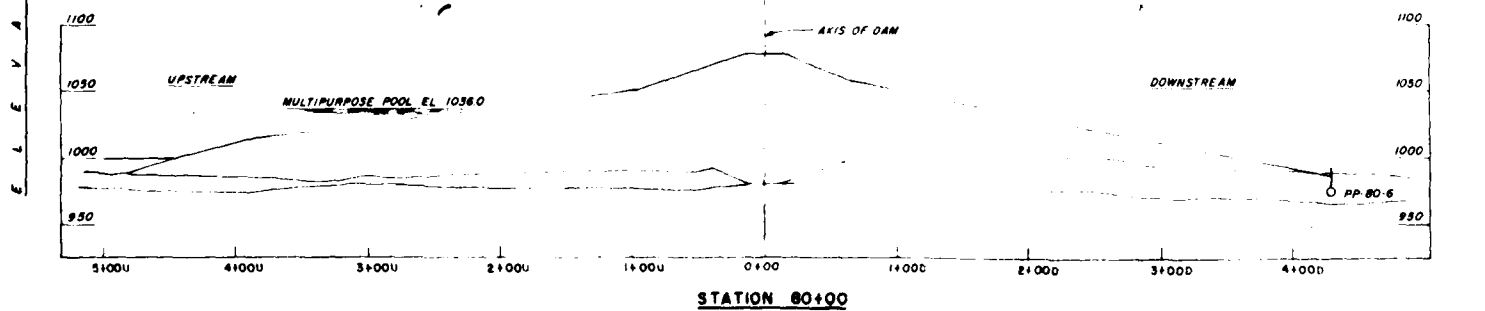
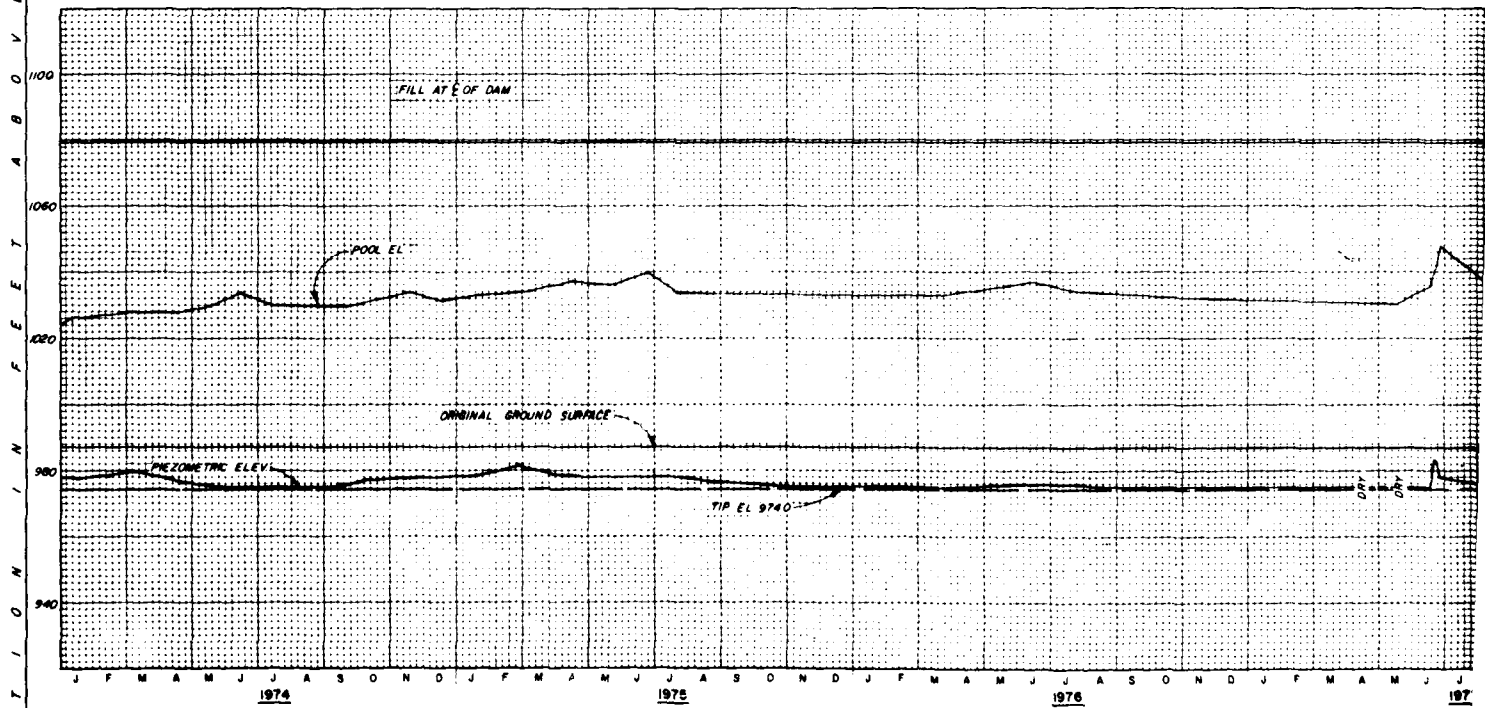
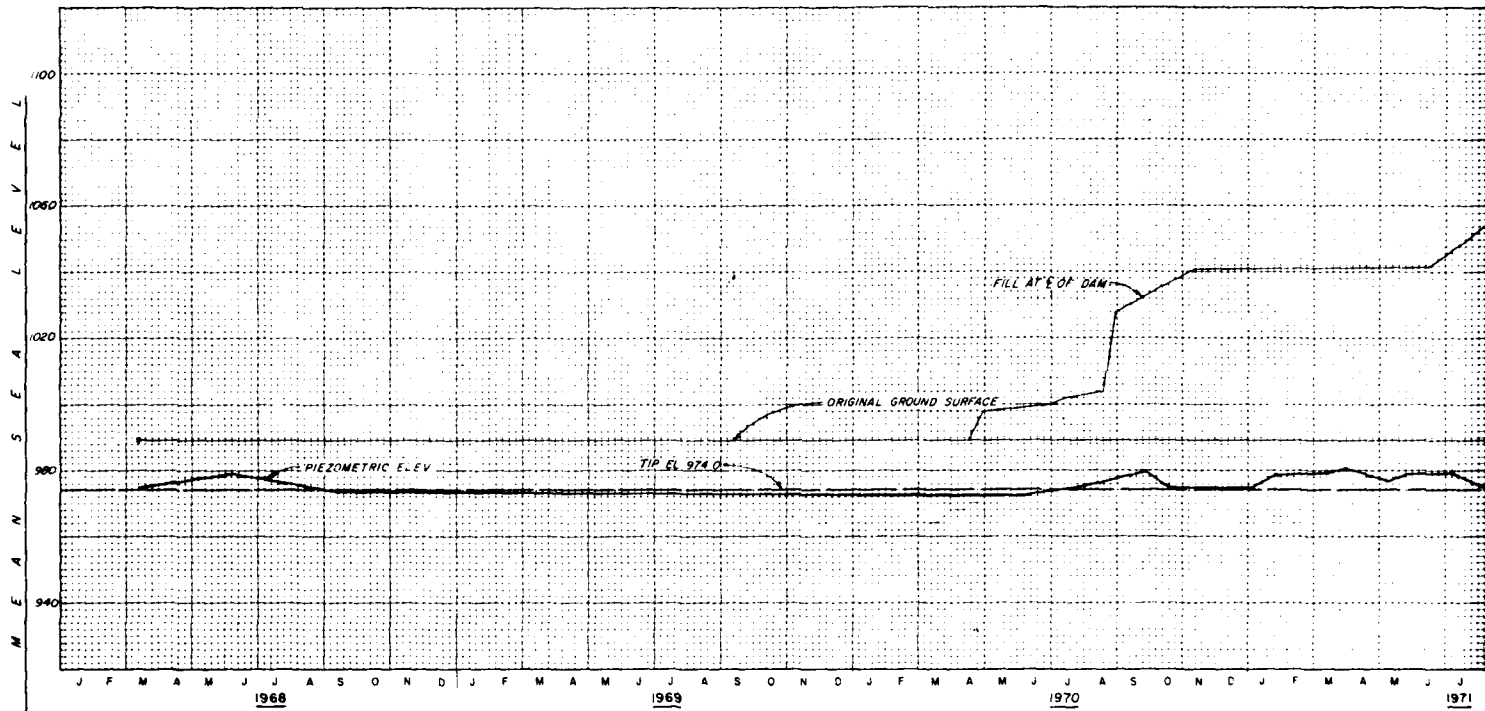
INSTRUMENTATION PLOTS
PP-80-2 (INSIDE TOWER)

In 1 sheet

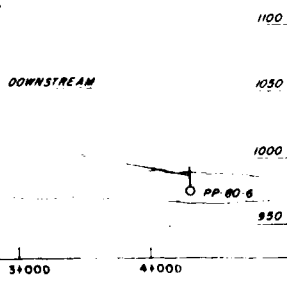
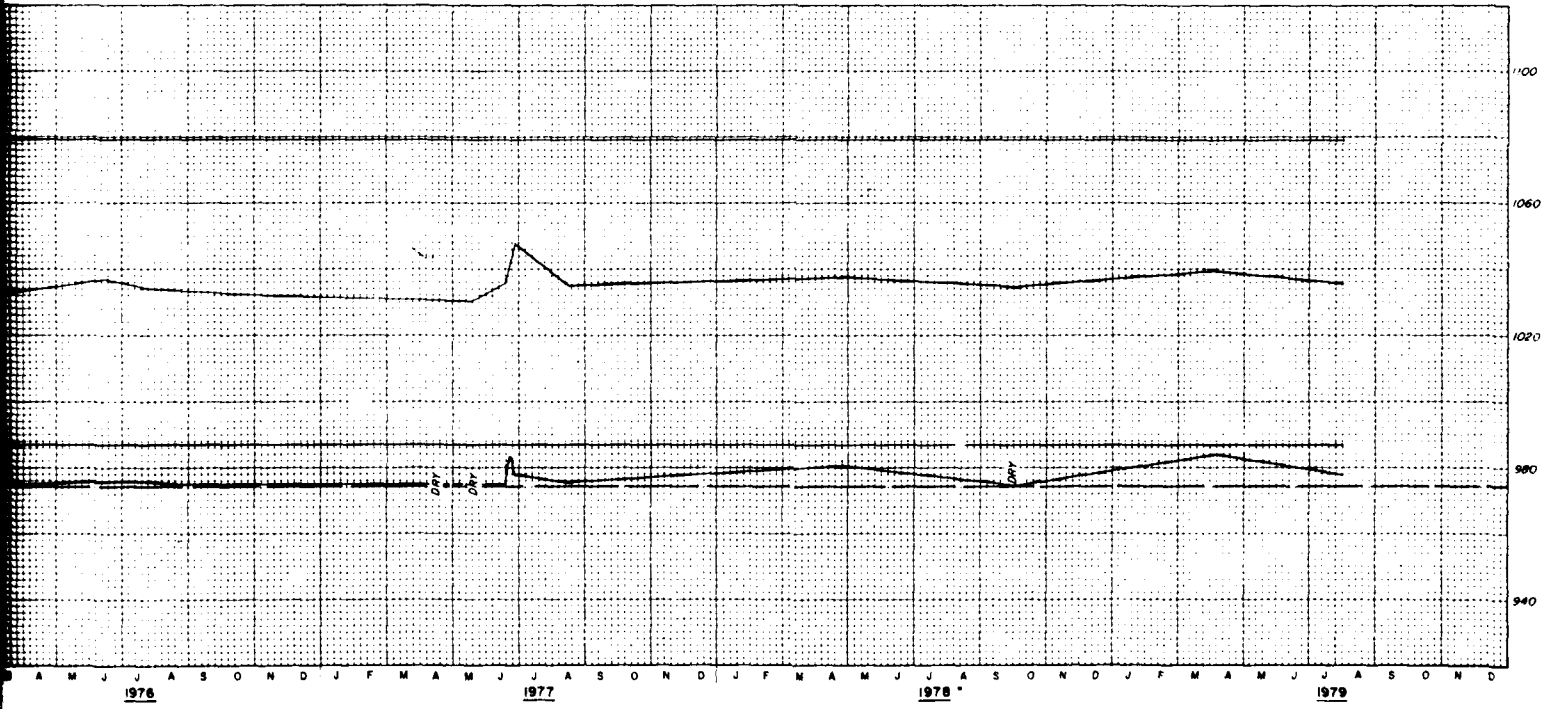
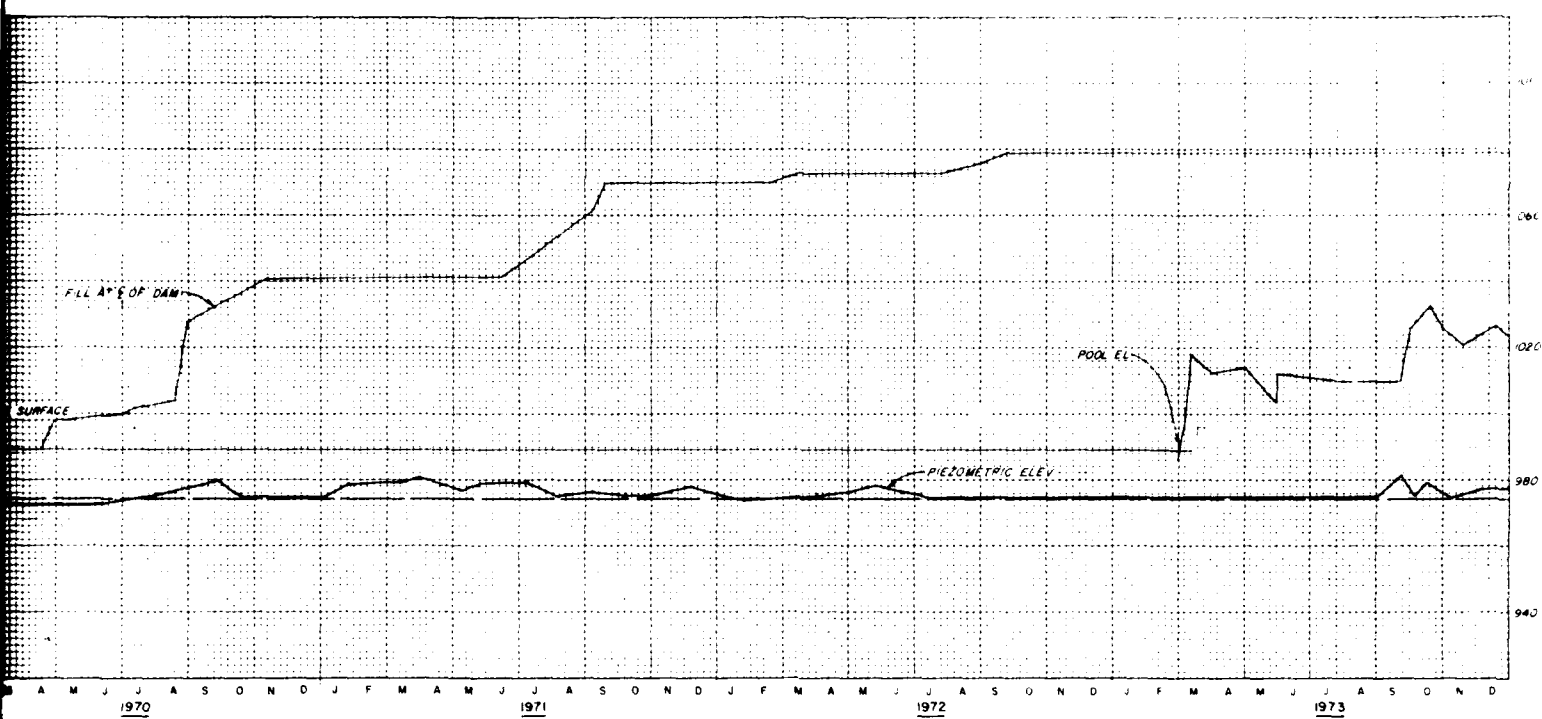
Sheet No. 1

Scale as shown

CORPS OF ENGINEERS U. S. ARMY
KANSAS CITY DISTRICT
FILE NO. 0-5-1310
AUGUST 1975



STATION 80+00



LEGEND
 OPEN TUBE ——— ○
 PNEUMATIC CELL ——— ●

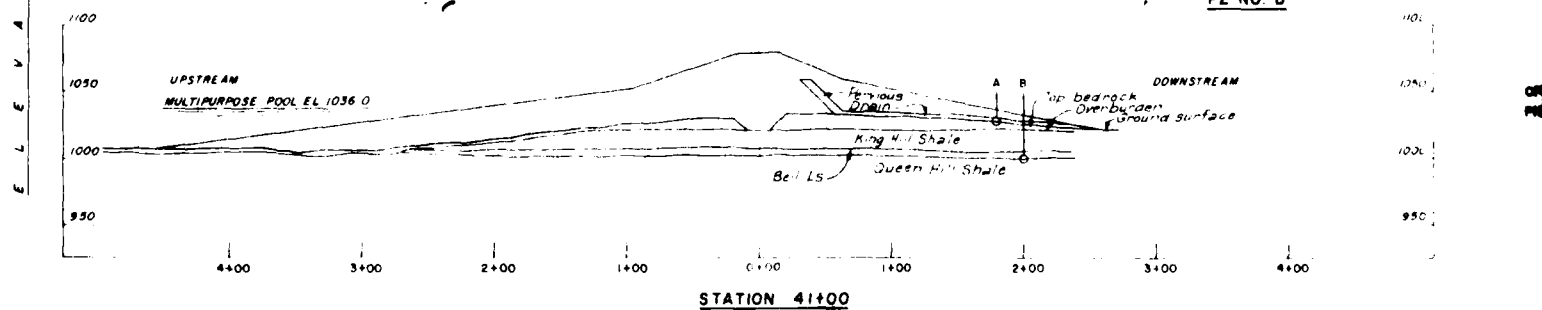
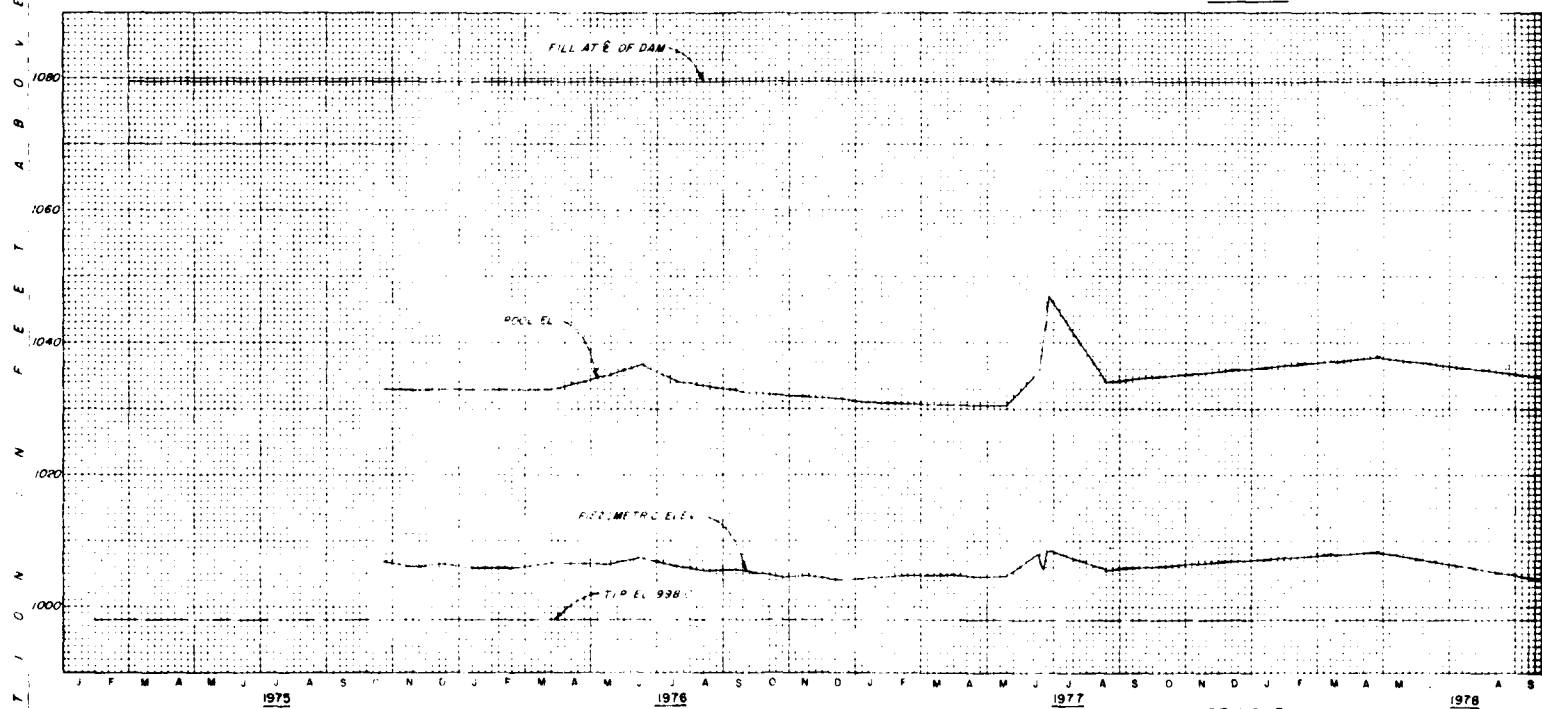
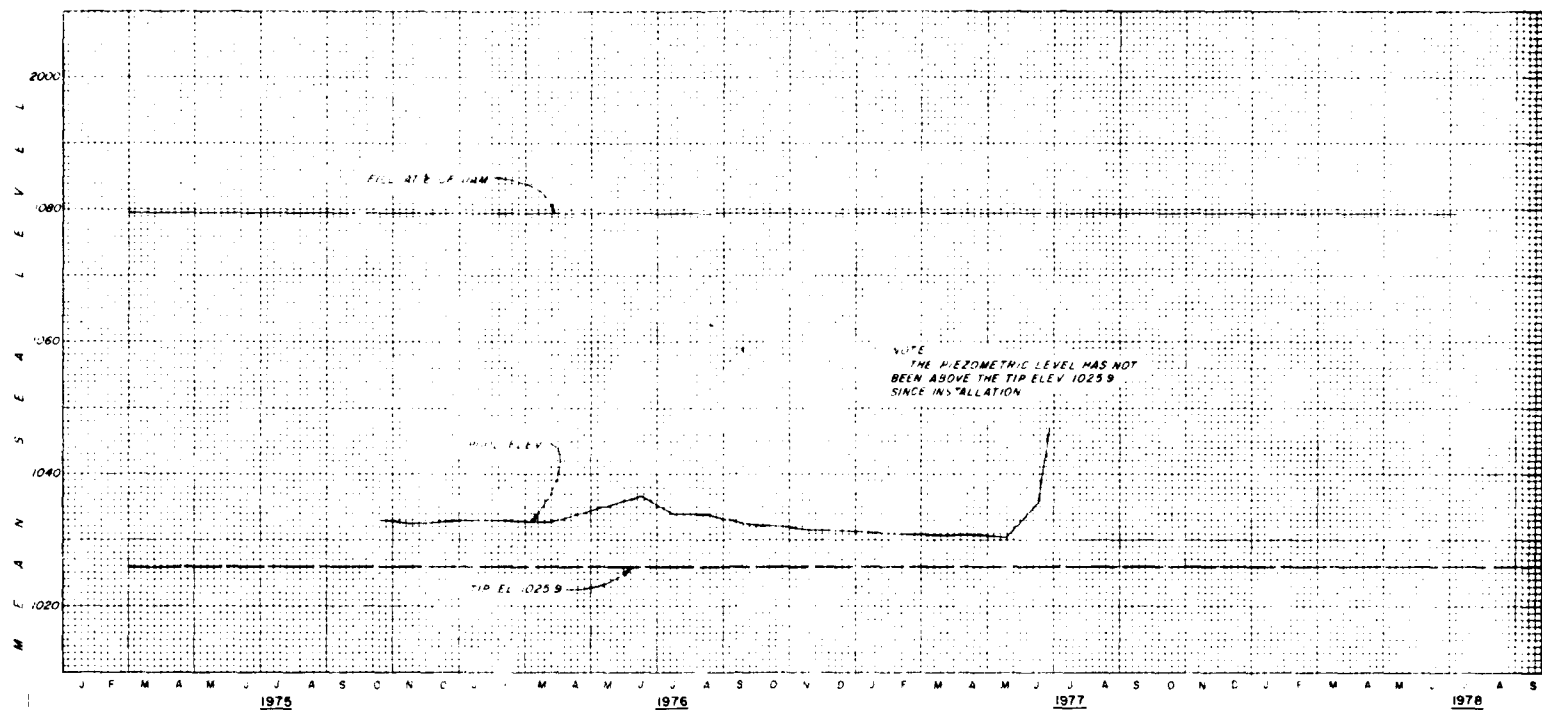
Revised August 1979
 MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

INSTRUMENTATION PLOTS
 PP-80-6 (OPEN TUBE)

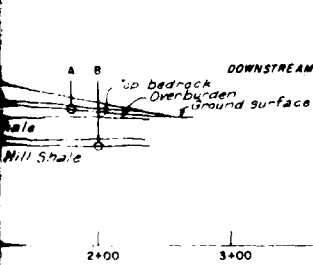
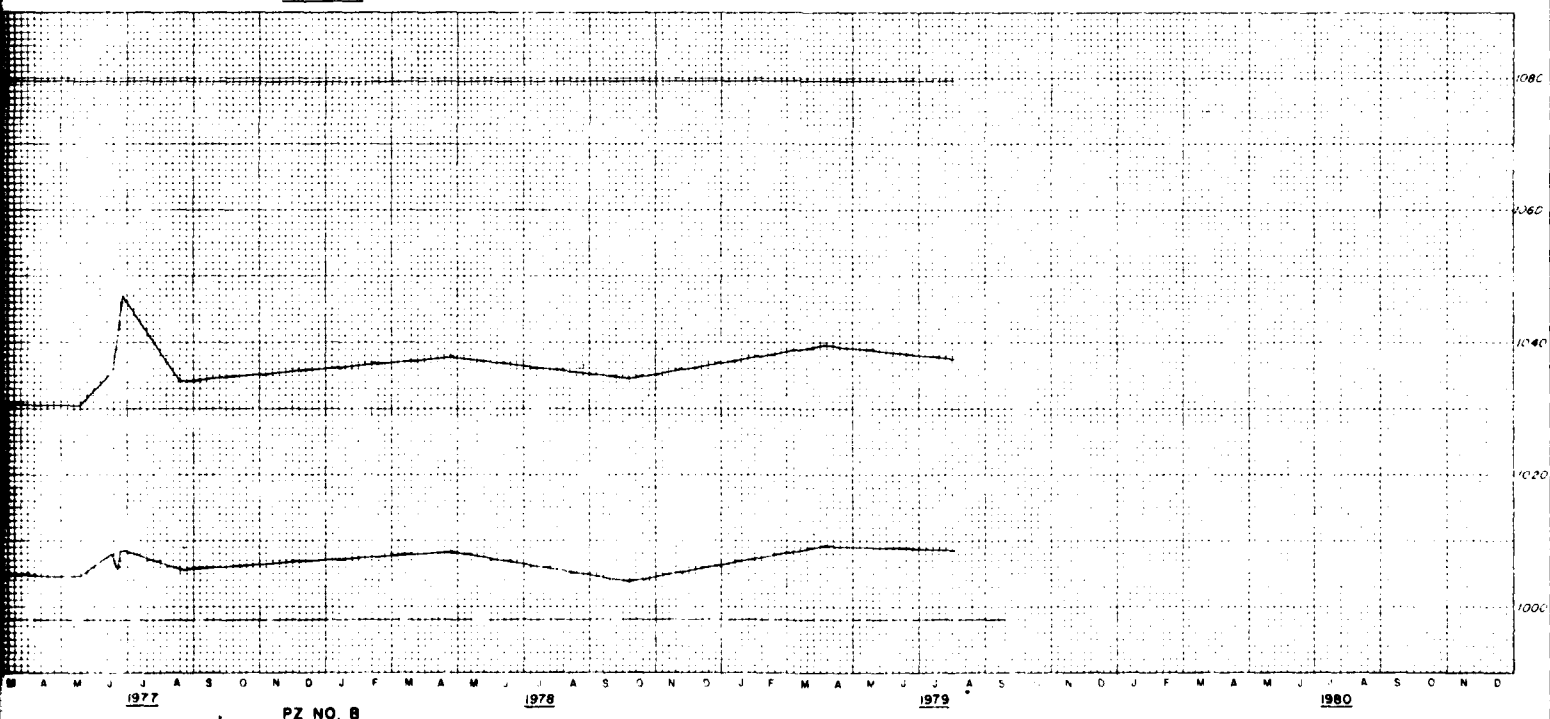
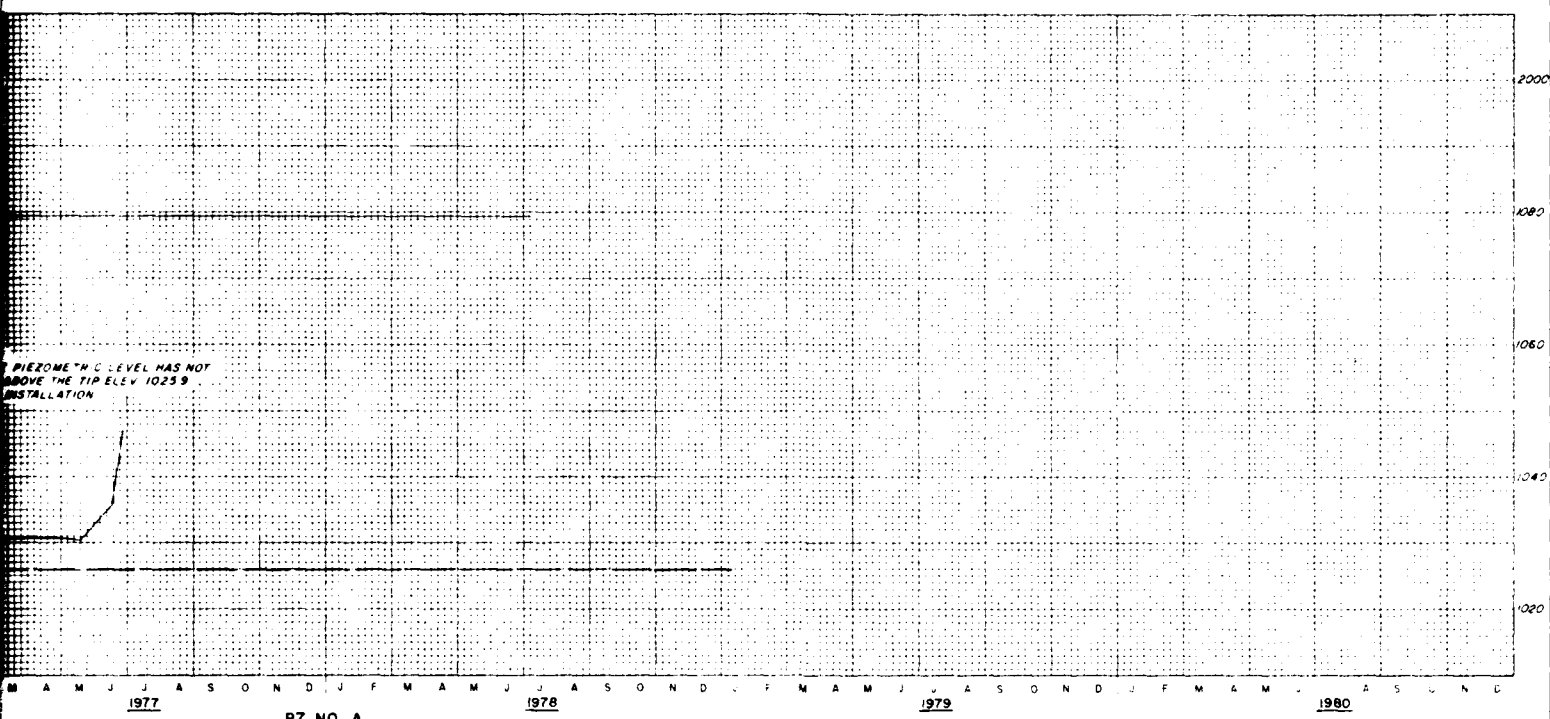
In 1 sheet

Sheet No 1
 CORPS OF ENGINEERS U.S. ARMY
 KANSAS CITY DISTRICT
FILE NO. 0-5-1311
 AUGUST 1975

Scale as shown



PIEZOMETER LEVEL HAS NOT
ABOVE THE TIP ELEV 1023.9
INSTALLATION



LEGEND
 OPEN TUBE — ○
 PNEUMATIC CELL — ●

Revised August 479
 MARAIS DES LYGNES RIVER KANSAS
MELVERN LAKE

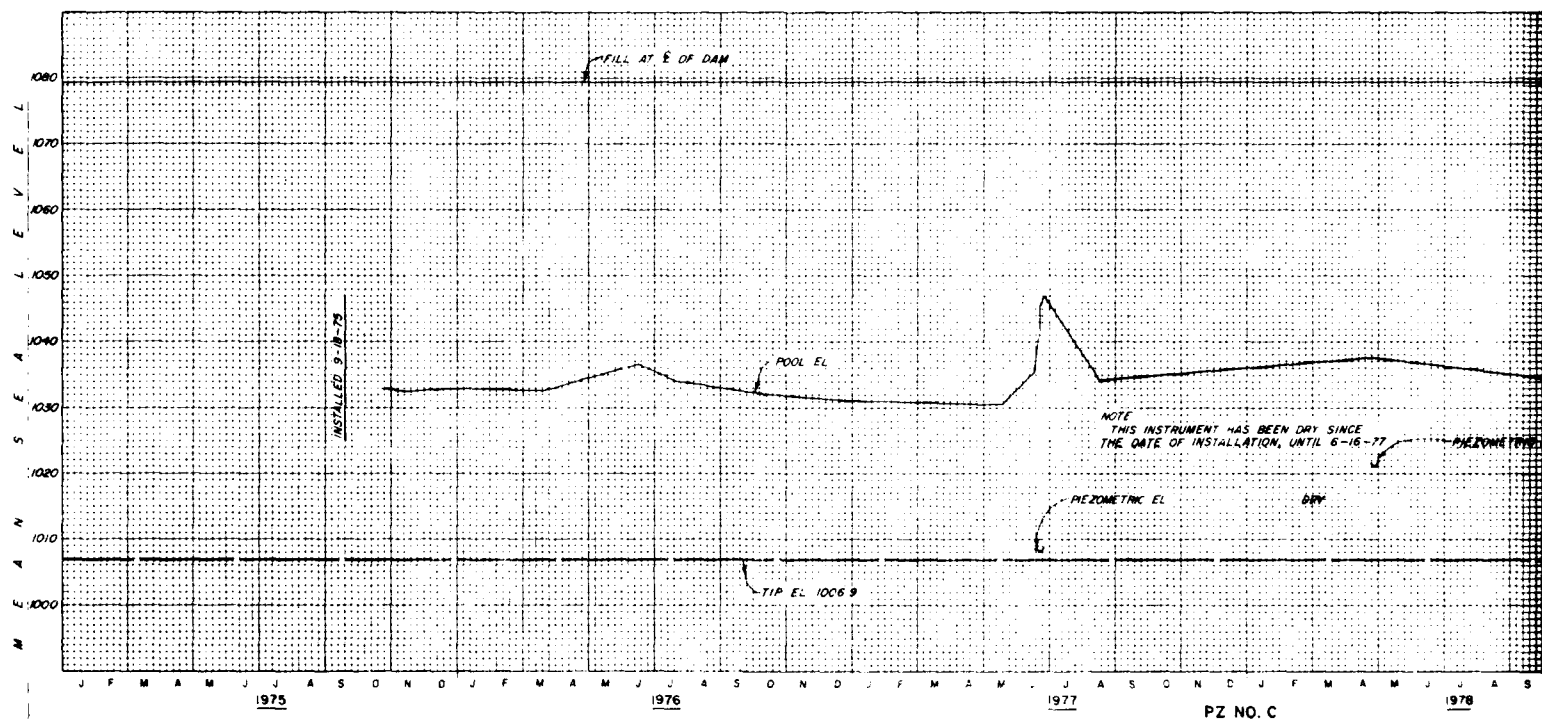
PIEZOMETER PLOTS
 PZ NO'S A & B

In 1 sheet

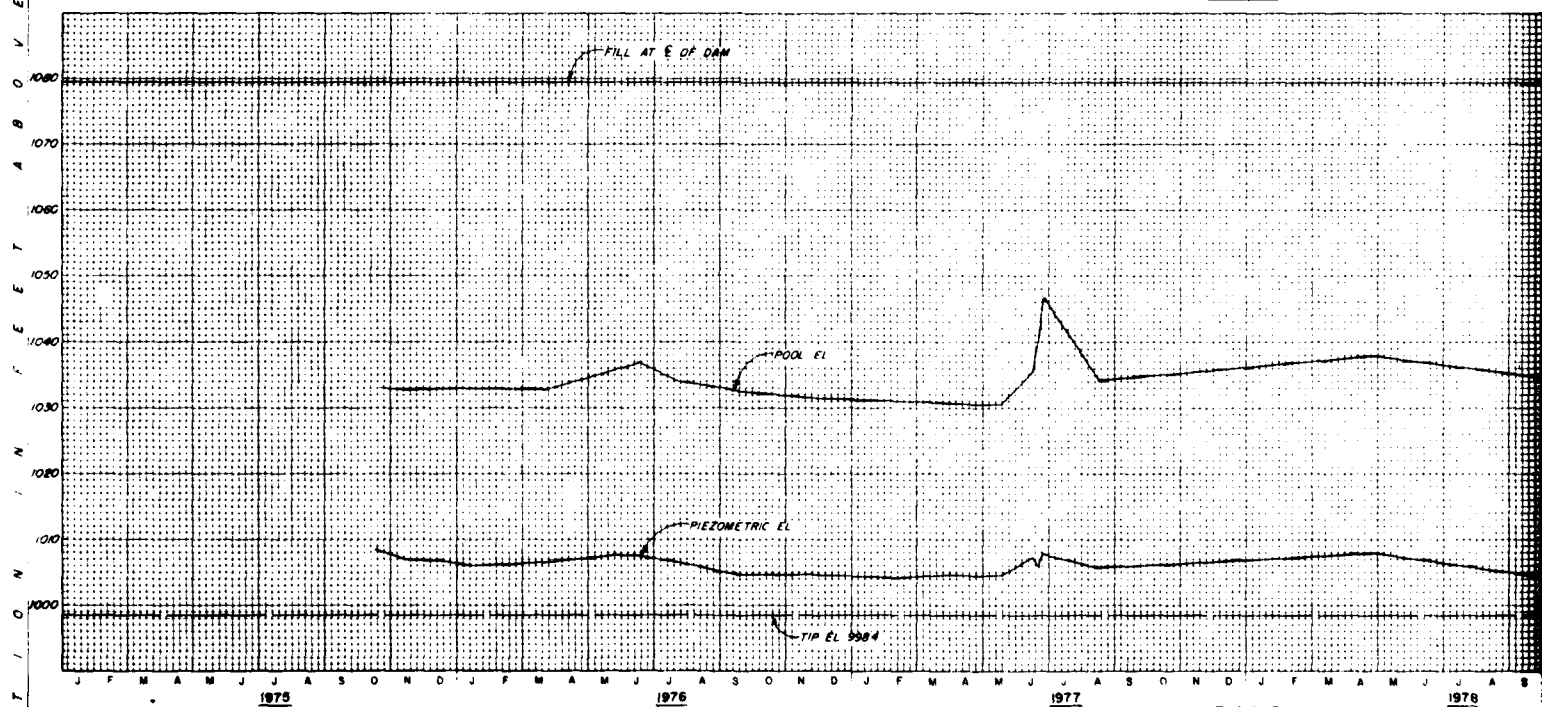
Sheet No. 1

Scale as shown

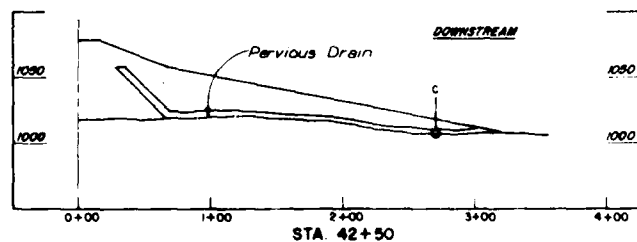
ENGINEERS U.S. ARMY
 KANSAS CITY DISTRICT
 FILE NO. 0-5-1007
 AUGUST 1977



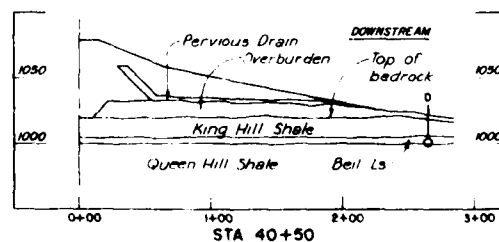
PZ NO. C



PZ NO. D

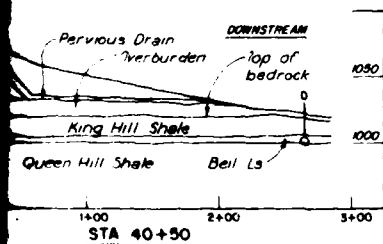
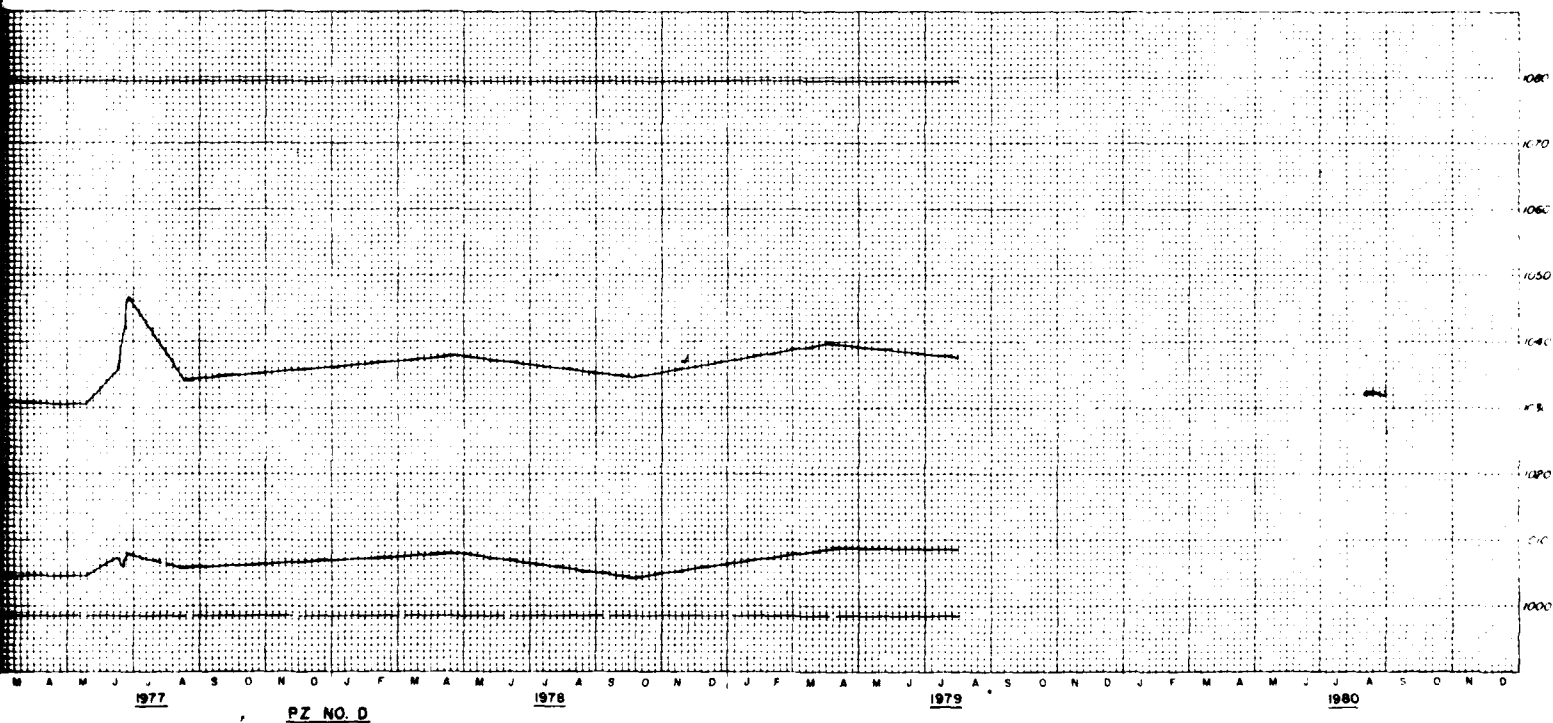
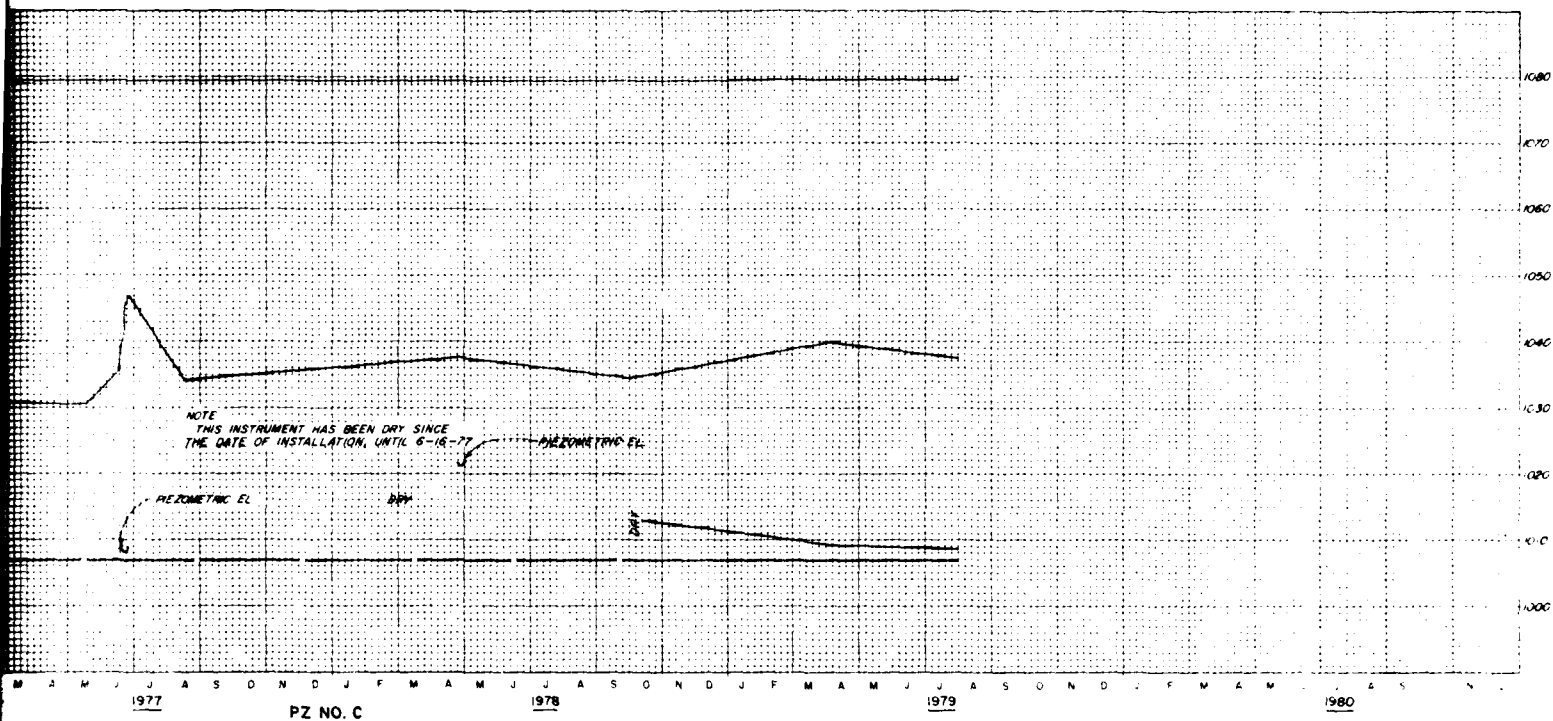


STA. 42+50



STA. 40+50

LEGEND
OPEN TUBE
PNEUMATIC CELL



LEGEND

OPEN TUBE
PNEUMATIC CELL

○
●

Revised August 1979
MARAIS DES CYGNES RIVER KANSAS
MELVERN LAKE

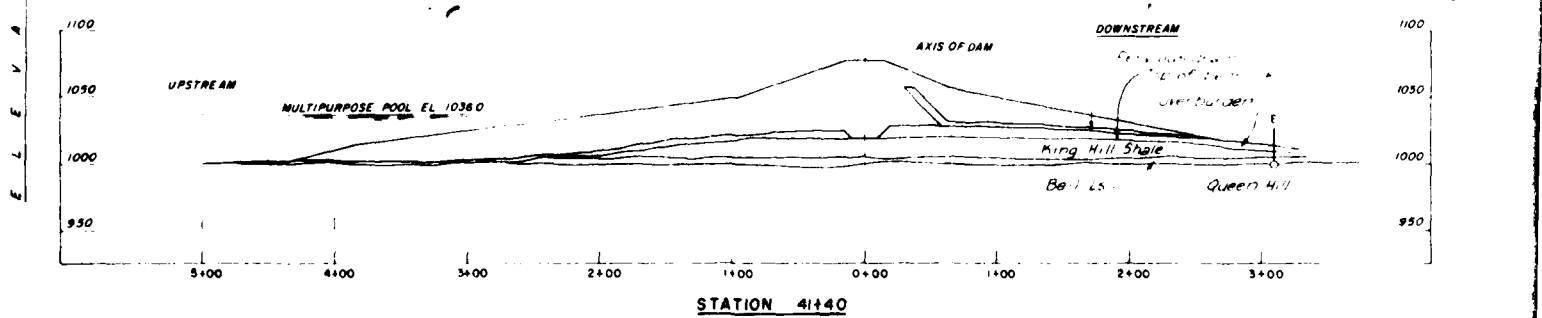
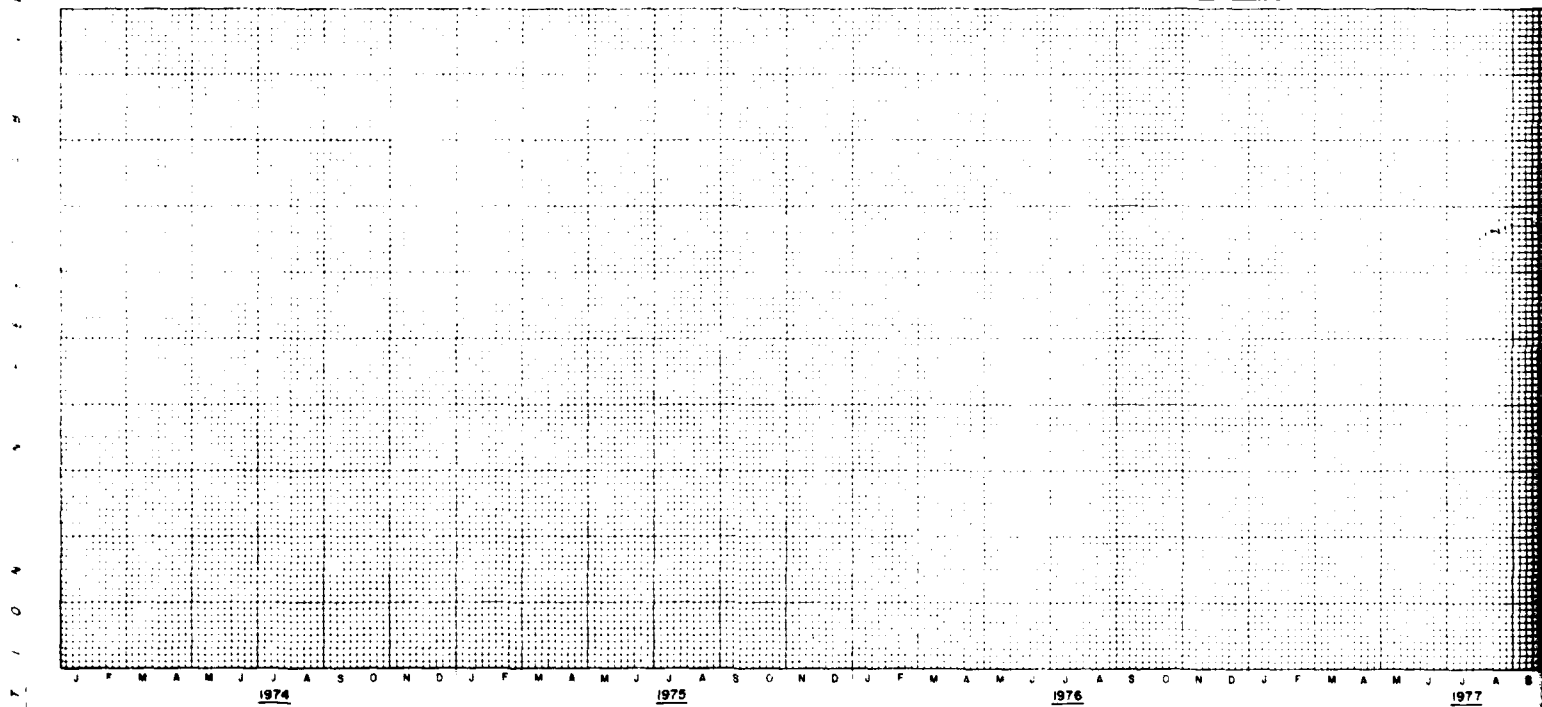
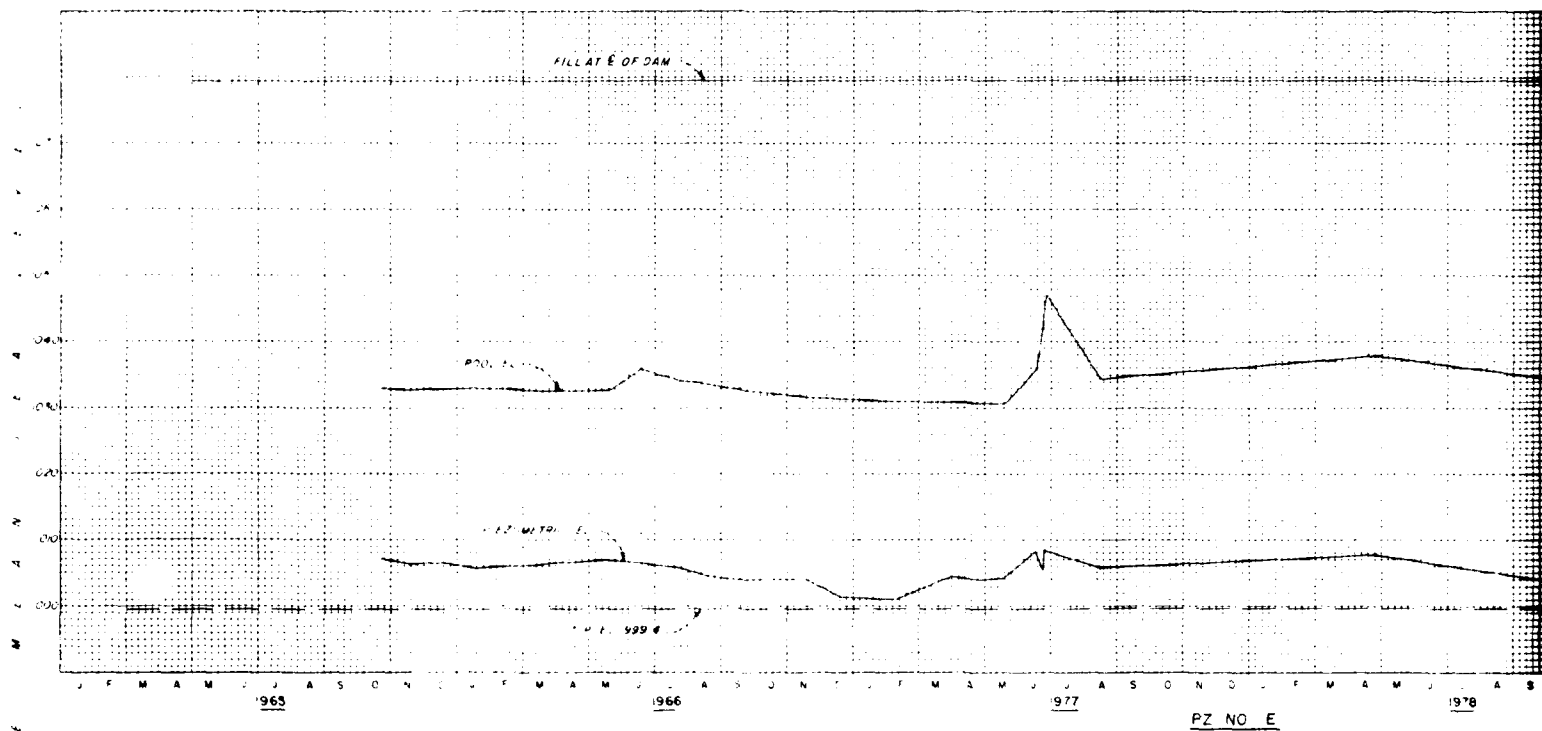
PIEZOMETER PLOTS
PZ NO'S C&D

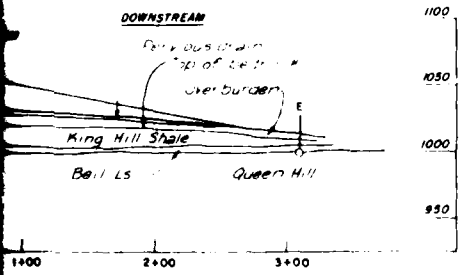
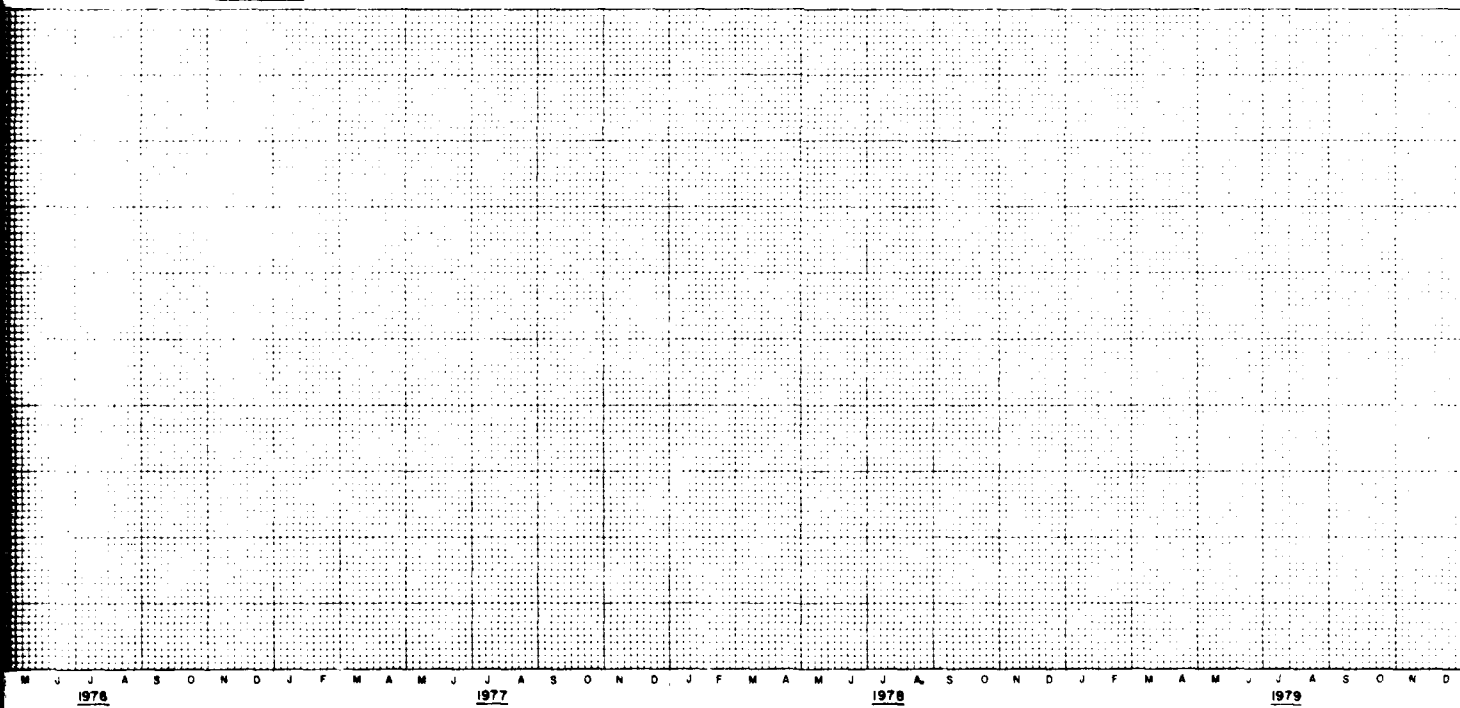
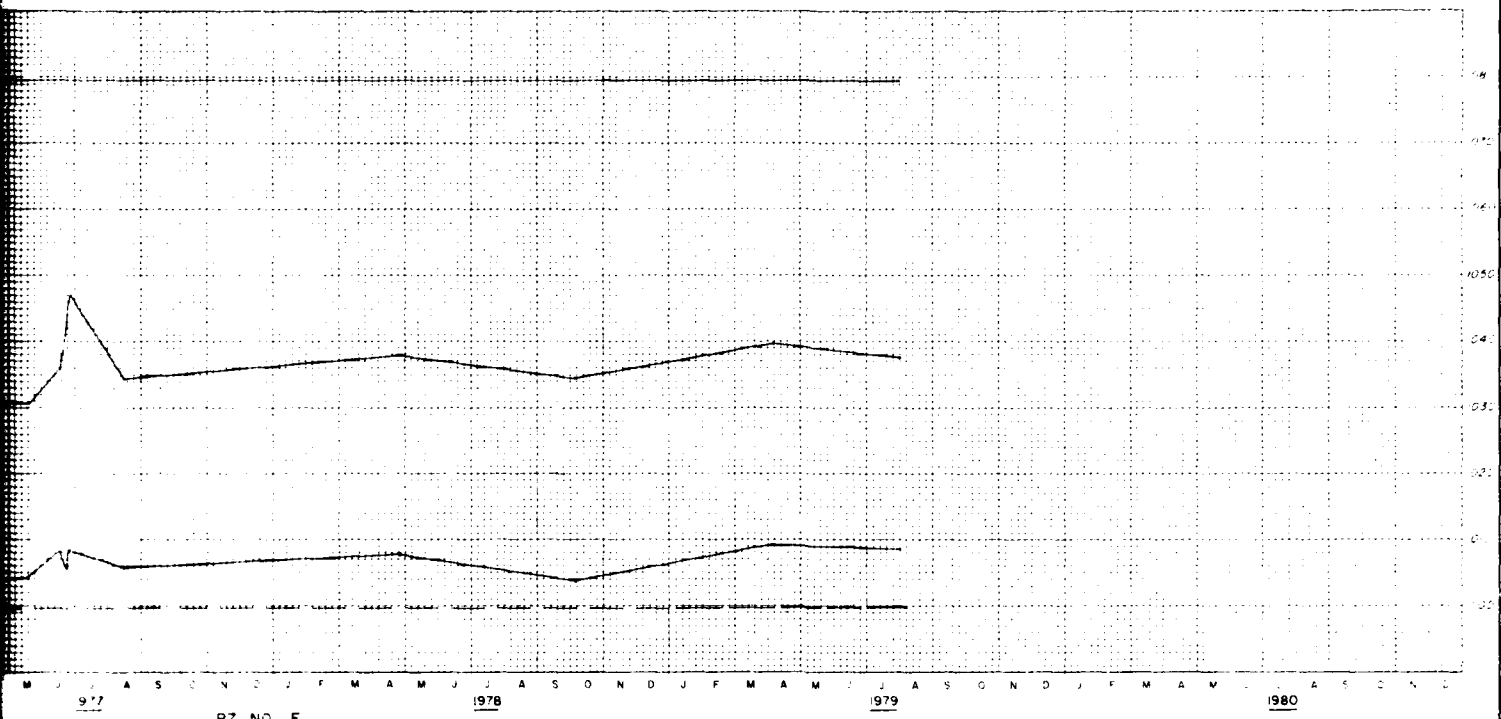
In 1 sheet

Sheet No. 1

Scale as shown

CORPS OF ENGINEERS U. S. ARMY
KANSAS CITY DISTRICT
FILE NO. 0-5-1008
AUGUST 1977





LEGEND
 OPEN TUBE ————
 PNEUMATIC CELL - - - -

Revised August 1979
 MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

PIEZOMETER PLOTS
 PZ NO. E

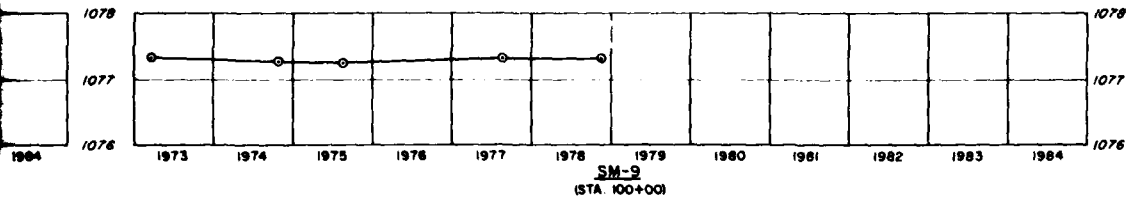
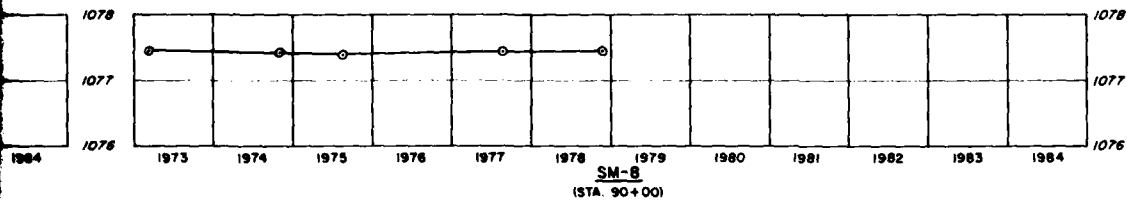
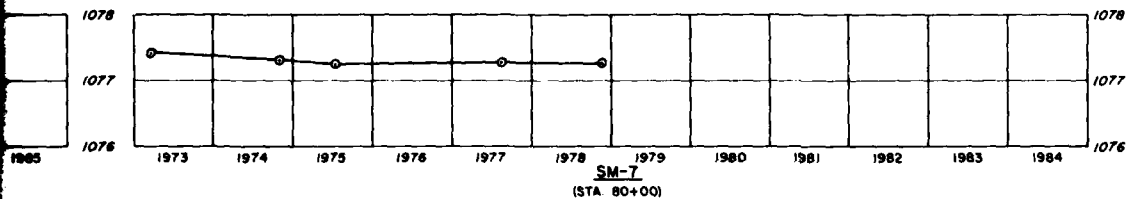
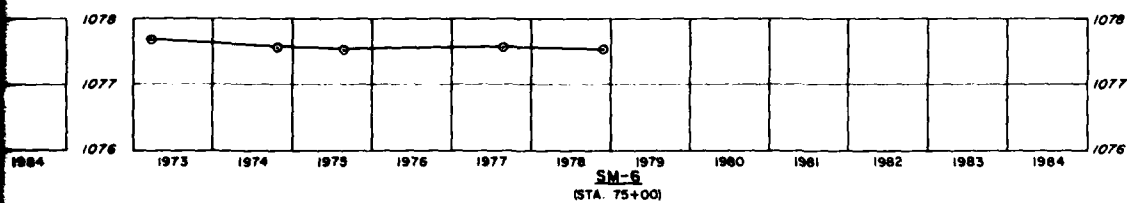
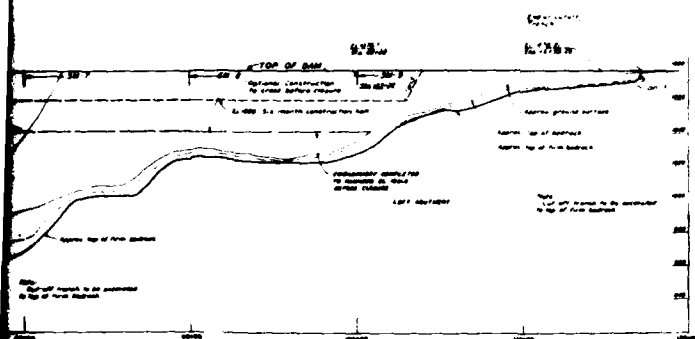
In 1 sheet

Sheet No. 1

CORPS OF ENGINEERS U. S. ARMY
 KANSAS CITY DISTRICT

FILE NO. 0-5-1006
 AUGUST 1977

Scale as shown



MARAI DES CYGNES RIVER, KANSAS
MELVERN LAKE
EMBANKMENT CRITERIA AND PERFORMANCE REPORT

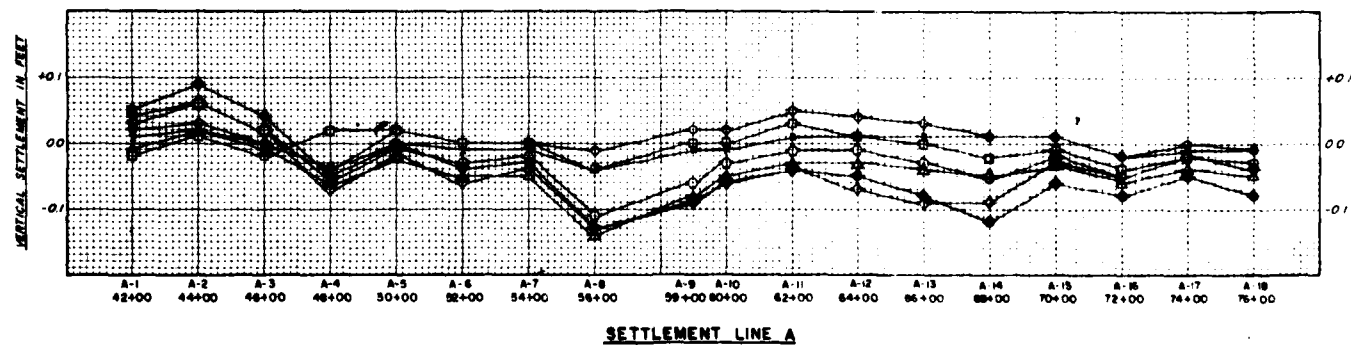
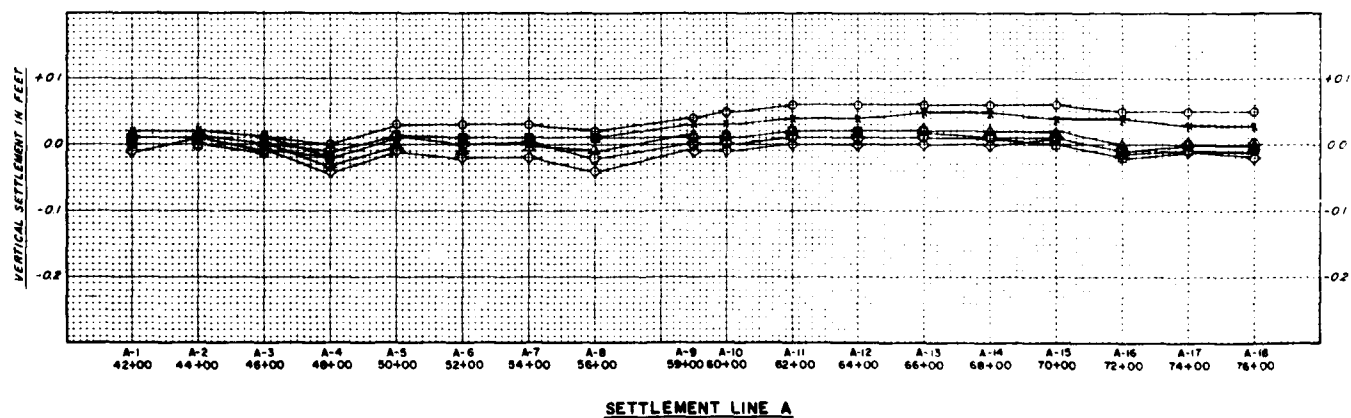
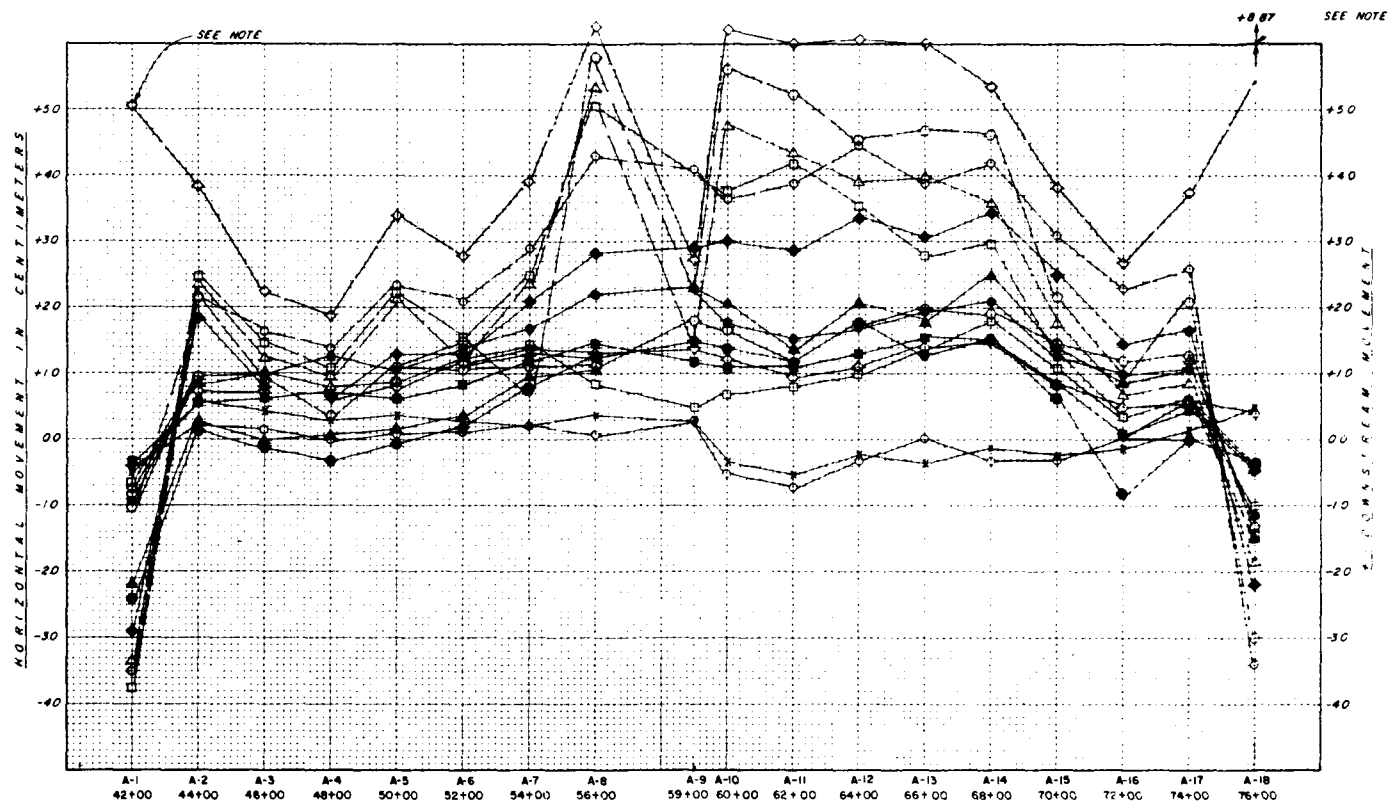
SETTLEMENT MONUMENT PLOTS
SM-1 THRU SM-9

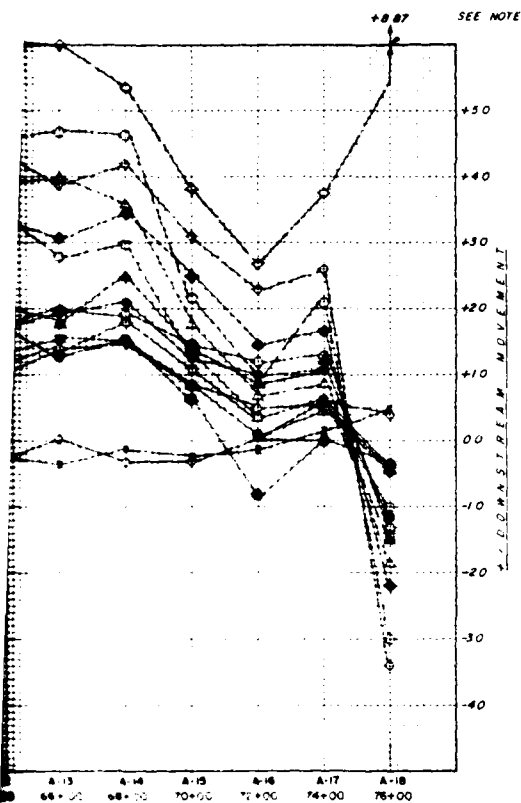
In 1 sheets

Sheet No. 1

Scale as shown

CORPS OF ENGINEERS U. S. ARMY
KANSAS CITY DISTRICT
FILE NO 0-5-1356
AUGUST 1979





LEGEND

- ORIGINAL SURVEY 11-5-71
- SECOND SURVEY 11-22-71
- THIRD SURVEY 12-8-71
- △ FOURTH SURVEY 1-10-72
- x FIFTH SURVEY 1-18-72
- SIXTH SURVEY 2-29-72
- SEVENTH SURVEY 3-30-72
- EIGHTH SURVEY 5-2-72
- NINTH SURVEY 6-2-72
- ▲ TENTH SURVEY 10-12-72
- ELEVENTH SURVEY 11-17-72
- TWELFTH SURVEY 3-8-73
- THIRTEENTH SURVEY 9-12-73
- FOURTEENTH SURVEY 10-24-74
- △ FIFTEENTH SURVEY 8-6-75
- SIXTEENTH SURVEY 8-5-77
- SEVENTEENTH SURVEY 11-30-78

NOTE:

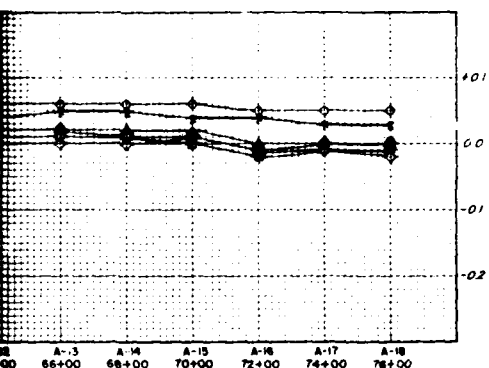
ALINEMENT WAS RUN ON NOV. 8 & 9 AND AGAIN ON NOV. 30 AND DEC. 1. BETWEEN THESE READINGS, THE INSTRUMENT PLATES WERE RESET ON MONUS 8-4, 8-17, A-1, AND A-18.

THE READINGS ON THESE PARTICULAR MONUMENTS SHOW EXPLAINABLE DIFFERENCES FROM PREVIOUS READINGS. THESE PLATES WERE ACTUALLY INSTALLED WRONG IN 1969 AND WERE NEVER CHANGED.

THE READINGS ON THE ALINEMENT MONUMENTS WERE BASICALLY THE SAME ON NOV. 8 & 9 AND NOV. 30 & DEC. 1.

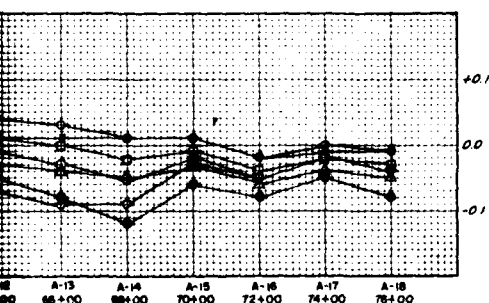
LEGEND

- ORIGINAL SURVEY 1-20-72
- x SECOND SURVEY 2-20-72
- THIRD SURVEY 3-29-72
- FOURTH SURVEY 4-24-72
- △ FIFTH SURVEY 5-1-72
- SIXTH SURVEY 6-22-72
- SEVENTH SURVEY 10-11-72



LEGEND

- ORIGINAL SURVEY 1-20-72
- x EIGHTH SURVEY 11-21-72
- NINTH SURVEY 3-7-72
- TENTH SURVEY 9-13-73
- △ ELEVENTH SURVEY 10-24-74
- TWELFTH SURVEY 8-1-75
- THIRTEENTH SURVEY 8-10-77
- FOURTEENTH SURVEY 11-30-78



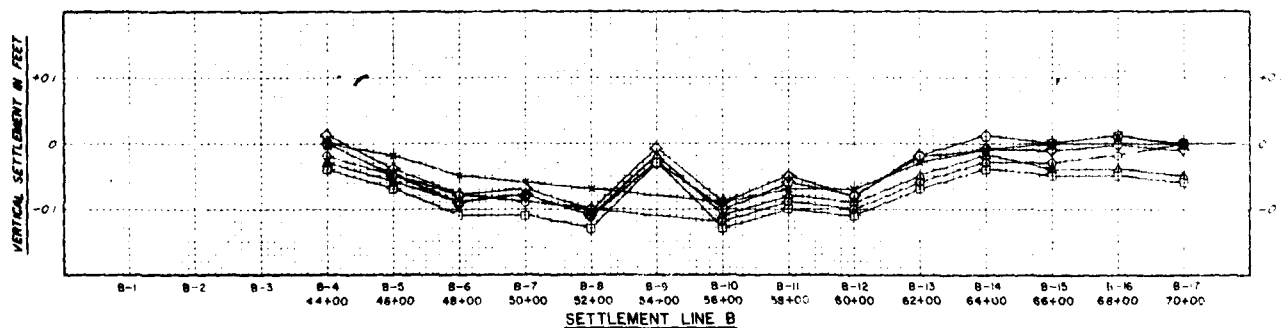
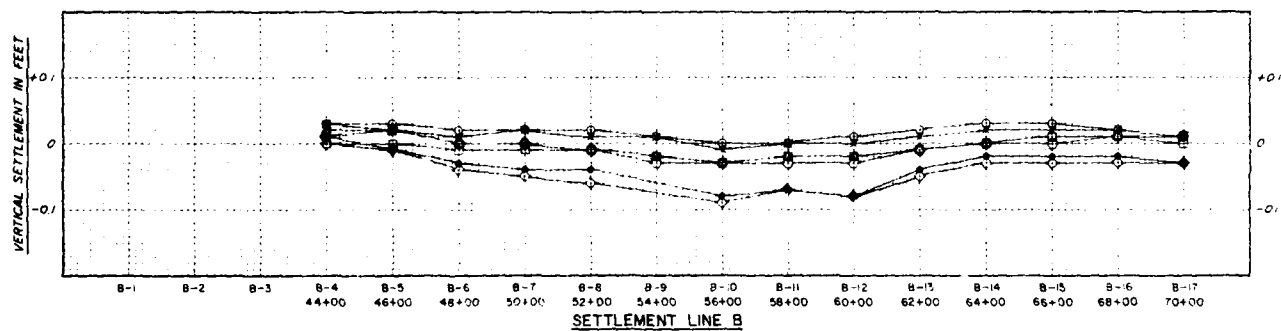
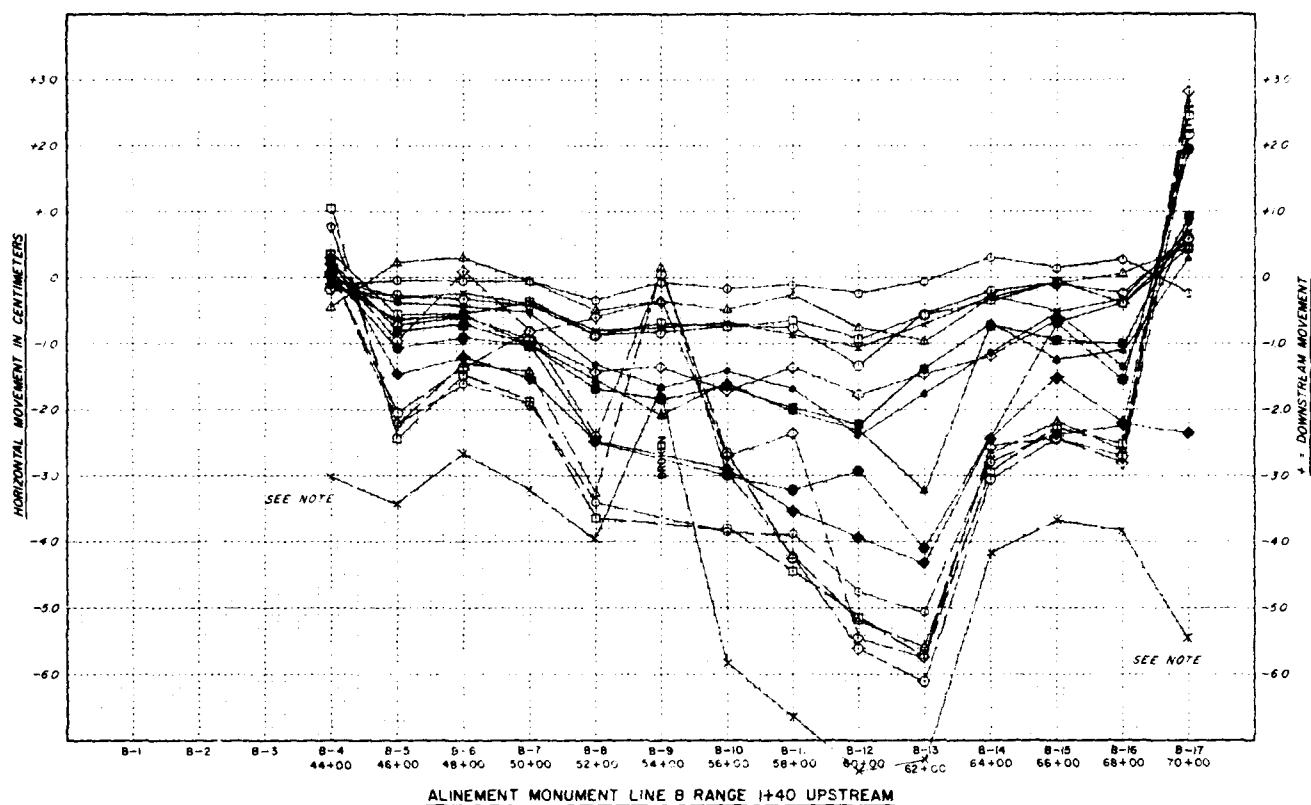
Revised August 15
MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE
PERIODIC INSPECTION

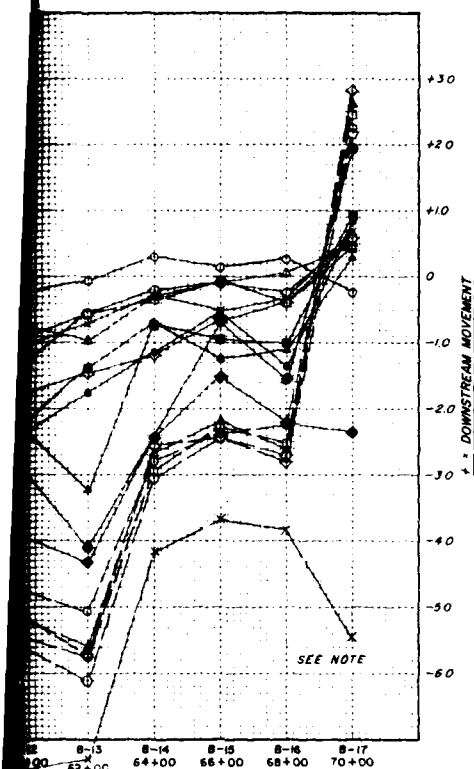
ALINEMENT MONUMENTS
LINE A

In 1 sheet

Sheet No. 1
CORPS OF ENGINEERS U.S. ARMY
KANSAS CITY DISTRICT
FILE NO. 0-5-1318

Scale as shown





LEGEND

- ORIGINAL SURVEY 11-4-71
- SECOND SURVEY 11-23-71
- THIRD SURVEY 12-8-71
- △ FOURTH SURVEY 1-10-72
- x FIFTH SURVEY 1-18-72
- SIXTH SURVEY 2-23-72
- SEVENTH SURVEY 3-30-72
- EIGHTH SURVEY 4-26-72
- NINTH SURVEY 5-2-72
- ▲ TENTH SURVEY 6-21-72
- ELEVENTH SURVEY 10-11-72
- ◆ TWELFTH SURVEY 11-15-72
- THIRTEENTH SURVEY 3-5-73
- FOURTEENTH SURVEY 9-12-73
- △ FIFTEENTH SURVEY 10-24-74
- SIXTEENTH SURVEY 8-7-75
- ◇ SEVENTEENTH SURVEY 8-9-77
- x EIGHTEENTH SURVEY 11-30-78

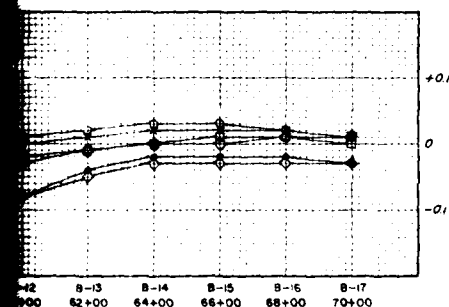
NOTES:

ALINEMENT WAS RUN ON NOV 8 & 9 AND AGAIN ON NOV 30 AND DEC 1

BETWEEN THESE READINGS, THE INSTRUMENT PLATES WERE RESET ON MONUS B-4, B-17, A-1, AND A-18.

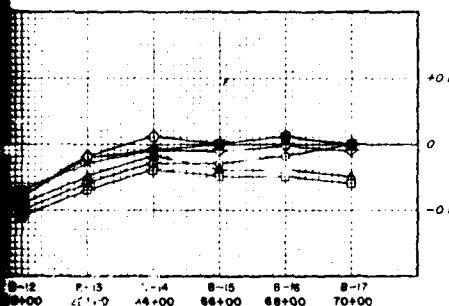
THE READINGS ON THESE PARTICULAR MONUMENTS SHOW EXPLAINABLE DIFFERENCES FROM PREVIOUS READINGS THESE PLATES WERE ACTUALLY INSTALLED WRONG IN 1969 AND WERE NEVER CHANGED.

THE READINGS ON THE ALINEMENT MONUMENTS WERE BASICALLY THE SAME ON NOV. 8 & 9 AND NOV 30 & DEC 1



LEGEND

- ORIGINAL SURVEY 1-20-72
- x SECOND SURVEY 2-22-72
- THIRD SURVEY 3-29-72
- FOURTH SURVEY 4-24-72
- △ FIFTH SURVEY 5-1-72
- SIXTH SURVEY 6-21-72
- ◇ SEVENTH SURVEY 10-11-72
- EIGHTH SURVEY 11-20-72



LEGEND

- ORIGINAL SURVEY 1-20-72
- v NINTH SURVEY 3-7-73
- TENTH SURVEY 9-13-73
- ELEVENTH SURVEY 10-24-74
- △ TWELFTH SURVEY 8-1-75
- THIRTEENTH SURVEY 8-9-77
- ◇ FOURTEENTH SURVEY 11-7-78

MAINTAINED August 1979
MARAI DES CYGNES RIVER, KANSAS
MELVERN LAKE
PERIODIC INSPECTION

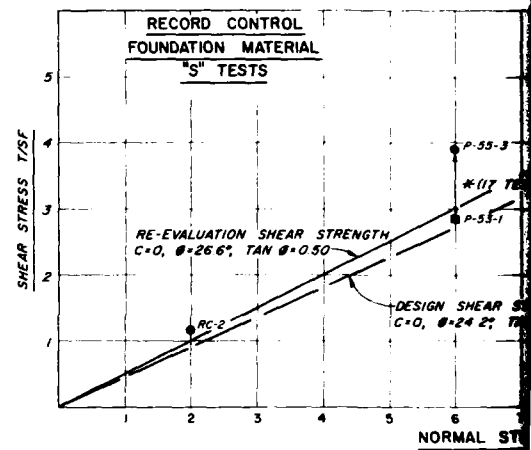
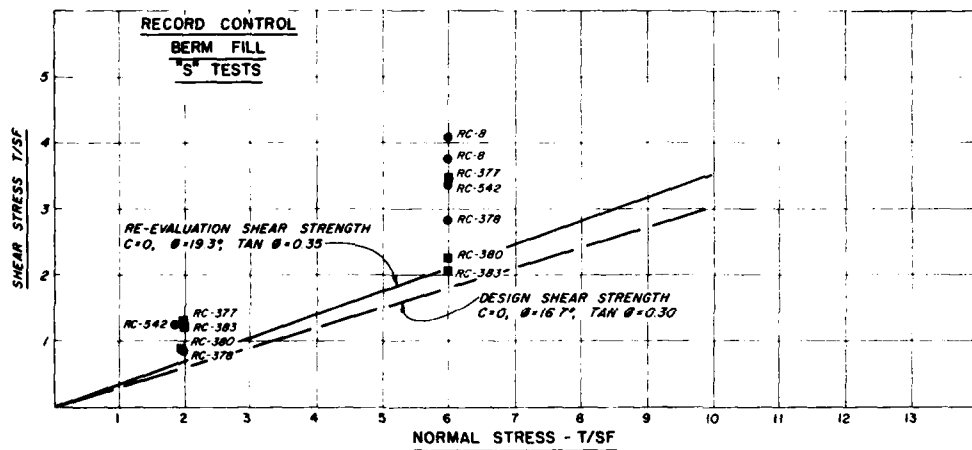
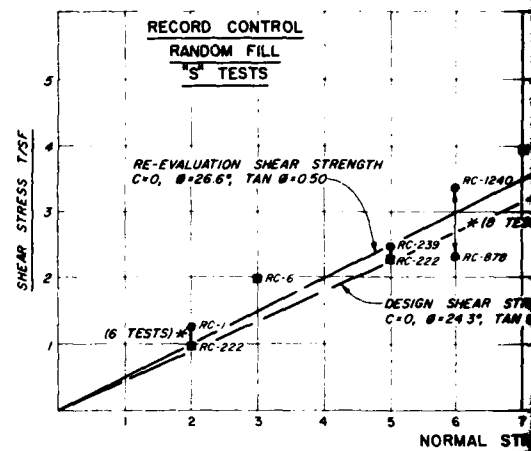
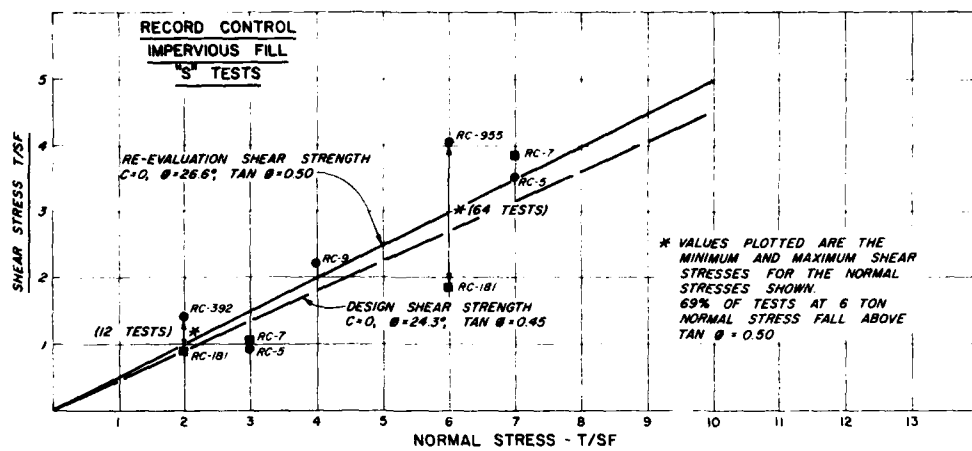
ALINEMENT MONUMENT
LINE B

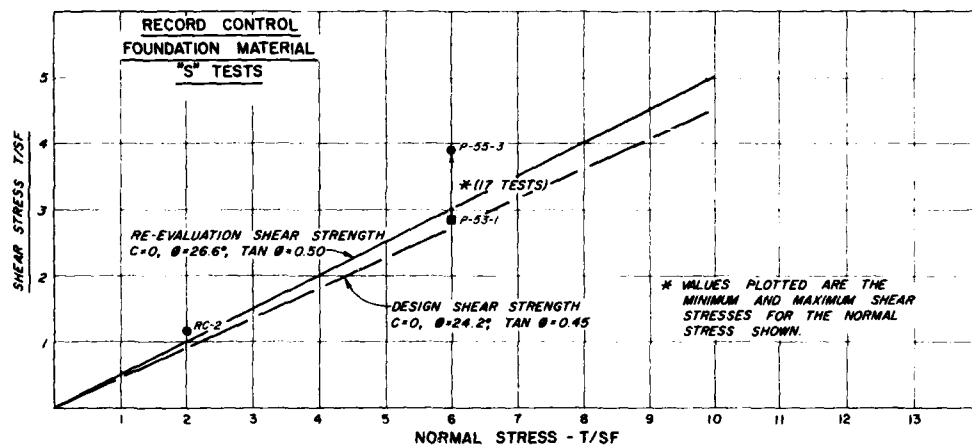
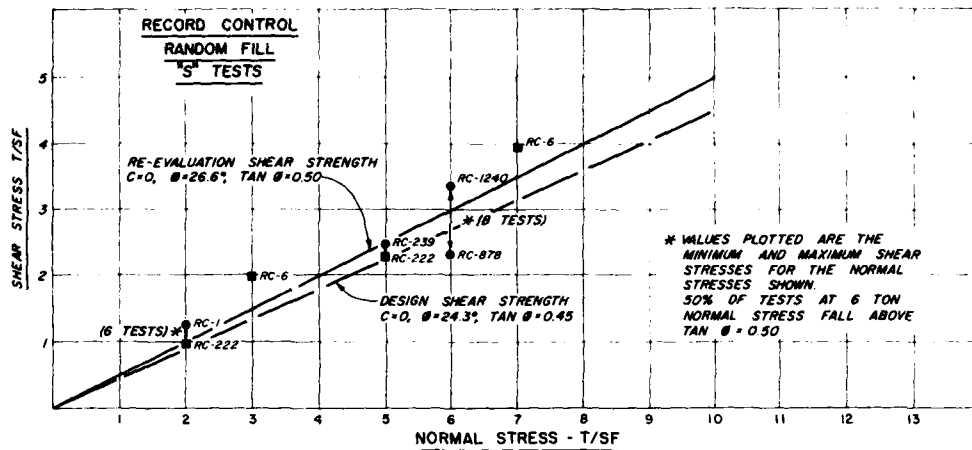
In 1 sheet

Sheet No. 1

Scale as shown

CORPS OF ENGINEERS U.S. ARMY
KANSAS CITY DISTRICT
FILE NO 0-5-1319





LEGEND

LEAN CLAY ●
FAT CLAY ■

Revised August 1979
MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

**RECORD CONTROL
"S" TESTS
EMBANKMENT MATERIALS**

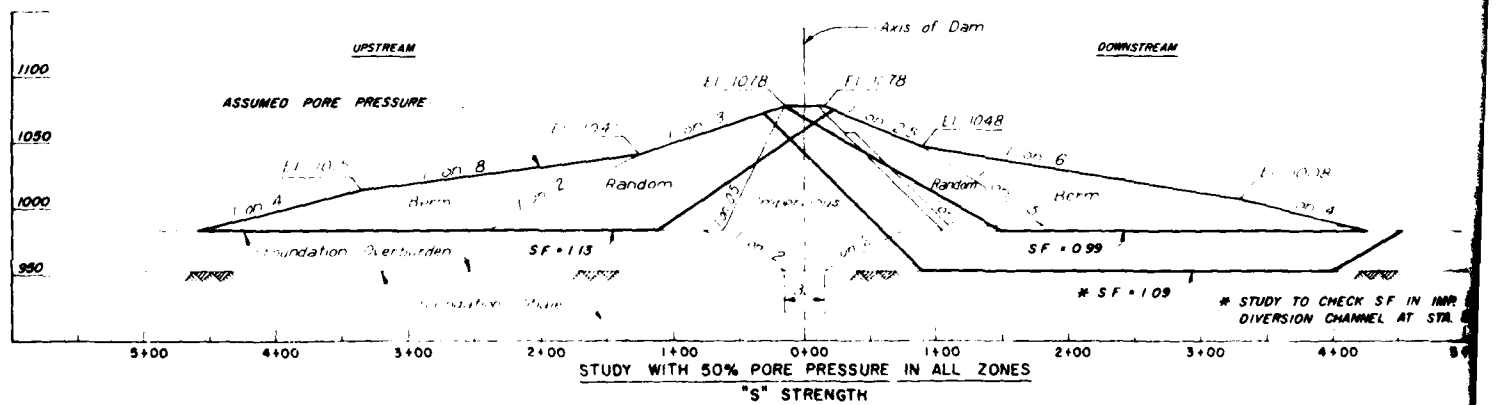
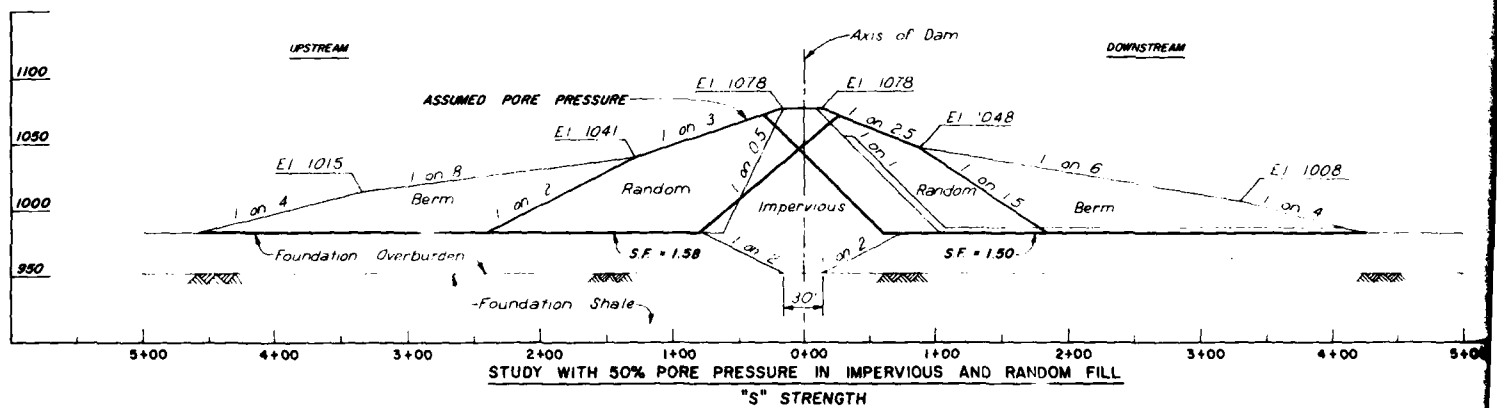
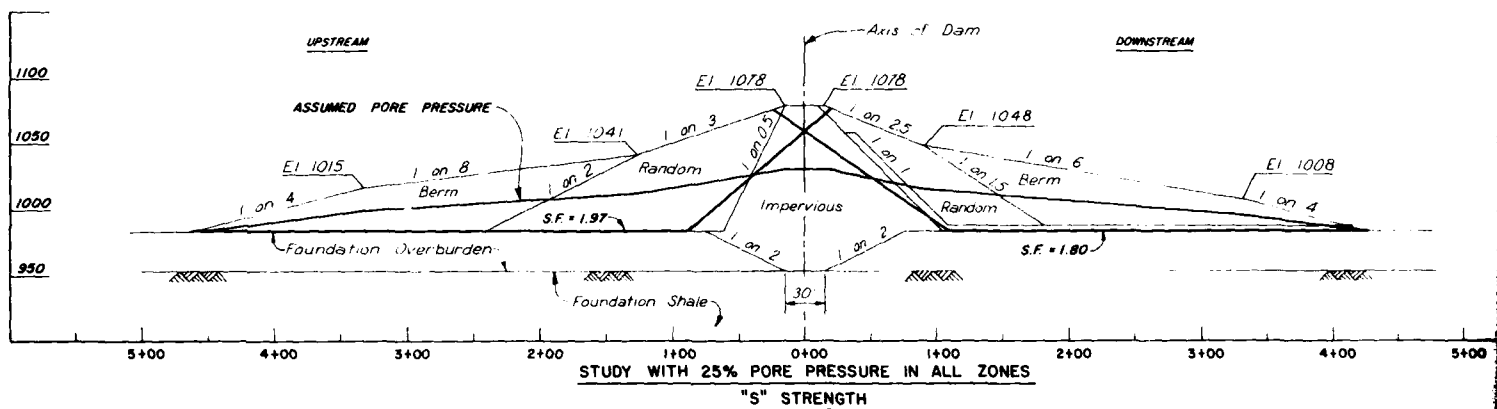
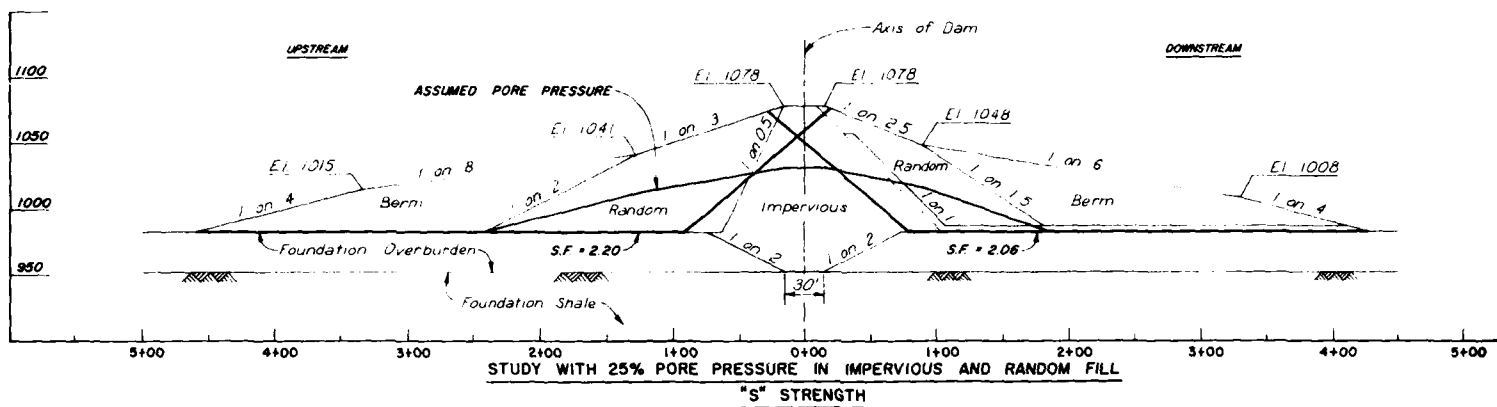
In 1 sheets

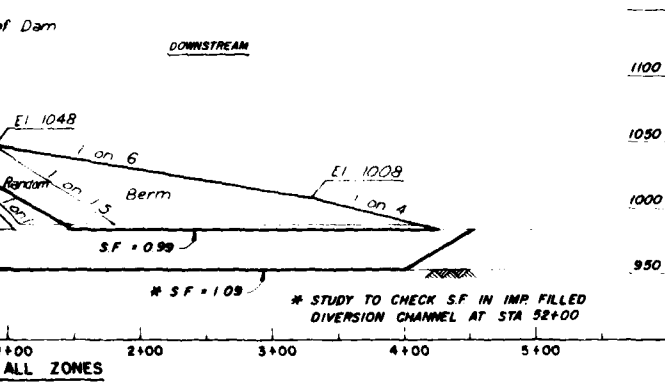
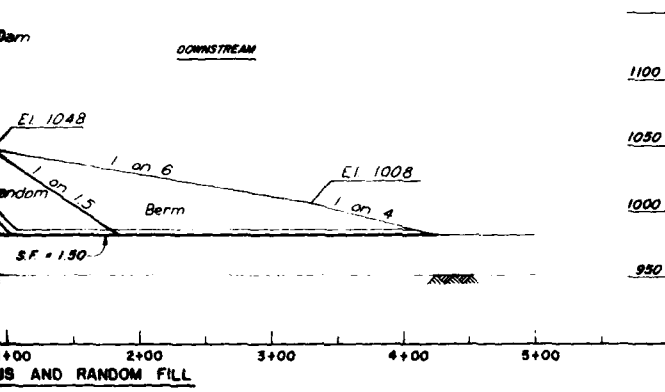
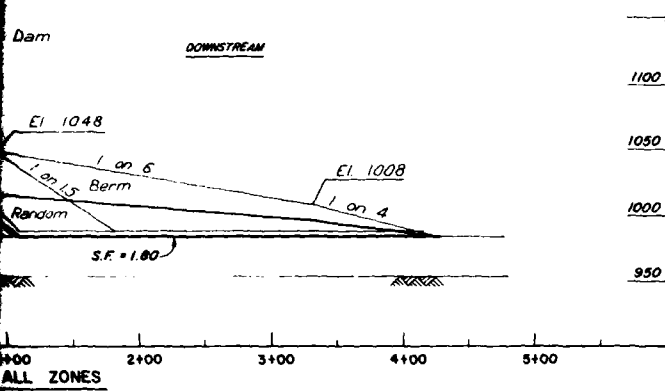
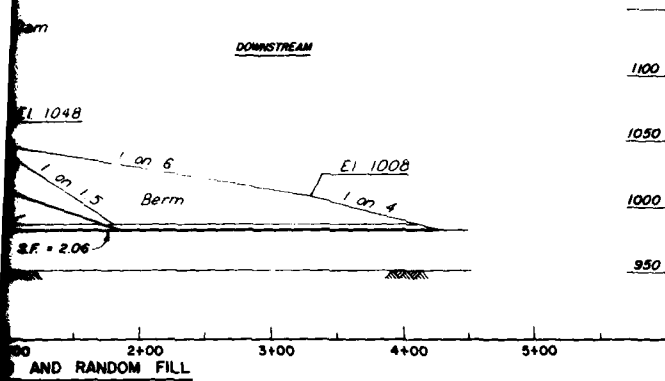
Sheet No. 1

Scale as shown

CORPS OF ENGINEERS U. S. ARMY
KANSAS CITY DISTRICT
FILE NO 0-5-1313
AUGUST 1975

ELEVATION IN FEET ABOVE MEAN SEA LEVEL

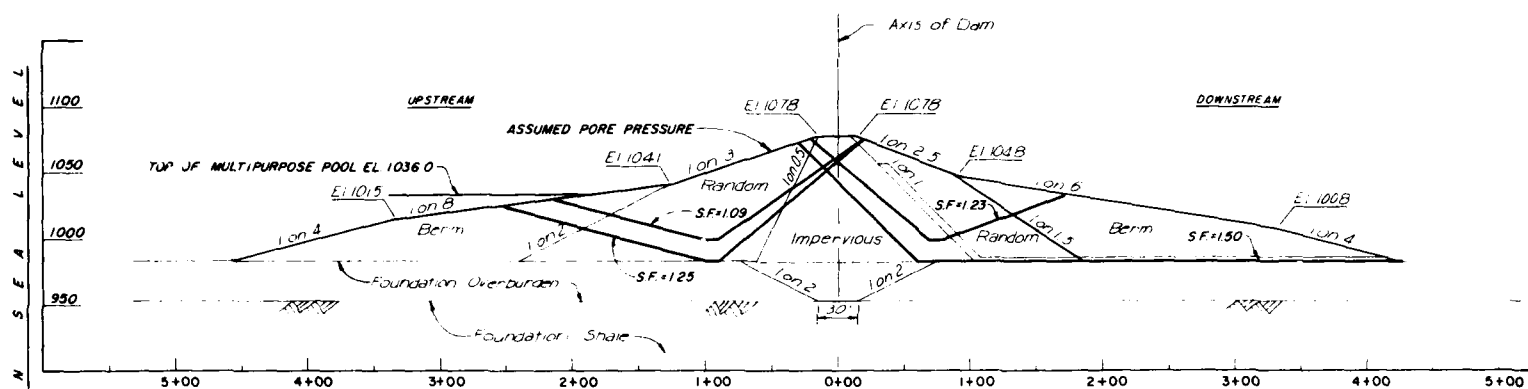




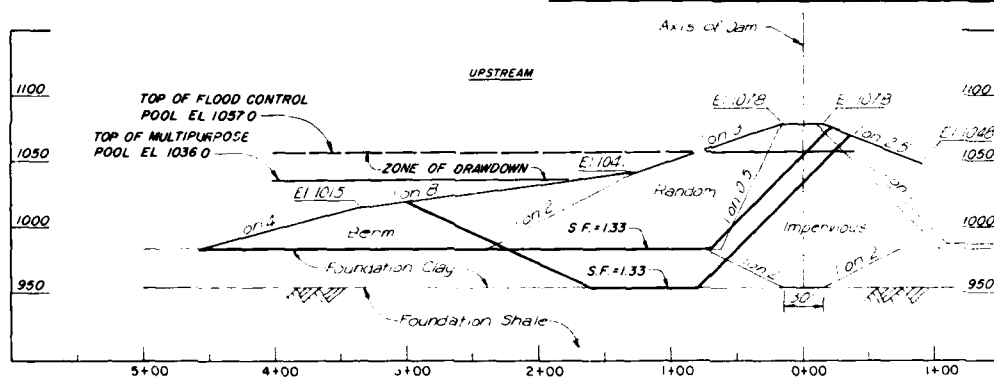
PHYSICAL SOIL CONSTANTS											
MATERIAL	UNIT WEIGHT		DESIGN SHEAR STRENGTHS (RECORD CONTROL)								
	SAT	DRAINED	C (TSF)	φ	TAN φ	C (TSF)	φ	TAN φ	C (TSF)	φ	TAN φ
IMPERVIOUS AND RANDOM	125	120	1.30	0.00	0.00	0.40	12.9°	0.23	0.00	26.6°	0.50
BERM	115	110	1.00	0.00	0.00	0.35	10.2°	0.16	0.00	19.3°	0.35
FOUNDATION OVERBURDEN	120	115	0.60	0.00	0.00	0.30	11.3°	0.20	0.00	26.6°	0.50
FOUNDATION SHALE	120	115	0.60	5.7°	0.10	0.40	11.3°	0.20	0.00	21.8°	0.40

Revised August 1979
MARAI DES CYGNES RIVER, KANSAS
MELVERN LAKE
RE-EVALUATION
STABILITY STUDIES
EMBANKMENT AND FOUNDATION

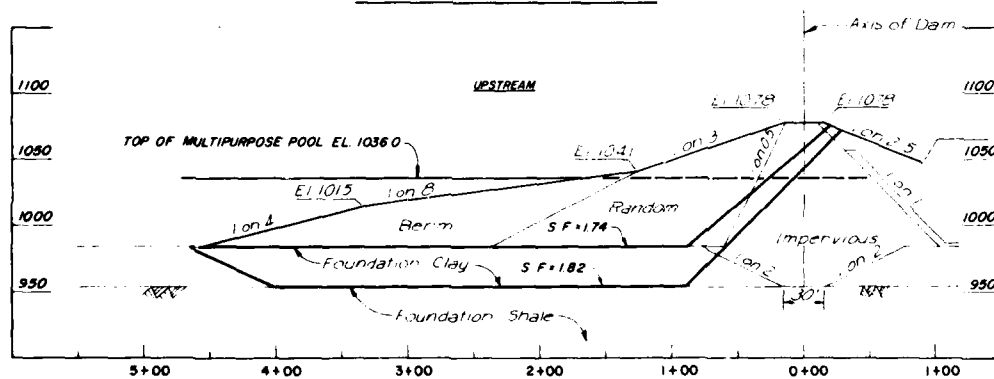
In 2 sheets
Sheet No. 1
Scale as shown
CORPS OF ENGINEERS
KANSAS CITY DISTRICT
FILE NO. O-5-1314
AUGUST 1975



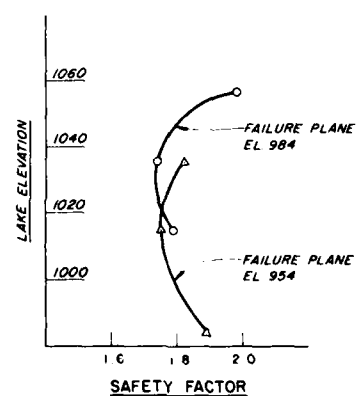
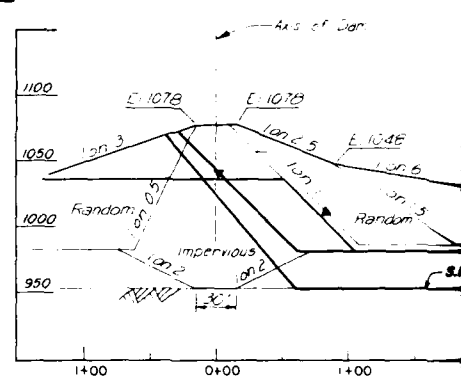
STUDY WITH LAKE AT ELEVATION 1036.0 AND 50% PORE
PRESSURE IN IMPERVIOUS AND RANDOM FILL - "S" STRENGTH

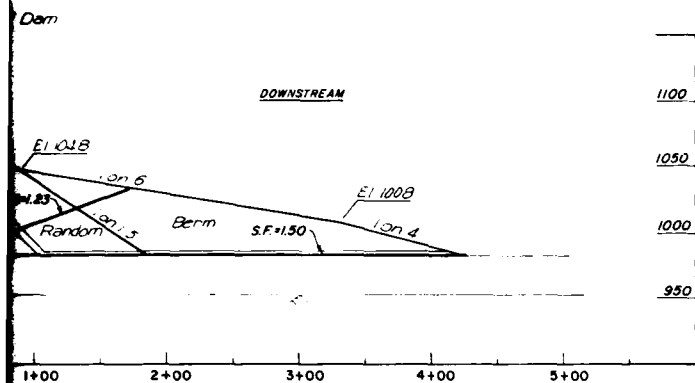


RAPID DRAWDOWN CASE
FULL POOL TO MULTIPURPOSE POOL

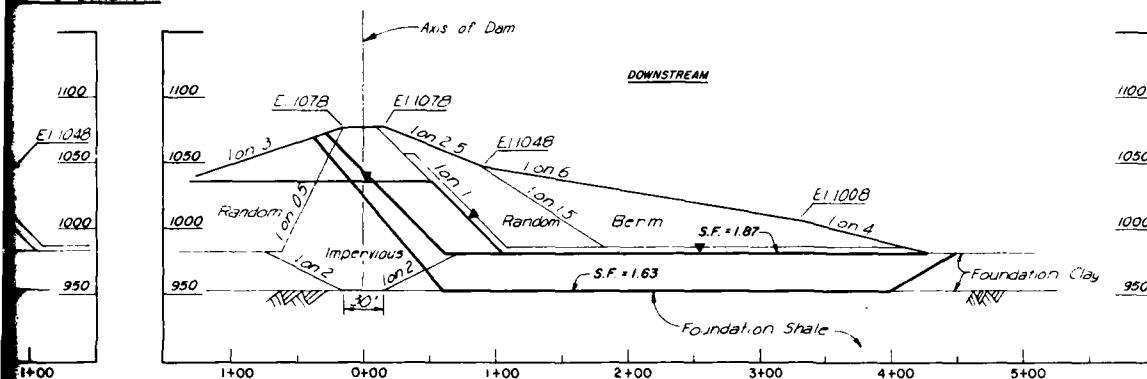


PARTIAL POOL CASE

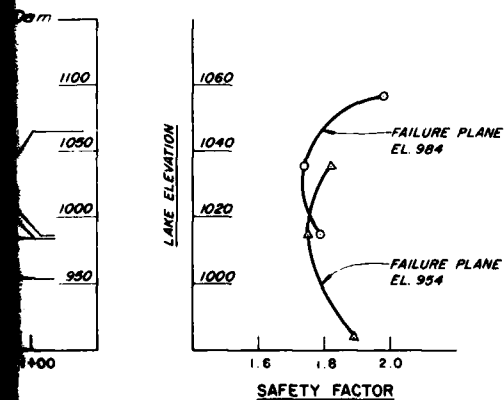




AND 50% PORE
WATER STRENGTH



STEADY SEEPAGE CASE
LAKE ELEVATION 1036.0



Revised August 1979
MARAIS DES CYGNES RIVER, KANSAS
MELVERN LAKE

RE-EVALUATION
STABILITY STUDIES
EMBANKMENT AND FOUNDATION

In 2 sheets

Sheet No 2
CORPS OF ENGINEERS U S ARMY
KANSAS CITY DISTRICT
FILE NO. 0-5-1315
AUGUST 1975

Scale as shown

2
PLATE NO. 73

**D
FI**